

1-1

$$m_e = 9.109 \times 10^{-31} \text{ kg}$$

$$m_p = 1.673 \times 10^{-27} \text{ kg}$$

$$G = 6.673 \times 10^{-11} \frac{\text{m}^3}{\text{kg s}^2}$$

$$r = 0.5 \text{ \AA} = 0.5 \times 10^{-10} \text{ m}$$

$$F_g = \frac{G m_1 m_2}{r^2}$$

$$= \frac{(6.673 \times 10^{-11})(9.109 \times 10^{-31})(1.673 \times 10^{-27})}{(0.5 \times 10^{-10})^2}$$

$$F_g = 4.068 \times 10^{-47} \text{ N}$$

$$F_e = \frac{K e_1 e_2}{r^2}$$

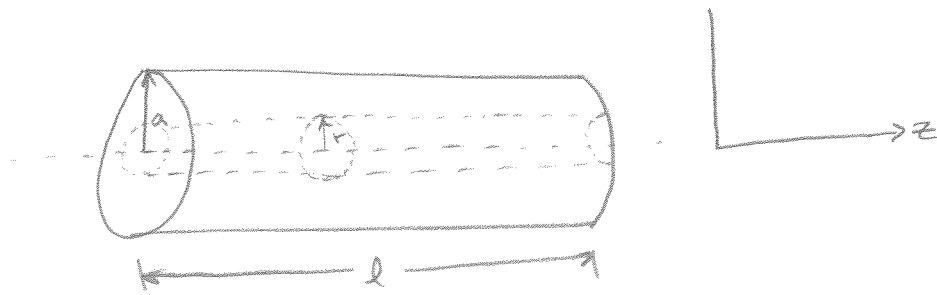
$$K = 8.987 \times 10^9 \frac{\text{Nm}^2}{\text{C}^2}$$

$$e = 1.602 \times 10^{-19} \text{ C}$$

$$F_e = \frac{(8.987 \times 10^9)(1.602 \times 10^{-19})^2}{(0.5 \times 10^{-10})^2}$$

$$F_e = 9.133 \times 10^{-8} \text{ N}$$

$$\frac{F_e}{F_g} = 2.245 \times 10^{39}$$



$$\Delta P \sim l$$

$$\frac{F_z}{A_v} = \eta \frac{dv_z}{dr}$$

$$A_v = 2\pi r l \quad \{\text{surface area of cylinder}\}$$

$$\Delta P (\pi r^2) + F_z = 0 \quad \{\text{steady flow}\}$$

$$\Delta P (\pi r^2) + 2\pi r l \eta \frac{dv_z}{dr} = 0$$

$$\frac{dv_z}{dr} = \frac{r \Delta P}{2\eta l}$$

$$v_z - v_0 = \frac{\Delta P}{2\eta l} \int_0^r r' dr'$$

$$v_z = \frac{\Delta P}{4\eta l} r^2 + v_0$$

$$\Phi = \int v_z dA$$

$$A = \pi r^2 \rightarrow dA = 2\pi r dr$$

$$= \int v_z (2\pi r dr)$$

$$= 2\pi \frac{\Delta P}{4\eta l} \int_0^a r^3 dr \quad \{\text{ignoring } v_0\}$$

$$= \frac{\pi \Delta P}{2\eta l} \left[\frac{r^4}{4} \right]_0^a$$

$$= \frac{\pi \Delta P a^4}{8\eta l}$$

$$\therefore \Delta P \sim \frac{\Phi \eta l}{a^4}$$

1-5

- a) v_0 = motorist speed
 τ = reaction time
 a = braking deceleration

$$v_f^2 = v_0^2 + 2a(\Delta x)$$

$$0 = v_0^2 - 2a(x_b) \quad x_b = \text{braking distance}$$

$$x_b = \frac{v_0^2}{2a}$$

$$x_r = v_0 \tau$$

$$S_{\min} = x_r + x_b$$

$$S_{\min} = v_0 \tau + \frac{v_0^2}{2a}$$

- b) t = time of amber light

when traveling at v_0 the maximum distance from the intersection when the light turns amber such that the car continues into the intersection with speed v_0 without running the red light is simply

$$S_{\max} = v_0 t$$

- c) Given $v_0 > v_{0\max} = 2a(t - \tau)$

at $v_{0\max}$

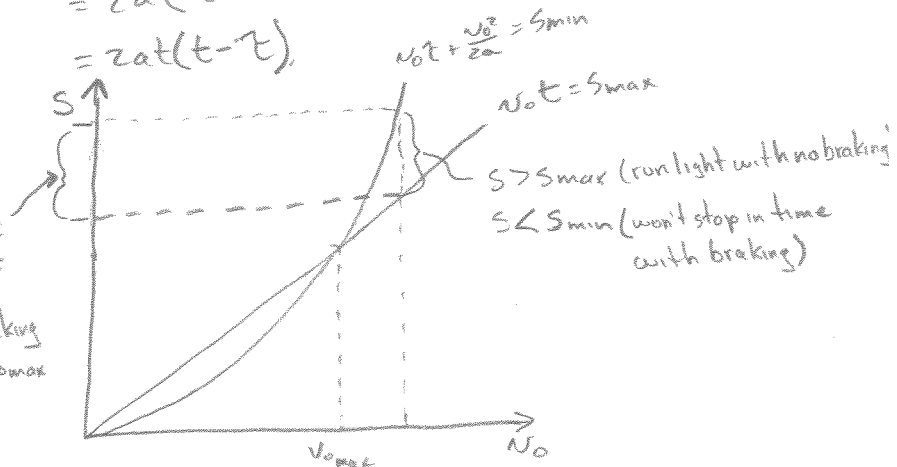
$$S_{\min} = 2a(t - \tau)\tau + \frac{(2a(t - \tau))^2}{2a}$$

$$S_{\min} = 2a(t - \tau)\tau + 2a(t - \tau)^2 = 2a(t\tau - \tau^2 + t^2 - 2t\tau + \tau^2) = 2a(t^2 - t\tau)$$

$$S_{\max} = 2a(t - \tau)t = 2at(t - \tau)$$

Hence $S_{\min} = S_{\max}$ at $v_{0\max}$

distance range where red light run will occur regardless of braking or not at $v_0 > v_{0\max}$



2

$V_0 > V_{0max}$ the range in question is

$$S_{\text{max}} \leq S \leq S_{\text{min}}$$

$$v_0 t < s < v_0 t + \frac{v_0^2}{2a}$$

d) $\tau = 0,5 \text{ s}$

$t = 5s$

$$a = 5 \text{ m/s}^2$$

$$N_{\text{max}} = 2a(t - \tau)$$

$$= 2(5)(5 - .5)$$

$$= 45 \text{ m/s} \cdot \frac{1 \text{ in}}{0.0254 \text{ m}} \cdot \frac{1 \text{ ft}}{12 \text{ in}} \cdot \frac{1 \text{ mile}}{5,280 \text{ ft}} \cdot \frac{3600 \text{ s}}{1 \text{ hr}}$$

$$V_{0\max} = 10 \text{ mph}$$

$$N_0 = \frac{2}{3} N_{\text{max}}$$

$$v_0 = 30 \text{ m/s} = 67 \text{ mph}$$

$$S_{\text{min}} = N_0 Z + \frac{V_0^2}{2a}$$

$$= 30(.5) + \frac{(30)^2}{14}$$

$$= 79 \text{ m}$$

$$S_{min} = 260 \text{ st}$$

$$S_{\max} = v_0 t$$

$$= 30 \times (5)$$

$$= 150 \text{ m}$$

$$s_{\max} = 495 \text{ ft}$$

1-11

$$r = 9.3 \times 10^7 \text{ miles} \cdot \frac{5,280 \text{ ft}}{1 \text{ mile}} \cdot \frac{12 \text{ in}}{1 \text{ ft}} \cdot \frac{.0254 \text{ m}}{1 \text{ in}} = 1.50 \times 10^{11} \text{ m}$$

$$T = 1 \text{ year} \cdot \frac{365 \text{ days}}{1 \text{ year}} \cdot \frac{24 \text{ hrs}}{1 \text{ day}} \cdot \frac{3600 \text{ sec}}{1 \text{ hr}} = 3.154 \times 10^7 \text{ sec}$$

$$F_g = \frac{G m_1 m_2}{r^2} \quad \begin{array}{l} m_1 = m_e \\ m_2 = m_s \end{array}$$

$$F_{\text{cent}} = m_1 \frac{v_r^2}{r}$$

$$F_{\text{cent}} = F_g$$

$$\frac{m_1 v_r^2}{r} = \frac{G m_1 m_2}{r^2}$$

$$\frac{v_r^2 r}{G} = m_2 \quad v_r = r \omega, \quad \omega = \frac{2\pi}{T}$$

$$m_s = \frac{\omega^2 r^3}{G} = 1.99 \times 10^{-7} \text{ sec}^{-1}$$

$$= \frac{(1.99 \times 10^{-7} \text{ s}^{-1})^2 (1.50 \times 10^{11} \text{ m})^3}{6.67 \times 10^{-11} \frac{\text{m}^3}{\text{kg} \cdot \text{s}^2}}$$

$$= 2.00 \times 10^{30} \text{ kg} \cdot \frac{2.2 \text{ lb}}{\text{kg}}$$

$$= 4.4 \times 10^{30} \text{ lbs} \times \frac{1 \text{ ton}}{2000 \text{ lb}}$$

$$m_s = 2.2 \times 10^{27} \text{ tons}$$

1-13

$$r_1 = 25,000 \text{ light years} \cdot 2.99 \times 10^8 \frac{\text{m}}{\text{s}} \cdot \frac{3600 \text{ s}}{\text{hr}} \cdot \frac{24 \text{ hr}}{\text{day}} \cdot \frac{365 \text{ day}}{\text{year}} = 2.357 \times 10^{20} \text{ m}$$

$$V_{T5} = 175 \frac{\text{miles}}{\text{sec}} \cdot \frac{5,280 \text{ ft}}{1 \text{ mile}} \cdot \frac{12 \text{ in}}{1 \text{ ft}} \cdot \frac{0.0254 \text{ m}}{1 \text{ in}} = 2.82 \times 10^5 \text{ m/s}$$

$$F_g = \frac{m_s m_G G}{r_1^2}$$

$$F_{\text{cent}} = \frac{m V_{T5}^2}{r_1}$$

$$= \frac{m_s V_{T5}^2}{r_1}$$

$$F_g = F_{\text{cent}}$$

$$\frac{m_s V_{T5}^2}{r_1} = G \frac{m_s m_G}{r_1^2}$$

$$m_G = \frac{V_{T5}^2 r_1}{G}$$

For the Sun-Earth system

$$F_g = \frac{G m_e m_s}{r_2^2}$$

$$F_{\text{cent}} = \frac{m_e V_{Te}^2}{r_2}$$

$$F_g = F_{\text{cent}}$$

$$\frac{G m_e m_s}{r_2^2} = \frac{m_e V_{Te}^2}{r_2}$$

$$G = \frac{V_{Te}^2 r_2}{m_s}$$

$$V_{Te} = \omega_e r_2 \quad \omega = \frac{2\pi}{T} = \frac{2\pi}{1 \text{ year}} = 1.99 \times 10^{-7} \text{ s}^{-1}$$

$$r_2 = 1.50 \times 10^{11} \text{ m}$$

$$m_G = \frac{V_{T5}^2 r_1}{G}$$

$$= \frac{V_{T5}^2 r_1 \cdot m_s}{V_{Te}^2 r_2}$$

$$= \frac{V_{T5}^2 r_1 \cdot m_s}{\omega_e^2 r_2^3}$$

$$\frac{m_G}{m_s} = \frac{V_{T5}^2 r_1}{\omega_e^2 r_2^3} = \frac{(2.82 \times 10^5)^2 (2.357 \times 10^{20})}{(1.99 \times 10^{-7})^2 (1.50 \times 10^{11})^3} = 1.40 \times 10^{11}$$

2-1

$$a) F = 3000 \text{ lb-wt}$$

convert to MKS units

$$1 \text{ lb force} = 4.448 \text{ N}$$

$$F = mg$$

$$F = \left(\frac{4.448 \text{ N}}{1 \text{ lb}} \cdot 3000 \text{ lb} \right)$$

$$F = 13344 \text{ N}$$

$$V_1 = 20 \text{ mph} = \frac{20 \text{ miles}}{1 \text{ hr}} \cdot \frac{5280 \text{ ft}}{1 \text{ mile}} \cdot \frac{12 \text{ in}}{1 \text{ ft}} \cdot \frac{.0254 \text{ m}}{1 \text{ in}} \cdot \frac{1 \text{ hr}}{3600 \text{ sec}} = 8.9 \frac{\text{m}}{\text{s}}$$

$$FV_1 = (13344 \text{ N}) (8.9 \frac{\text{m}}{\text{s}})$$

$$= 118761 \frac{\text{N} \cdot \text{m}}{\text{s}}$$

$$= 118761 \text{ W} \cdot \frac{1 \text{ hp}}{746 \text{ W}}$$

$$\boxed{FV_1 = 160 \text{ hp}}$$

$$V_2 = 160 \text{ mph} \cdot \frac{8.9 \text{ m/s}}{20 \text{ mph}} =$$

$$= 5V_1$$

$$FV_2 = 5FV_1$$

$$\boxed{FV_2 = 800 \text{ hp}}$$

$$V_3 = 300 \text{ mph} \cdot \frac{8.9 \text{ m/s}}{20 \text{ mph}} =$$

$$= 15V_1$$

$$FV_3 = 15FV_1$$

$$\boxed{FV_3 = 2400 \text{ hp}}$$

b) $P = 500 \text{ hp}$

$$V_1 = 20 \text{ mph} = 8.9 \frac{\text{m}}{\text{s}}$$

$$P = 500 \text{ hp} \cdot \frac{746 \text{ W}}{\text{hp}}$$

$$= 373000 \text{ W}$$

$$P = Fv$$

$$F = \frac{P}{v}$$

$$F_1 = \frac{P}{V_1}$$

$$= \frac{373000 \text{ W}}{8.9 \frac{\text{m}}{\text{s}}}$$

$$= 41910.11 \text{ N}$$

$$= 41910.11 \text{ N} \cdot \frac{1 \text{ lb-wt}}{4.448 \text{ N}}$$

$$= 9422 \text{ lb-wt}$$

$$F_1 = 9420 \text{ lb-wt}$$

$$F_2 = \frac{P}{V_2}$$

$$= \frac{P}{5V_1}$$

$$= \frac{F_1}{5}$$

$$F_2 = 1880 \text{ lb-wt}$$

$$F_3 = \frac{P}{V_3}$$

$$= \frac{P}{3V_2}$$

$$= \frac{F_2}{3}$$

$$F_3 = 630 \text{ lb-wt}$$

2-3

$$F(t) = \frac{P_0 \delta t}{\pi} \frac{1}{(t-t_0)^2 + (\delta t)^2}, \quad -\infty < t < \infty$$

$$I = \int_{t_1}^{t_2} F dt$$

$$= \int_{-\infty}^{\infty} \frac{P_0 \delta t}{\pi} \frac{dt}{(t-t_0)^2 + (\delta t)^2} \quad \{ \delta t \text{ is fixed} \}$$

$$= \frac{P_0}{\pi \delta t} \int_{-\infty}^{\infty} \frac{dt}{\left(\frac{t-t_0}{\delta t}\right)^2 + 1}$$

$$u = \frac{t-t_0}{\delta t}$$

$$= \frac{P_0}{\pi} \int_{u_1}^{u_2} \frac{du}{u^2 + 1}$$

$$du = \frac{dt}{\delta t}$$

$$dt = du \delta t$$

$$= \frac{P_0}{\pi} \int_{\theta_1}^{\theta_2} \frac{\sec^2 \theta d\theta}{\tan^2 \theta + 1}$$

$$u = \tan \theta$$

$$du = \sec^2 \theta d\theta$$

$$= \frac{P_0}{\pi} \int_{\theta_1}^{\theta_2} d\theta$$

$$= \frac{P_0}{\pi} (\theta_2 - \theta_1)$$

$$= \frac{P_0}{\pi} (\tan^{-1} u_2 - \tan^{-1} u_1)$$

$$= \frac{P_0}{\pi} (\tan^{-1}(\infty) - \tan^{-1}(-\infty))$$

$$= \frac{P_0}{\pi} \left(\frac{\pi}{2} - \left(-\frac{\pi}{2} \right) \right)$$

$$\boxed{I = P_0}$$

For N_0 at $t = -\infty$

$$P_f \cdot P_0 = \int_{-\infty}^{\infty} F dt = P_0$$

$$m v_f - m v_0 = P_0 \rightarrow$$

$$\boxed{N_f = \frac{P_0}{m} + v_0}$$

2-5

$$F(t) = F_0 \sin^2 \omega t$$

$$v_0 = v(0) = 0$$

$$x_0 = x(t) = 0$$

$$m \ddot{x} = F$$

$$\ddot{x} = \frac{F_0}{m} \sin^2 \omega t$$

$$\begin{aligned} v - v_0 &= \int dv = \int \frac{F_0}{m} \sin^2 \omega t dt \\ &= \int_0^t \frac{F_0}{m} \frac{1}{2} (1 - \cos 2\omega t') dt' \\ &= \frac{F_0}{2m} \left[t - \int_0^t \cos 2\omega t' dt' \right] \\ &= \frac{F_0}{2m} \left[t - \frac{1}{2\omega} \sin 2\omega t' \Big|_0^t \right] \\ &= \frac{F_0}{2m} \left[t - \frac{1}{2\omega} \sin 2\omega t \right] \end{aligned}$$

$$v_0 = v(0) = 0$$

$$v = \frac{F_0}{2m} \left[t - \frac{1}{2\omega} \sin 2\omega t \right]$$

$$\frac{dx}{dt} = v$$

$$\begin{aligned} x - x_0 &= \int v dt \\ &= \frac{F_0}{2m} \int_0^t \left[t' - \frac{1}{2\omega} \sin 2\omega t' \right] dt' \\ &= \frac{F_0}{2m} \left[\frac{t'^2}{2} + \frac{1}{4\omega^2} \cos 2\omega t' \right] \Big|_0^t \end{aligned}$$

$$x_0 = -\frac{F_0}{8m\omega^2}$$

$$x = \frac{F_0}{2m} \left[\frac{t^2}{2} + \frac{1}{4\omega^2} \cos 2\omega t \right] - \frac{F_0}{8m\omega^2}$$

$$x = \frac{F_0}{8m\omega^2} \left[2\omega^2 t^2 - 1 + \cos 2\omega t \right]$$

2-7

$$F(t) = \begin{cases} 0, & t < t_0 \\ \frac{p_0}{\delta t}, & t_0 \leq t \leq t_0 + \delta t \\ 0, & t > t_0 + \delta t \end{cases}$$

Find $v(t)$ and $x(t)$

$$m \frac{dv}{dt} = F(t) \quad v(0) = v_0$$

i) $t < t_0$

$$m \frac{dv}{dt} = 0, \quad v(0) = v_0$$

$$dv = 0$$

$$\int_{v_0}^v dv = 0 \quad \text{or} \quad \int dv = 0 \rightarrow v(t) + C = 0 \rightarrow v(0) + C = 0 \rightarrow v_0 + C = 0 \rightarrow C = -v_0 \Rightarrow v - v_0 = 0$$

$$v - v_0 = 0$$

$$\boxed{v(t) = v_0}$$

$$\frac{dx}{dt} = v_0$$

$$\int_{x_0=0}^x dx = \int_0^t v_0 dt \quad x(0) = 0$$

$$\boxed{x = v_0 t}$$

$$\text{ii) } t_0 \leq t \leq t_0 + \delta t$$

$$m \frac{dv}{dt} = \frac{P_0}{\delta t}$$

$$dv = \frac{P_0}{m \delta t}$$

$$\int_{v_0}^v dv = \int_{t_0}^t \frac{P_0}{m \delta t} dt$$

$$v - v_0 = \frac{P_0}{m \delta t} (t - t_0)$$

$$\boxed{v = v_0 + \frac{P_0}{m \delta t} (t - t_0)}$$

$$\frac{dx}{dt} = v_0 + \frac{P_0}{m \delta t} (t - t_0)$$

$$dx = \left(v_0 + \frac{P_0}{m \delta t} (t - t_0) \right) dt$$

$$\int_{x_0}^x dx = \int_{t_0}^t \left(v_0 + \frac{P_0}{m \delta t} (t - t_0) \right) dt$$

$$x - x_0 = v_0 t - v_0 t_0 + \frac{P_0}{2 m \delta t} (t - t_0)^2 \Big|_{t_0}^t$$

$$x - x_0 = v_0 t - v_0 t_0 + \frac{P_0}{2 m \delta t} (t - t_0)^2, \quad x_0 = v_0 t_0, \text{ the start point of the interval.}$$

$$x - v_0 t_0 = v_0 t - v_0 t_0 + \frac{P_0}{2 m \delta t} (t - t_0)^2$$

$$\boxed{x = v_0 t + \frac{P_0}{2 m \delta t} (t - t_0)^2}$$

$$\text{iii) } t > t_0 + \Delta t$$

$$m \frac{dv}{dt} = 0$$

$$dv = 0$$

$$\int_{v_0}^v dv = 0$$

$$v - v_0' = 0$$

$$v = v_0'$$

$$\boxed{v = v_0 + \frac{P_0}{m}}$$

$$v_0' = v(t_0 + \Delta t) \text{ at end of previous interval}$$

$$= v_0 + \frac{P_0}{m \Delta t} (t - t_0) \Big|_{t_0 + \Delta t}$$

$$= v_0 + \frac{P_0}{m \Delta t} (\Delta t)$$

$$v_0' = v_0 + \frac{P_0}{m}$$

$$\frac{dx}{dt} = v_0 + \frac{P_0}{m}$$

$$dx = \left(v_0 + \frac{P_0}{m} \right) dt$$

$$\int_{x_0}^x dx = \int_{t_0 + \Delta t}^t \left(v_0 + \frac{P_0}{m} \right) dt$$

$$x - x_0 = v_0 t - v_0(t_0 + \Delta t) + \frac{P_0}{m} t - \frac{P_0}{m} (t_0 + \Delta t) \quad x_0' = v_0(t_0 + \Delta t) + \frac{P_0}{2m \Delta t} (t_0 + \Delta t - t_0)^2$$

$$x - v_0(t_0 + \Delta t) - \frac{P_0}{2m} \Delta t = v_0 t - v_0(t_0 + \Delta t) + \frac{P_0}{m} t - \frac{P_0}{m} (t_0 + \Delta t) = v_0(t_0 + \Delta t) + \frac{P_0}{2m} \Delta t$$

$$x = v_0 t + \frac{P_0 \Delta t}{2m} + \frac{P_0}{m} t - \frac{P_0}{m} (t_0 + \Delta t)$$

$$x = v_0 t + \frac{P_0 \Delta t}{2m} + \frac{P_0}{m} t - \frac{P_0}{m} t_0 - \frac{P_0 \Delta t}{m}$$

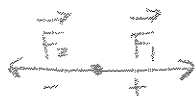
$$\boxed{x = v_0 t - \frac{P_0 \Delta t}{2m} + \frac{P_0}{m} (t - t_0)}$$

2-9

$$\sum F = Ma$$

$$M = \frac{(10)(160)}{32} = 50 \text{ slugs}$$

$$M \frac{d\vec{v}}{dt} = \vec{F}_1 + \vec{F}_2$$



$$\vec{F}_1 = 5\vec{F}_2 \quad \vec{F}_2 = -5\vec{F}_1, \quad F_1 = 200e^{-t/10}, \quad F_2 = 200e^{-t/20}$$

$$M \frac{dv}{dt} = 1000e^{-t/10} - 1000e^{-t/20}$$

$$dv = \frac{1000}{M} (e^{-t/10} - e^{-t/20}) dt$$

$$\int_0^v dv = \frac{1000}{M} \int_0^t (e^{-t/10} - e^{-t/20}) dt$$

$$v = \frac{1000}{M} \left[-10e^{-t/10} + 20e^{-t/20} \right] \Big|_0^t$$

$$= 20 \left[-10e^{-t/10} + 20e^{-t/20} - (-10 + 20) \right]$$

$$= 20 \left[20e^{-t/20} - 10e^{-t/10} - 10 \right]$$

$$\frac{dx}{dt} = 20 \left[20e^{-t/20} - 10e^{-t/10} - 10 \right]$$

$$\int_0^x dx = 20 \int_0^t \left[20e^{-t/20} - 10e^{-t/10} - 10 \right] dt$$

$$x = 20 \left[-400e^{-t/20} + 100e^{-t/10} - 10t \right] \Big|_0^t$$

$$= 200 \left[-40e^{-t/20} + 10e^{-t/10} - t \right] \Big|_0^t$$

$$= 200 \left[-40e^{-t/20} + 10e^{-t/20} - t - (-40 + 10) \right]$$

$$= 200 \left[10e^{-t/20} - 40e^{-t/20} - t + 30 \right]$$

$$x = -200t + 2000(1 - e^{-t/10})(3 - e^{-t/20})$$

$$v_{t \rightarrow \infty} = \frac{dx}{dt} \Big|_{t \rightarrow \infty} = -200 \text{ ft/s}$$

$v_{t \rightarrow \infty}$ is unreasonable because F is independent of v

$$10y^2 - 40y + 30 = 10(y^2 - 4y + 3)$$

$$y = e^{-t/20} \quad = 10(y-1)(y-3)$$

$$= 10(1-y)(3-y)$$

2-11

$$m \frac{dv}{dt} = -b e^{\alpha v}$$

$$\frac{dv}{e^{\alpha v}} = -\frac{b}{m} dt$$

$$e^{-\alpha v} dv = -\frac{b}{m} dt$$

$$\int_{v_0}^v e^{-\alpha v} dv = -\frac{b}{m} t$$

$$-\frac{1}{\alpha} e^{-\alpha v} \Big|_{v_0}^v = -\frac{b}{m} t$$

$$-\frac{1}{\alpha} [e^{-\alpha v} - e^{-\alpha v_0}] = -\frac{b}{m} t$$

$$e^{-\alpha v} - e^{-\alpha v_0} = \frac{\alpha b}{m} t$$

Time to stop, $v=0$

$$1 - e^{-\alpha v_0} = \frac{\alpha b}{m} t$$

$$\boxed{t_s = \frac{m(1 - e^{-\alpha v_0})}{\alpha b}}$$

$$e^{-\alpha v} = \frac{\alpha b}{m} t + e^{-\alpha v_0}$$

$$-\alpha v = \ln\left(\frac{\alpha b}{m} t + e^{-\alpha v_0}\right)$$

$$\frac{dx}{dt} = -\frac{1}{\alpha} \ln\left(\frac{\alpha b}{m} t + e^{-\alpha v_0}\right)$$

$$\int_0^x dx = -\frac{1}{\alpha} \int_0^t \ln\left(\frac{\alpha b}{m} t + e^{-\alpha v_0}\right) dt$$

$$x = -\frac{m}{\alpha^2 b} \left[\left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) \left(\ln\left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) - 1 \right) \right] \Big|_0^t$$

$$u = \frac{\alpha b}{m} t + e^{-\alpha v_0}$$

$$du = \frac{\alpha b}{m} dt$$

$$\frac{m}{\alpha b} du = dt$$

$$\begin{aligned} \int \ln\left(\frac{\alpha b}{m} t + e^{-\alpha v_0}\right) dt &= \frac{m}{\alpha b} \int \ln u du \\ &= \frac{m}{\alpha b} (u \ln u - u) \end{aligned}$$

$$X = \frac{-m}{\alpha^2 b} \left[\left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) \left(\ln \left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) - 1 \right) - \left(e^{-\alpha v_0} (-\alpha v_0 - 1) \right) \right]$$

$$= \frac{-m}{\alpha^2 b} \left[\left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) \left(\ln \left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) \right) - \frac{\alpha b}{m} t - e^{-\alpha v_0} + \alpha v_0 e^{-\alpha v_0} + e^{-\alpha v_0} \right]$$

$$X = \frac{-m}{\alpha^2 b} \left[\left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) \left(\ln \left(\frac{\alpha b}{m} t + e^{-\alpha v_0} \right) \right) - \frac{\alpha b}{m} t + \alpha v_0 e^{-\alpha v_0} \right]$$

$$X_s = \frac{m}{\alpha^2 b} \left[\frac{\alpha b}{m} t_s - \alpha v_0 e^{-\alpha v_0} - \left(\frac{\alpha b}{m} t_s + e^{-\alpha v_0} \right) \ln \left(\frac{\alpha b}{m} t_s + e^{-\alpha v_0} \right) \right]$$

$$\frac{\alpha b}{m} t_s = \frac{\alpha b}{m} \left[\frac{m(1 - e^{-\alpha v_0})}{\alpha b} \right]$$

$$= (1 - e^{-\alpha v_0})$$

$$X_s = \frac{m}{\alpha^2 b} \left[1 - e^{-\alpha v_0} - \alpha v_0 e^{-\alpha v_0} - (1 - e^{-\alpha v_0} + e^{-\alpha v_0}) \ln(1 - e^{-\alpha v_0} + e^{-\alpha v_0}) \right]$$

$$X_s = \frac{m}{\alpha^2 b} \left[1 - e^{-\alpha v_0} - \alpha v_0 e^{-\alpha v_0} \right]$$

2-13

$$m \frac{dv}{dt} = F_0 - bv^2 \quad x_0 = v_0 = 0 \text{ at } t_0 = 0$$

$$\frac{dv}{F_0 - bv^2} = \frac{dt}{m}$$

$$\int_0^v \frac{dv}{F_0 - bv^2} = \int_0^t \frac{dt}{m}$$

$$\int_0^v \frac{dv}{F_0 - bv^2} = \frac{t}{m}$$

$$v^2 = \frac{F_0}{b} \tanh^2 y$$

$$v = \sqrt{\frac{F_0}{b}} \tanh y \rightarrow y = \tanh^{-1}\left(v \sqrt{\frac{b}{F_0}}\right)$$

$$\int_0^y \frac{\sqrt{\frac{F_0}{b}} \operatorname{sech}^2 y \, dy}{F_0(1 - \tanh^2 y)} = \frac{t}{m}$$

$$dv = \sqrt{\frac{F_0}{b}} \operatorname{sech}^2 y \, dy$$

$$\frac{1}{\sqrt{F_0 b}} \int_0^y dy = \frac{t}{m} \quad \{1 - \tanh^2 y = \operatorname{sech}^2 y\}$$

$$\frac{1}{\sqrt{F_0 b}} \left[\tanh^{-1}\left(v \sqrt{\frac{b}{F_0}}\right) \right] = \frac{t}{m}$$

$$\tanh^{-1}\left(v \sqrt{\frac{b}{F_0}}\right) = \frac{t}{m} \sqrt{F_0 b}$$

$$v \sqrt{\frac{b}{F_0}} = \tanh\left(\frac{t}{m} \sqrt{F_0 b}\right)$$

$$v = \sqrt{\frac{F_0}{b}} \tanh\left(\frac{t}{m} \sqrt{F_0 b}\right)$$

$$2-15 \quad v_0=0, t_0=0, F=\frac{P}{v}-bv$$

$$m \frac{dv}{dt} = \frac{P}{v} - bv$$

$$= \frac{-bv^2 + P}{v}$$

$$\frac{v dv}{-bv^2 + P} = \frac{dt}{m}$$

$$\frac{v dv}{-v^2 + \frac{P}{b}} = \frac{b dt}{m}$$

$$\int_0^v \frac{v dv}{-v^2 + \frac{P}{b}} = \int_0^t \frac{b dt}{m}$$

$$-\frac{1}{2} \ln \left| -\frac{b}{P} v^2 + 1 \right| = \frac{b t}{m}$$

$$\ln \left| -\frac{b}{P} v^2 + 1 \right| = \frac{-2bt}{m}$$

$$-\frac{b}{P} v^2 + 1 = e^{\frac{-2bt}{m}}$$

$$-\frac{b}{P} v^2 = -1 + e^{\frac{-2bt}{m}}$$

$$\frac{b}{P} v^2 = 1 - e^{\frac{-2bt}{m}}$$

$$v^2 = \frac{P}{b} \left(1 - e^{\frac{-2bt}{m}} \right)$$

$$v = \sqrt{\frac{P}{b}} \left(1 - e^{\frac{-2bt}{m}} \right)^{1/2}$$

$$\text{let } u = -v^2 + \frac{P}{b}$$

$$du = -2v dv$$

$$\frac{-du}{2} = v dv \Rightarrow \int_0^v \frac{v dv}{-v^2 + \frac{P}{b}} = -\frac{1}{2} \int_{\frac{P}{b}}^{-v^2 + \frac{P}{b}} \frac{du}{u}$$

$$= -\frac{1}{2} \ln \left| \frac{-v^2 + \frac{P}{b}}{\frac{P}{b}} \right|$$

$$= -\frac{1}{2} \ln \left| -\frac{b}{P} v^2 + 1 \right|$$

2-17

$$F = (-)bv^n \quad (n \neq 1)$$

$$x_0 = 0$$

$$v(0) = v_0$$

$$m \ddot{x} = F$$

$$m \frac{dv}{dt} = F$$

$$m dv = -bv^n dt$$

$$\frac{dv}{v^n} = -\frac{b}{m} dt$$

$$\int \frac{dv}{v^n} = -\frac{b}{m} t \quad \{t_0 = 0\}$$

$$\int_{v_0}^{v} v'^{-n} dv' = -\frac{b}{m} t$$

$$\frac{v^{-n+1}}{-n+1} \Big|_{v_0}^v = -\frac{b}{m} t$$

$$\frac{v^{1-n}}{1-n} - \frac{v_0^{1-n}}{1-n} = -\frac{b}{m} t$$

$$v^{1-n} - v_0^{1-n} = -\frac{b}{m} t (1-n)$$

$$v^{1-n} = -\frac{b}{m} t (1-n) + v_0^{1-n}$$

$$(1-n) \ln v = \ln \left[-\frac{b}{m} t (1-n) + v_0^{1-n} \right]$$

$$\ln v = \frac{\ln \left[-\frac{b}{m} t (1-n) + v_0^{1-n} \right]}{1-n}$$

$$\ln v = \ln \left[-\frac{b}{m} t (1-n) + v_0^{1-n} \right]^{\frac{1}{1-n}}$$

$$v = \left[v_0^{1-n} - (1-n) \frac{b}{m} t \right]^{\frac{1}{1-n}}$$

$$dx = \left[v_0^{1-n} - (1-n) \frac{b}{m} t \right]^{\frac{1}{1-n}} dt$$

$$x = \int_0^t \left[v_0^{1-n} - (1-n) \frac{b}{m} t' \right]^{\frac{1}{1-n}} dt'$$

$$= \int_{u_0}^{u'} -\frac{u^{\frac{1}{1-n}}}{(1-n) \frac{b}{m}} du$$

$$= \frac{-m}{(1-n)b} \frac{u^{1+\frac{1}{1-n}}}{1+\frac{1}{1-n}} \Big|_{u_0}^{u'}$$

$$u = v_0^{1-n} - (1-n) \frac{b}{m} t'$$

$$du = -(1-n) \frac{b}{m} dt'$$

$$dt' = \frac{du}{-(1-n) \frac{b}{m}}$$

$$X = \frac{-m}{(1-n)b} \left[u^{\frac{2-n}{1-n}} \right]_{u_0}^{u'}$$

$$= \frac{-m}{(1-n)b} \frac{u^{\frac{2-n}{1-n}}}{\frac{2-n}{1-n}} \Big|_{u_0}^{u'}$$

$$= \frac{-m}{(2-n)b} u^{\frac{2-n}{1-n}} \Big|_{u_0}^{u'}$$

$$= \frac{-m}{(2-n)b} \left[v_0^{1-n} - (1-n) \frac{b}{m} t^{\frac{2-n}{1-n}} \right] \Big|_0^t$$

$$= \frac{-m}{(2-n)b} \left(\left[v_0^{1-n} - (1-n) \frac{b}{m} t^{\frac{2-n}{1-n}} \right] - \left[v_0^{1-n} \right] \right)$$

$$= \frac{-m}{(2-n)b} \left[-v_0^{2-n} + \left[v_0^{1-n} - (1-n) \frac{b}{m} t^{\frac{2-n}{1-n}} \right] \right]$$

$$X = \frac{m}{(2-n)b} \left[v_0^{2-n} - \left[v_0^{1-n} - (1-n) \frac{b}{m} t^{\frac{2-n}{1-n}} \right] \right]$$

Time to stop:

$$v=0$$

$$0 = \left[v_0^{1-n} - (1-n) \frac{b}{m} t_s^{\frac{2-n}{1-n}} \right]^{\frac{1}{1-n}}$$

$$(1-n) \frac{b}{m} t_s = v_0^{1-n}$$

$$t_s = v_0^{1-n} \frac{m}{b(1-n)} \quad , n > 1$$

Distance required to stop:

$$X_s = \frac{m}{(2-n)b} \left[v_0^{2-n} - \left[v_0^{1-n} - (1-n) \frac{b}{m} t_s^{\frac{2-n}{1-n}} \right] \right]$$

$$X_s = \frac{m}{(2-n)b} \left[v_0^{2-n} \right]$$

2-19

$$m \frac{dv}{dt} = \frac{K}{x^3}, \quad t_0=0, v_0=0$$

$$m \frac{dv}{dt} = F$$

$$\sqrt{\frac{m}{2}} \int_{x_0}^x [E - V(x)]^{-1/2} dx = t - t_0 \quad (2.46)$$

$$\sqrt{\frac{m}{2}} \int_{x_0}^x \left[\frac{K}{2} x_0^{-2} - \frac{K}{2} x^{-2} \right]^{-1/2} dx = t$$

$$\sqrt{\frac{m}{2}} \sqrt{\frac{2}{K}} \int_{x_0}^x [x_0^{-2} - x^{-2}]^{-1/2} dx = t$$

$$\sqrt{\frac{m}{K}} x_0 [x^2 - x_0^2]^{1/2} \Big|_{x_0}^x = t$$

$$\sqrt{\frac{m}{K}} x_0 (x^2 - x_0^2)^{1/2} = t$$

$$\frac{m}{K} x_0^2 (x^2 - x_0^2) = t^2$$

$$x^2 - x_0^2 = \frac{K t^2}{m x_0^2}$$

$$x^2 = \frac{K t^2}{m x_0^2} + x_0^2$$

$$x = \left[x_0^2 + \frac{K t^2}{m x_0^2} \right]^{1/2}$$

$$V(x) = - \int_{\infty}^x F dx$$

$$= -K \int_{\infty}^x x^{-3} dx$$

$$V(x) = \frac{K}{2} x^{-2}$$

$$E = T_0 + V(x_0)$$

$$= 0 + \frac{K}{2} x_0^{-2}$$

$$E = \frac{K}{2} x_0^{-2}$$

$$\int [x_0^{-2} - x^{-2}]^{-1/2} dx = \int \left[\frac{1}{x_0^2} - \frac{1}{x^2} \right]^{-1/2} dx$$

$$= \int \left[\frac{x^2 - x_0^2}{x_0^2 x^2} \right]^{-1/2} dx$$

$$= x_0 \int \frac{x dx}{(x^2 - x_0^2)^{1/2}}$$

$$\text{Let } u = x^2 - x_0^2$$

$$du = 2x dx$$

$$\frac{du}{2} = x dx$$

$$= \frac{x_0}{2} \int u^{-1/2} du$$

$$= \frac{x_0}{2} \frac{2}{1} u^{1/2} + C$$

$$= x_0 (x^2 - x_0^2)^{1/2} + C$$

2-21

$$V = ax^2 - bx^3$$

$$\frac{1}{2}mv^2 + V(x) = \frac{1}{2}mV_0^2 + V(x_0)$$

$$= E$$

$$V^2 = \frac{2}{m}(E - V(x))$$

$$E = \frac{1}{2}mV_0^2 + V(0)$$

$$E = \frac{1}{2}mV_0^2$$

a) Find F

$$F = -\frac{dV}{dx}$$

$$= -\frac{d}{dx}(ax^2 - bx^3)$$

$$\boxed{F = -2ax + 3bx^2}$$

b) Find V_c , $x_0 = 0$

$F = 0$ { where $V(x)$ is a maximum }

$$-2ax + 3bx^2 = 0$$

$$x(3bx - 2a) = 0$$

$$x = 0, 3bx - 2a = 0$$

$$x_c = \frac{2a}{3b}$$

$$V^2 = \frac{2}{m}(E - V(x))$$

$$= \frac{2}{m}\left(\frac{1}{2}mV_0^2 - ax^2 + bx^3\right)$$

$$0 = \frac{2}{m}\left(\frac{1}{2}mV_c^2 - ax_c^2 + bx_c^3\right)$$

$$= V_c^2 - \frac{2}{m}ax_c^2 + \frac{2}{m}bx_c^3$$

$$V_c^2 = \frac{2}{m}(ax_c^2 - bx_c^3)$$

$$= \frac{2}{m}\left(a\left(\frac{2a}{3b}\right)^2 - b\left(\frac{2a}{3b}\right)^3\right)$$

$$= \frac{2}{m}\left[\frac{4a^3}{9b^2} - \frac{8a^3}{27b^2}\right]$$

$$= \frac{2}{m}\left[\frac{12a^3}{27b^2} - \frac{8a^3}{27b^2}\right]$$

$$\boxed{V_c^2 = \frac{8a^3}{27b^2m}}$$

2-23

$$F = -kx + ax^{-3}$$

a) Find $V(x)$ and $x(t)$

$$\begin{aligned} V(x) &= -\int F dx \\ &= -\int -kx dx - \int ax^{-3} dx \\ &= \frac{k}{2}x^2 + \frac{a}{2}x^{-2} \end{aligned}$$

$$V(x) = \frac{1}{2}(kx^2 + ax^{-2})$$

$$\sqrt{\frac{m}{2}} \int_{x_0}^x [E - V(x)]^{-\frac{1}{2}} dx = t, \quad t_0 = 0$$

$$\sqrt{\frac{m}{2}} \int_{x_0}^x \left[E - \frac{1}{2}(kx^2 + ax^{-2}) \right]^{-\frac{1}{2}} dx = t$$

$$\sqrt{\frac{m}{2}} \sqrt{2} \int_{x_0}^x [2E - (kx^2 + ax^{-2})]^{-\frac{1}{2}} dx =$$

$$\sqrt{m} \int_{x_0}^x \left[2E - kx^2 - \frac{a}{x^2} \right]^{-\frac{1}{2}} dx =$$

$$\sqrt{m} \int_{x_0}^x \left[2E - \frac{kx^4 - a}{x^2} \right]^{-\frac{1}{2}} dx =$$

$$\sqrt{m} \int_{x_0}^x \left[\frac{2Ex^2 - kx^4 - a}{x^2} \right]^{-\frac{1}{2}} dx =$$

$$\sqrt{m} \int_{x_0}^x \frac{x dx}{(2Ex^2 - kx^4 - a)^{\frac{1}{2}}} = t$$

$$-kx^4 + 2Ex^2 - a = -k \left(x^4 - \frac{2E}{k}x^2 + \frac{a}{k} \right)$$

$$= -k \left(x^4 - \frac{2E}{k}x^2 + \frac{E^2}{k^2} + \frac{a}{k} - \frac{E^2}{k^2} \right)$$

$$= -k \left[\left(x^2 - \frac{E}{k} \right)^2 - \left(\frac{E^2}{k^2} - \frac{a}{k} \right) \right]$$

$$= k \left[\frac{E^2 - ak}{k^2} - \left(x^2 - \frac{E}{k} \right)^2 \right]$$

$$\sqrt{m} \int_{x_0}^x \frac{x dx}{\left[K \left(\frac{E^2 - ak}{K^2} - \left(x^2 - \frac{E}{K} \right)^2 \right)^{1/2} \right]} = t$$

$$\sqrt{\frac{m}{K}} \int_{x_0}^x \frac{x dx}{\left[\frac{E^2 - ak}{K^2} - \left(x^2 - \frac{E}{K} \right)^2 \right]^{1/2}} = t$$

$$\frac{1}{2} \sqrt{\frac{m}{K}} (\theta - \theta_0) = t$$

$$\theta = 2t \sqrt{\frac{K}{m}} + \theta_0$$

$$x^2 = \frac{E}{K} + \frac{\sqrt{E^2 - ak}}{K} \sin \theta$$

$$x^2 = \frac{E}{K} + \frac{\sqrt{E^2 - ak}}{K} \sin \left[2t \sqrt{\frac{K}{m}} + \theta_0 \right]$$

$$\sqrt{\frac{m}{K}} \int_{x_0}^x \frac{x dx}{\left[\frac{E^2 - ak}{K^2} - \left(x^2 - \frac{E}{K} \right)^2 \right]^{1/2}}$$

$$\text{let } x^2 - \frac{E}{K} = \frac{\sqrt{E^2 - ak}}{K} \sin \theta$$

$$2x dx = \frac{\sqrt{E^2 - ak}}{K} \cos \theta d\theta$$

$$\frac{1}{2} \sqrt{\frac{m}{K}} \int_{\theta_0}^{\theta} \frac{\frac{\sqrt{E^2 - ak}}{K} \cos \theta d\theta}{\left[\frac{E^2 - ak}{K^2} - \frac{E^2 - ak}{K^2} \sin^2 \theta \right]^{1/2}} =$$

$$\frac{1}{2} \sqrt{\frac{m}{K}} \int_{\theta_0}^{\theta} \frac{\cos \theta d\theta}{(1 - \sin^2 \theta)^{1/2}} =$$

$$\frac{1}{2} \sqrt{\frac{m}{K}} \int_{\theta_0}^{\theta} d\theta = \frac{1}{2} \sqrt{\frac{m}{K}} (\theta - \theta_0)$$

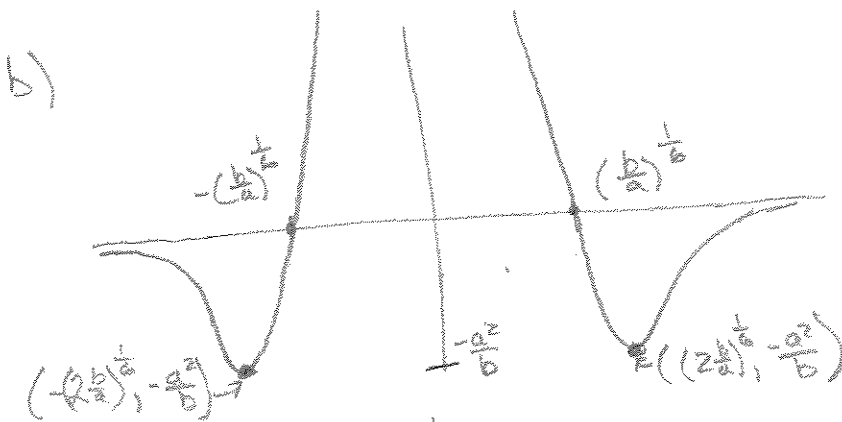
2-25

$$V(x) = -\frac{a}{x^6} + \frac{b}{x^{12}}$$

$$a) F = -\frac{dV}{dx}$$

$$= -\frac{d}{dx}(-ax^{-6} + bx^{-12})$$

$$F = -6ax^{-7} + 12bx^{-13}$$



Zeros: $0 = -\frac{a}{x^6} + \frac{b}{x^{12}}$

$$\frac{a}{x^6} = \frac{b}{x^{12}}$$

$$\frac{x^6}{a} = \frac{x^{12}}{b}$$

$$\frac{x^{12}}{b} - \frac{x^6}{a} = 0$$

$$x^6 \left(\frac{x^6}{b} - \frac{1}{a} \right) = 0$$

$$\frac{x^6}{b} - \frac{1}{a} = 0$$

$$\frac{x^6}{b} = \frac{1}{a}$$

$$x^6 = \frac{b}{a}$$

$$x = \pm \sqrt[6]{\frac{b}{a}}$$

max, min

$$0 = -6ax^{-7} + 12bx^{-13}$$

$$6ax^{-7} = 12bx^{-13}$$

$$\frac{6a}{x^7} = \frac{12b}{x^{13}}$$

$$\frac{x^7}{6a} = \frac{x^{13}}{12b}$$

$$\frac{x^{13}}{12b} - \frac{x^7}{6a} = 0$$

$$x^7 \left(\frac{x^6}{12b} - \frac{1}{6a} \right) = 0$$

$$\frac{x^6}{12b} = \frac{1}{6a}$$

$$x^6 = 2\frac{b}{a}$$

$$x = \pm \sqrt[6]{2\frac{b}{a}}$$

$$\begin{aligned} V\left(\pm \sqrt[6]{2\frac{b}{a}}\right) &= -\frac{a}{2\frac{b}{a}} + \frac{b}{4\frac{b^2}{a^2}} \\ &= -\frac{a^2}{2b} + \frac{a^2}{4b} \\ &= \frac{-2a^2 + a^2}{4b} \\ &= -\frac{a^2}{4b} \end{aligned}$$

c) From b) equilibrium distance is

$$x_{eq} = \pm \left(\frac{2b}{a}\right)^{1/6}$$

To determine period of small oscillations about x_{eq}

$$V(x) = V(x_{eq}) + \left(\frac{dV}{dx}\right)_{x_{eq}} (x - x_{eq}) + \frac{1}{2} \left(\frac{d^2V}{dx^2}\right)_{x_{eq}} (x - x_{eq})^2 + \frac{1}{6} \left(\frac{d^3V}{dx^3}\right)_{x_{eq}} (x - x_{eq})^3 + \dots$$

{Taylor expansion about x_{eq} }

$\left(\frac{dV}{dx}\right)_{x_{eq}} = 0$, can drop $V(x_{eq})$ without affecting physical results,

$$V(x) = \frac{1}{2} \left(\frac{d^2V}{dx^2}\right)_{x_{eq}} (x - x_{eq})^2$$

Letting $\left(\frac{d^2V}{dx^2}\right)_{x_{eq}} = k$ and $x' = x - x_{eq}$

$V(x') = \frac{1}{2} k x'^2 + \dots$, since $x - x_{eq} \ll 1$, higher terms can be ignored.

So, $\omega = \sqrt{\frac{k}{m}}$.

$$\begin{aligned} k &= \frac{d^2}{dx^2} \left(-\frac{a}{x^6} + \frac{b}{x^{12}} \right)_{x_{eq}} \\ &= \frac{d}{dx} \left(6ax^{-7} - 12bx^{-13} \right)_{x_{eq}} \\ &= \left(-42ax^{-8} + 156bx^{-14} \right)_{x_{eq}} = \left(\frac{2b}{a} \right)^{1/6} \\ &= -42a \left(\frac{2b}{a} \right)^{-4/3} + 156b \left(\frac{2b}{a} \right)^{-7/3} \\ &= -42a \left(\frac{a}{2b} \right)^{4/3} + 156b \left(\frac{a}{2b} \right)^{7/3} \\ &= -42 \frac{a^2}{2b} \left(\frac{a}{2b} \right)^{1/3} + 156 \frac{a^2}{4b} \left(\frac{a}{2b} \right)^{1/3} \\ &= -21 \frac{a^2}{b} \left(\frac{a}{2b} \right)^{1/3} + 39 \frac{a^2}{b} \left(\frac{a}{2b} \right)^{1/3} \\ &= 18 \frac{a^2}{b} \left(\frac{a}{2b} \right)^{1/3} \end{aligned}$$

$$\omega = \sqrt{\frac{k}{m}}$$

$$2\pi f = \sqrt{\frac{k}{m}}$$

$$\frac{1}{2\pi f} = \sqrt{\frac{m}{k}}$$

$$T = \frac{1}{f} = 2\pi \sqrt{\frac{m}{k}}$$

$$T = 2\pi \left(\frac{m}{18 \frac{a^2}{b} \left(\frac{a}{2b} \right)^{1/3}} \right)^{1/2}$$

$$= 2\pi \frac{m^{1/2}}{18^{1/2} \left(\frac{a^2}{b} \right)^{1/2} \left(\frac{a}{2b} \right)^{1/6}}$$

$$= \frac{2\pi}{3} \left[\frac{m^{1/2}}{2^{1/2} \left(\frac{a^2}{b} \right)^{1/2} \left(\frac{a}{2b} \right)^{1/6}} \right]$$

$$= \frac{2\pi}{3} \left[\frac{m^{3/6}}{2^{3/6} \left(\frac{a^2}{b} \right)^{3/6} \left(\frac{a}{2b} \right)^{1/6}} \right]$$

$$T = \frac{2\pi}{3} \left[\frac{m^{3/4} b}{4a^7} \right]^{1/6}$$

$$2-27 \quad V(x) = \frac{-V_0 a^2 (a^2 + x^2)}{8a^4 + x^4}$$

$$a) \quad F = -\frac{dV}{dx}$$

$$= -\frac{d}{dx} \left(\frac{-V_0 a^4 - V_0 a^2 x^2}{8a^4 + x^4} \right)$$

$$= \frac{d}{dx} \left(\frac{V_0 a^4 + V_0 a^2 x^2}{8a^4 + x^4} \right)$$

$$F = \frac{(8a^4 + x^4)(2V_0 a^2 x) - (V_0 a^4 + V_0 a^2 x^2)(4x^3)}{(8a^4 + x^4)^2}$$

$$\text{max and min of } V(x) \rightarrow \frac{dV}{dx} = 0$$

$$0 = \frac{d}{dx} \left(\frac{-V_0 a^2 (a^2 + x^2)}{8a^4 + x^4} \right)$$

$$= -V_0 a^2 \frac{d}{dx} \left(\frac{a^2 + x^2}{8a^4 + x^4} \right)$$

$$= \frac{(8a^4 + x^4)2x - (a^2 + x^2)4x^3}{(8a^4 + x^4)^2}$$

$$= \frac{16a^4 x + 2x^5 - 4a^2 x^3 - 4x^5}{(8a^4 + x^4)^2}$$

$$= \frac{-2x^5 - 4a^2 x^3 + 16a^4 x}{(8a^4 + x^4)^2}$$

$$= \frac{x^5 + 2a^2 x^3 - 8a^4 x}{(8a^4 + x^4)^2}$$

$$= \frac{x(x^4 + 2a^2 x^2 - 8a^4)}{(8a^4 + x^4)^2}$$

$$\boxed{x=0}, \quad x^4 + 2a^2 x^2 - 8a^4 = 0$$

$$y^2 + 2a^2 y - 8a^4 = 0$$

$$y^2 + 2a^2 y + a^4 = 8a^4 + a^4$$

$$(y + a^2)^2 = 9a^4$$

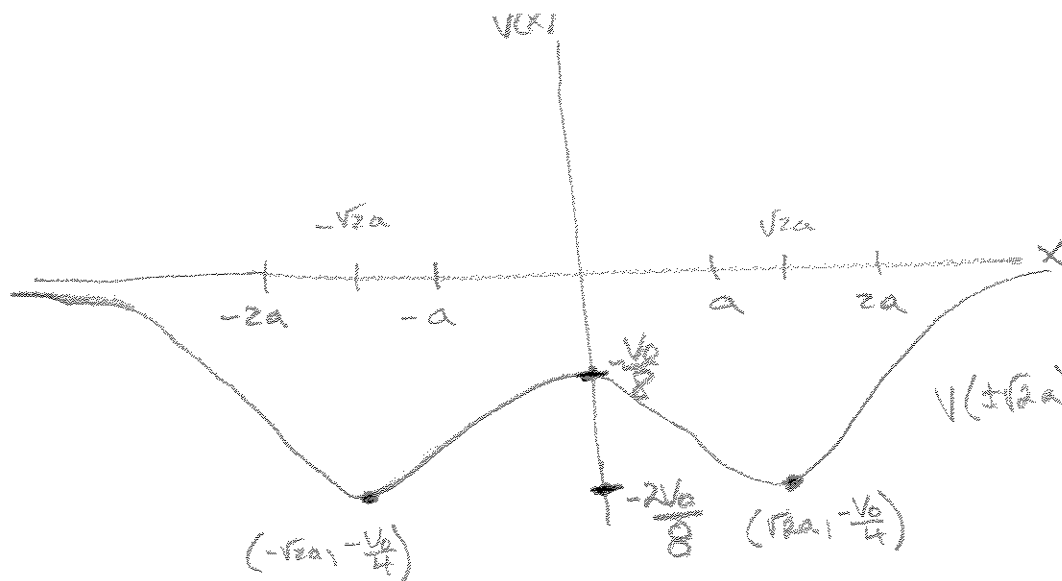
$$y + a^2 = \pm 3a^2$$

$$y = -4a^2 \text{ or } 2a^2$$

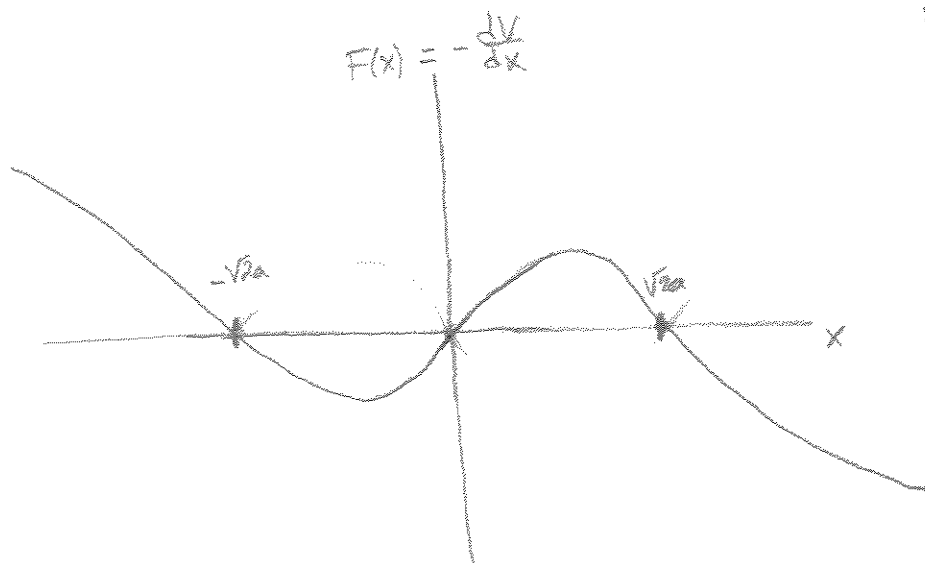
$$y = x^2$$

$$x^2 = -4a^2 \text{ or } 2a^2$$

$$\boxed{x = \pm \sqrt{2}a}$$



$$\begin{aligned}
 V(\pm\sqrt{2}a) &= \frac{-V_0 a^2 (a^2 + 2a^2)}{8a^4 + 4a^4} \\
 &= \frac{-V_0 a^2 (3a^2)}{12a^4} \\
 &= -\frac{3V_0 a^4}{12a^4} \\
 &= -\frac{3V_0}{12} \\
 &= -\frac{V_0}{4}
 \end{aligned}$$



b) $-\frac{V_0}{4} < V(x) < -\frac{V_0}{8}$ is oscillatory about $x_{eq} = \pm\sqrt{2}a$

$-\frac{V_0}{8} < V(x) < 0$ is oscillatory about $x=0$

Small oscillations are about $x_{eq} = \pm\sqrt{2}a$

$$\begin{aligned}
 V(x) &= V(x_{eq}) + \left(\frac{dV}{dx}\right)_{x_{eq}}(x-x_{eq}) + \frac{1}{2}\left(\frac{d^2V}{dx^2}\right)_{x_{eq}}(x-x_{eq})^2 + \frac{1}{6}\left(\frac{d^3V}{dx^3}\right)_{x_{eq}}(x-x_{eq})^3 + \dots \\
 &= \frac{1}{2}\left(\frac{d^2V}{dx^2}\right)_{x_{eq}}(x-x_{eq})^2 + \dots
 \end{aligned}$$

$$K = \left(\frac{d^2V}{dx^2}\right)_{x_{eq}}$$

$$\frac{dV}{dx} = -V_0 a^2 \frac{d}{dx} \left(\frac{a^2 + x^2}{8a^4 + x^4} \right)$$

$$\frac{dV}{dx} = -V_0 a^2 \left[\frac{(8a^4 + x^4) 2x - (a^2 + x^2) 4x^3}{(8a^4 + x^4)^2} \right]$$

$$= -V_0 a^2 \left[\frac{16a^4 x + 2x^5 - 4a^2 x^3 - 4x^5}{(8a^4 + x^4)^2} \right]$$

$$= -V_0 a^2 \left[\frac{-2x^5 - 4a^2 x^3 + 16a^4 x}{(8a^4 + x^4)^2} \right]$$

$$\frac{d^2 V}{dx^2} = -V_0 a^2 \left[\frac{(8a^4 + x^4)^2 (-10x^4 - 12a^2 x^2 + 16a^4) - (-2x^5 - 4a^2 x^3 + 16a^4 x) 2(8a^4 + x^4) 4x^3}{(8a^4 + x^4)^4} \right]$$

$$= -V_0 a^2 (8a^4 + x^4) \left[\frac{(8a^4 + x^4) (-10x^4 - 12a^2 x^2 + 16a^4) - 8x^3 (-2x^5 - 4a^2 x^3 + 16a^4 x)}{(8a^4 + x^4)^4} \right]$$

$$= -V_0 a^2 \left[\frac{(8a^4 + x^4) (-10x^4 - 12a^2 x^2 + 16a^4) + 16x^4 (x^4 + 2a^2 x^2 - 8a^4)}{(8a^4 + x^4)^3} \right]$$

$$K = \left(\frac{d^2 V}{dx^2} \right)_{x_{eq}} = -V_0 a^2 \left[\frac{(8a^4 + 4a^4) (-10(4a^4) - 12a^2(2a^2) + 16a^4) + 16x^4 (4a^4 + 2a^2(2a^2) - 8a^4)}{(8a^4 + 4a^4)^3} \right]$$

$$x_{eq} = \pm \sqrt{2} a$$

$$= -V_0 a^2 \left[\frac{-40a^4 - 24a^4 + 16a^4}{(12a^4)^2} \right]$$

$$= -V_0 a^2 \left[\frac{-48a^4}{144a^8} \right]$$

$$= V_0 a^2 \left[\frac{a^4}{3a^8} \right]$$

$$K = \frac{V_0}{3a^2}$$

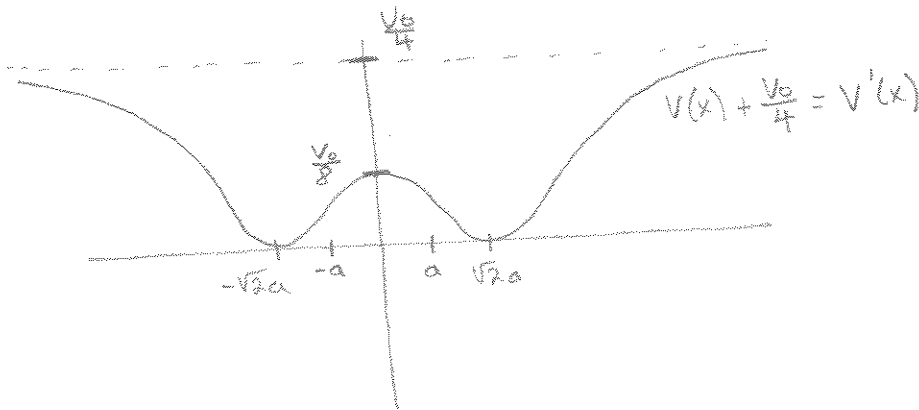
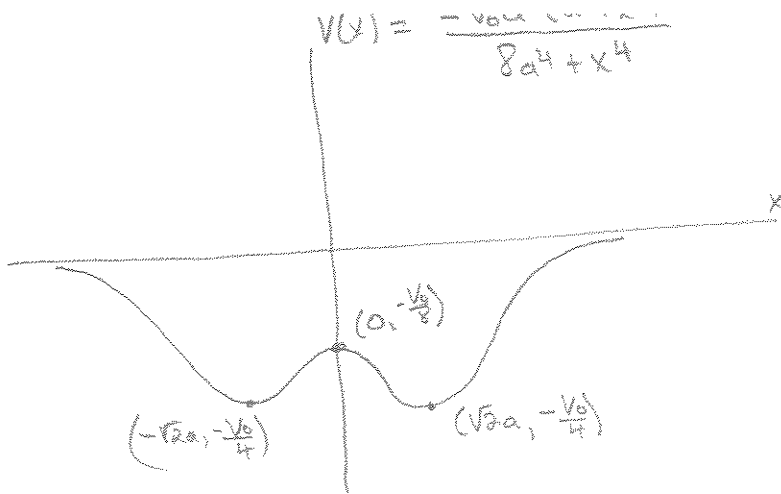
$$\omega = \sqrt{\frac{K}{m}}$$

$$2\pi f = \sqrt{\frac{K}{m}}$$

$$f = \frac{\left(\frac{V_0}{3a^2 m} \right)^{1/2}}{2\pi}$$

$$f = \left(\frac{V_0}{12\pi^2 a^2 m} \right)^{1/2}$$

c)



$$E = \frac{1}{2} m v_0^2 + V(x \gg 0) + \frac{V_0}{4}$$

$$= \frac{1}{2} m v_0^2 + 0 + \frac{V_0}{4}$$

$$E = \frac{1}{2} m v_0^2 + \frac{V_0}{4}$$

$$V'(a) = V(a) + \frac{V_0}{4}$$

$$= \frac{-V_0 a^2 (a^2 + a^2)}{8a^4 + a^4} + \frac{V_0}{4}$$

$$= -\frac{2V_0 a^4}{9a^4} + \frac{V_0}{4}$$

$$= -\frac{2V_0}{9} + \frac{V_0}{4} = -\frac{8V_0}{36} + \frac{9V_0}{36} = \frac{V_0}{36}$$

$$E = T_a + V'(a)$$

$$\frac{1}{2} m v_0^2 + \frac{V_0}{4} = T_a + V'(a)$$

$$\frac{1}{2} m v_0^2 + \frac{V_0}{4} - V(a) = T_a$$

$$\frac{1}{2} m v_0^2 + \frac{V_0}{4} - \left(\frac{V_0}{36}\right) = T_a$$

$$\frac{1}{2} m v_0^2 + \frac{9V_0}{36} - \frac{V_0}{36} = T_a$$

$$\frac{1}{2} m v_0^2 + \frac{8V_0}{36} = T_a$$

$$\frac{1}{2} m v_0^2 + \frac{2V_0}{9} = T_a$$

$$\alpha > \frac{T_0}{T_a} \quad \left\{ \alpha T_a > T_0, \alpha T_a = \text{kinetic energy removed by collision} \right\}$$

$$\alpha > \frac{\frac{1}{2} m v_0^2}{\frac{1}{2} m v_0^2 + \frac{2V_0}{9}}$$

$$\frac{1}{\alpha} < \frac{\frac{1}{2} m v_0^2 + \frac{2V_0}{9}}{\frac{1}{2} m v_0^2}$$

$$< 1 + \frac{4V_0}{9 m v_0^2}$$

$$\alpha > \left[1 + \frac{4V_0}{9 m v_0^2} \right]^{-1}$$

remains in well

Trapped in one side of well

$$T_a = \frac{1}{2} m v_0^2 + \frac{2V_0}{9}$$

Energy must be reduced by

$$\frac{V_0}{4} - \frac{V_0}{8} = \frac{V_0}{8}$$

to be trapped in one side of well

$$\begin{aligned} T_a &= \frac{1}{2} m v_0^2 + \frac{2V_0}{9} - \frac{V_0}{8} \\ &= \frac{1}{2} m v_0^2 + \frac{16V_0}{72} - \frac{9V_0}{72} \end{aligned}$$

$$T_a = \frac{1}{2} m v_0^2 + \frac{7V_0}{72}$$

$$\alpha T_a > T_0$$

$$\alpha > \frac{T_0}{T_a}$$

$$\frac{1}{\alpha} < \frac{T_a}{T_0} = \frac{\frac{1}{2} m v_0^2 + \frac{7V_0}{72}}{\frac{1}{2} m v_0^2}$$

$$\frac{1}{\alpha} < 1 + \frac{7V_0}{36 m v_0^2}$$

$$\alpha > \left[1 + \frac{7V_0}{36 m v_0^2} \right]^{-1}$$

Turning points when $\alpha = 1$

$\alpha = 1 \rightarrow 100\%$ loss of kinetic energy

$$E = V(a) = \frac{V_0}{36}$$

$$\frac{V_0}{36} = V(a) + \frac{V_0}{4}$$

$$\frac{V_0}{36} - \frac{9V_0}{36} = \frac{-V_0 a^2 (a^2 + x^2)}{8a^4 + x^4}$$

$$\frac{8}{36} = \frac{a^2 (a^2 + x^2)}{8a^4 + x^4}$$

$$2 \cdot (8a^4 + x^4) = 9a^2(a^2 + x^2)$$

$$2x^4 + 16a^4 - 9a^4 - 9a^2x^2 = 0$$

$$2x^4 - 9a^2x^2 + 7a^4 = 0 \quad y = x^2$$

$$2y^2 - 9a^2y + 7a^4 = 0$$

$$y = \frac{9a^2 \pm \sqrt{81a^4 - 4(2)(7a^4)}}{4}$$

$$= \frac{9a^2 \pm \sqrt{25a^4}}{4}$$

$$= \frac{9a^2 \pm 5a^2}{4}$$

$$= a^2 \text{ or } \frac{7}{2}a^2$$

$$x = \pm a \text{ or } \pm \left(\frac{7}{2}\right)^{1/2} a$$

$$\boxed{x = a, \left(\frac{7}{2}\right)^{1/2} a}$$

2-29 Derive Eq. 2.74 and 2.75, $x_0 = v_0 = 0$ at $t_0 = 0$

$$F = bv^2$$

$$m \frac{dv}{dt} = -mg + bv^2$$

$$\frac{m}{b} \frac{dv}{dt} = -\frac{mg}{b} + v^2$$

$$\frac{dv}{-\frac{mg}{b} + v^2} = \frac{b}{m} dt$$

$$\int_0^v \frac{dv}{-\frac{mg}{b} + v^2} = \frac{b}{m} t$$

$$-\int_0^v \frac{dv}{\frac{mg}{b} - v^2} = \frac{b}{m} t$$

$$-\sqrt{\frac{b}{mg}} \tanh^{-1}\left(\sqrt{\frac{b}{mg}} v\right) = \frac{b}{m} t$$

$$\tanh^{-1}\left(\sqrt{\frac{b}{mg}} v\right) = -\sqrt{\frac{bg}{m}} t$$

$$v = \sqrt{\frac{mg}{b}} \tanh\left(-\sqrt{\frac{bg}{m}} t\right)$$

$$\boxed{v = -\sqrt{\frac{mg}{b}} \tanh\left(\sqrt{\frac{bg}{m}} t\right) \text{ \{odd function\}}}$$

$$\frac{dx}{dt} = -\sqrt{\frac{mg}{b}} \tanh\left(\sqrt{\frac{bg}{m}} t\right)$$

$$x = \int_0^t -\sqrt{\frac{mg}{b}} \tanh\left(\sqrt{\frac{bg}{m}} t\right) dt$$

$$\boxed{x = -\frac{m}{b} \ln\left[\cosh\left(\sqrt{\frac{bg}{m}} t\right)\right] \text{ \{cosh } x \geq 1\}}}$$

Expansions for large and small t
on next page.

$$1 - \tanh^2 y = \operatorname{sech}^2 y$$

$$v^2 = \frac{mg}{b} \tanh^2 y$$

$$v = \sqrt{\frac{mg}{b}} \tanh y$$

$$dv = \sqrt{\frac{mg}{b}} \operatorname{sech}^2 y dy$$

$$\left\{ \frac{dv}{\frac{mg}{b} - v^2} = -\sqrt{\frac{mg}{b}} \int \frac{\operatorname{sech}^2 y dy}{\frac{mg}{b} - \frac{mg}{b} \tanh^2 y} \right.$$

$$= -\sqrt{\frac{mg}{b}} \frac{b}{mg} \int \frac{\operatorname{sech}^2 y dy}{1 - \tanh^2 y}$$

$$= -\sqrt{\frac{b}{mg}} \int \frac{\operatorname{sech}^2 y dy}{\operatorname{sech}^2 y} \quad 1 - \tanh^2 y = \operatorname{sech}^2 y$$

$$= -\sqrt{\frac{b}{mg}} y + C$$

$$= -\sqrt{\frac{b}{mg}} \tanh^{-1}\left(\sqrt{\frac{b}{mg}} v\right) + C$$

$$-\sqrt{\frac{mg}{b}} \int \tanh\left(\sqrt{\frac{bg}{m}} t\right) dt = -\frac{m}{b} \int \tanh(u) du$$

$$u = \sqrt{\frac{bg}{m}} t$$

$$du = \sqrt{\frac{bg}{m}} dt$$

$$\sqrt{\frac{m}{bg}} du = dt$$

$$= -\frac{m}{b} \int \frac{\sinh u du}{\cosh u}$$

$$z = \cosh u$$

$$dz = \sinh u du$$

$$= -\frac{m}{b} \int \frac{du}{u}$$

$$= -\frac{m}{b} \ln|u| + C$$

$$V = -\sqrt{\frac{mg}{b}} \tanh\left(\sqrt{\frac{bg}{m}} t\right)$$

$$\tanh z = z - \frac{z^3}{3} + \frac{2z^5}{15} - \dots$$

$$V \doteq -\sqrt{\frac{mg}{b}} \left(\sqrt{\frac{bg}{m}} t - \frac{\left(\frac{bg}{m}\right)^{\frac{3}{2}} t^3}{3} + \dots \right)$$

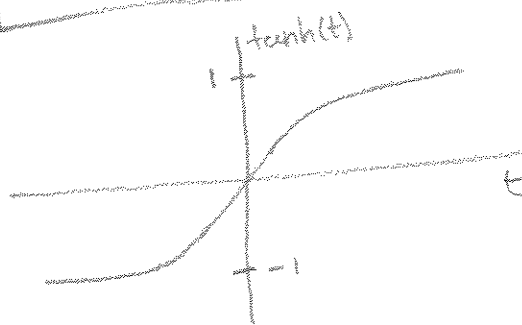
$$\text{if } t \ll \sqrt{\frac{m}{bg}}$$

$$V \doteq -\sqrt{\frac{mg}{b}} \left(\sqrt{\frac{bg}{m}} t \right)$$

$$V \doteq -gt$$

$$\text{if } t \gg \sqrt{\frac{m}{bg}}$$

$$V \doteq -\sqrt{\frac{mg}{b}} (1) \quad \{ \tanh(t) \rightarrow 1$$



$$x = -\frac{m}{b} \ln \cosh\left(\sqrt{\frac{bg}{m}} t\right)$$

$$\cosh(z) = 1 + \frac{z^2}{2!} + \frac{z^4}{4!} + \dots$$

$$\ln(x) = (x-1) - \frac{(x-1)^2}{2} + \frac{(x-1)^3}{3} - \dots \quad |x| \leq 1$$

$$\text{if } t \ll \sqrt{\frac{m}{bg}}$$

$$x \doteq -\frac{m}{b} \ln\left(1 + \frac{bg}{2m} t^2\right)$$

$$x \doteq -\frac{m}{b} \left(\frac{bg}{2m} t^2 \right)$$

$$x \doteq -\frac{1}{2} g t^2$$

$$\text{if } t \gg \sqrt{\frac{m}{bg}}$$

$$\cosh z = \frac{1}{2}(e^z + e^{-z})$$

$$\cosh z \approx \frac{1}{2} e^z \quad z \gg 1$$

$$x \doteq -\frac{m}{b} \ln\left(\frac{e^{\sqrt{\frac{bg}{m}} t}}{2}\right)$$

$$\doteq -\frac{m}{b} \left[\sqrt{\frac{bg}{m}} t - \ln 2 \right]$$

$$x = \frac{m}{b} \ln 2 - \sqrt{\frac{mg}{b}} t$$

2-31

i) Object starting at $x_0=0$ and reaching max height

$$v(0) = v_0 \quad v_f = 0 \quad t_0 = 0 \quad t_f = t_0$$

$$m \frac{dv}{dt} = -mg - bv^2$$

$$-\frac{m}{b} \frac{dv}{dt} = \frac{mg}{b} + v^2$$

$$\frac{dv}{\frac{mg}{b} + v^2} = -\frac{b}{m} dt$$

$$\int_{v_0}^0 \frac{dv}{\frac{mg}{b} + v^2} = \int_0^{t_0} -\frac{b}{m} dt$$

$$\sqrt{\frac{b}{mg}} \tan^{-1}\left(\sqrt{\frac{b}{mg}} v\right) \Big|_{v_0}^0 = -\frac{b}{m} t \Big|_0^{t_0}$$

$$-\sqrt{\frac{b}{mg}} \tan^{-1}\left(\sqrt{\frac{b}{mg}} v_0\right) = -\frac{b}{m} t_0$$

$$\sqrt{\frac{m}{bg}} \tan^{-1}\left(\sqrt{\frac{b}{mg}} v_0\right) = t_0 \quad \{ \text{time for max } x \}$$

$$\sqrt{\frac{m}{bg}} \tan^{-1}\left(\sqrt{\frac{b}{mg}} v\right) = t_0 - t \quad \{ 0 < t < t_0 \}$$

$$v = \sqrt{\frac{mg}{b}} \tan\left(\sqrt{\frac{bg}{m}}(t_0 - t)\right)$$

$$\int_0^x dx = \int_0^t \sqrt{\frac{mg}{b}} \tan\left(\sqrt{\frac{bg}{m}}(t_0 - t)\right) dt$$

$$x = \frac{m}{b} \ln \cos\left(\sqrt{\frac{bg}{m}}(t_0 - t)\right) \Big|_0^t$$

$$= \frac{m}{b} \left[\ln \cos\left(\sqrt{\frac{bg}{m}}(t_0 - t)\right) - \ln \cos\left(\sqrt{\frac{bg}{m}} t_0\right) \right]$$

$$= \frac{m}{b} \left[-\ln\left(\sqrt{1 + \frac{bv_0^2}{mg}}\right) + \ln \cos\left(\sqrt{\frac{bg}{m}}(t_0 - t)\right) \right]$$

$$x = \frac{m}{2b} \left[\ln\left(1 + \frac{bv_0^2}{mg}\right) + 2 \ln \cos\left(\sqrt{\frac{bg}{m}}(t_0 - t)\right) \right]$$

$$\int \frac{dv}{\frac{mg}{b} + v^2} = \sqrt{\frac{mg}{b}} \int \frac{\sec^2 \theta d\theta}{\frac{mg}{b} + \frac{mg}{b} \tan^2 \theta} \quad v^2 = \frac{mg}{b} \tan^2 \theta$$

$$= \sqrt{\frac{b}{mg}} \int \frac{\sec^2 \theta d\theta}{1 + \tan^2 \theta} \quad v = \sqrt{\frac{mg}{b}} \tan \theta$$

$$= \sqrt{\frac{b}{mg}} \theta + C$$

$$= \sqrt{\frac{b}{mg}} \tan^{-1}\left(\sqrt{\frac{b}{mg}} v\right) + C$$

$$dv = \sqrt{\frac{mg}{b}} \sec^2 \theta d\theta$$

$$\sqrt{\frac{mg}{b}} \int \tan\left(\sqrt{\frac{bg}{m}}(t_0 - t)\right) dt = -\frac{m}{b} \int \tan u du$$

$$u = \sqrt{\frac{bg}{m}}(t_0 - t)$$

$$du = -\sqrt{\frac{bg}{m}} dt$$

$$-\sqrt{\frac{m}{bg}} du = dt$$

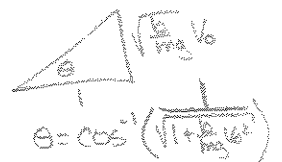
$$= \frac{m}{b} \ln \cos u + C$$

$$\cos\left(\sqrt{\frac{bg}{m}} t_0\right) = \cos\left(\sqrt{\frac{bg}{m}} \sqrt{\frac{m}{bg}} \tan^{-1}\left(\sqrt{\frac{b}{mg}} v_0\right)\right)$$

$$= \cos\left(\tan^{-1}\left(\sqrt{\frac{b}{mg}} v_0\right)\right)$$

$$= \cos \theta$$

$$= \left(\sqrt{1 + \frac{bv_0^2}{mg}}\right)^{-1}$$



ii) for $t > t_0$, $v_0 = 0$

$$m \frac{dv}{dt} = -mg + bv^2$$

$$\frac{m}{b} \frac{dv}{dt} = -\frac{mg}{b} + v^2$$

$$\frac{dv}{\frac{mg}{b} - v^2} = -\frac{b}{m} dt$$

$$\int_0^v \frac{dv}{\frac{mg}{b} - v^2} = \int_{t_0}^t -\frac{b}{m} dt$$

$$\sqrt{\frac{b}{mg}} \tanh^{-1}\left(\sqrt{\frac{b}{mg}} v\right) = -\frac{b}{m}(t-t_0)$$

$$\tanh^{-1}\left(\sqrt{\frac{b}{mg}} v\right) = -\sqrt{\frac{bg}{m}}(t-t_0)$$

$$v = \sqrt{\frac{mg}{b}} \tanh\left(-\sqrt{\frac{bg}{m}}(t-t_0)\right)$$

$$= -\sqrt{\frac{mg}{b}} \tanh\left(\sqrt{\frac{bg}{m}}(t-t_0)\right) \quad \{\text{odd function}\}$$

$$\int_{x_h}^x dx = -\sqrt{\frac{mg}{b}} \int_{t_0}^t \tanh\left(\sqrt{\frac{bg}{m}}(t-t_0)\right) dt$$

$$x - x_h = -\frac{m}{b} \ln \cosh\left(\sqrt{\frac{bg}{m}}(t-t_0)\right) \Big|_{t_0}^t$$

$$x = x_h - \frac{m}{b} \ln \cosh\left(\sqrt{\frac{bg}{m}}(t-t_0)\right)$$

$$x_h = x|_{t=t_0}$$

$$= \frac{m}{2b} \ln\left(1 + \frac{bv_0^2}{mg}\right)$$

$$x = \frac{m}{2b} \ln\left(1 + \frac{bv_0^2}{mg}\right) - \frac{m}{b} \ln \cosh\left(\sqrt{\frac{bg}{m}}(t-t_0)\right)$$

$$\int \frac{dv}{\frac{mg}{b} - v^2} = \frac{b}{mg} \sqrt{\frac{mg}{b}} \int \frac{\text{sech}^2 u du}{1 + \tanh^2 u}$$

$$v^2 = \frac{mg}{b} \tanh^2 u \quad = \sqrt{\frac{b}{mg}} \int du$$

$$v = \sqrt{\frac{mg}{b}} \tanh u$$

$$dv = \sqrt{\frac{mg}{b}} \text{sech}^2 u du$$

$$= \sqrt{\frac{b}{mg}} u + C$$

$$= \sqrt{\frac{b}{mg}} \tanh^{-1}\left(\sqrt{\frac{b}{mg}} v\right) + C$$

$$\int \tanh\left(\sqrt{\frac{bg}{m}}(t-t_0)\right) dt = \sqrt{\frac{m}{bg}} \int \tanh u du$$

$$u = \sqrt{\frac{bg}{m}}(t-t_0)$$

$$du = \sqrt{\frac{bg}{m}} dt$$

$$\sqrt{\frac{m}{bg}} du = dt$$

$$= \sqrt{\frac{m}{bg}} \int \frac{\sinh u du}{\cosh u}$$

$$= \sqrt{\frac{m}{bg}} \ln \cosh u + C$$

$$2-33 \quad v_0 = v_e = \left(\frac{2MG}{x} \right)^{1/2}$$

$$v = \frac{dx}{dt} = \left(\frac{2MG}{x} \right)^{1/2}$$

$$\frac{dx}{\left(\frac{2MG}{x} \right)^{1/2}} = dt$$

$$\int_{x_0}^x \frac{x^{1/2} dx}{(2MG)^{1/2}} = \int_0^t dt$$

$$\frac{1}{(2MG)^{1/2}} \left[\frac{2}{3} x^{3/2} \right]_{x_0}^x = t$$

$$\left(\frac{2}{9MG} \right)^{1/2} \left[x^{3/2} - x_0^{3/2} \right] = t$$

$$x^{3/2} - x_0^{3/2} = \left(\frac{9MG}{2} \right)^{1/2} t$$

$$x^{3/2} = x_0^{3/2} + \left(\frac{9MG}{2} \right)^{1/2} t$$

$$x = \left[x_0^{3/2} + \left(\frac{9MG}{2} \right)^{1/2} t \right]^{2/3}$$

$$\frac{1}{2} m v_0^2 + - \frac{mMG}{x} = E$$

$$= 0 \quad \{ \text{Escape condition} \}$$

$$\frac{1}{2} m v_0^2 = \frac{mMG}{x}$$

$$v_0^2 = \frac{2MG}{x}$$

$$v_e = \sqrt{\frac{2MG}{x}}$$

2-35

$$\cos \theta = \frac{1}{2}(e^{i\theta} + e^{-i\theta})$$

$$\cos^3 \theta = \frac{1}{8}(e^{i\theta} + e^{-i\theta})^3$$

$$= \frac{1}{8}(e^{i\theta} + e^{-i\theta})(e^{i\theta} + e^{-i\theta})(e^{i\theta} + e^{-i\theta})$$

$$= \frac{1}{8}[e^{2i\theta} + 1 + 1 + e^{-2i\theta}](e^{i\theta} + e^{-i\theta})$$

$$= \frac{1}{8}[e^{3i\theta} + 2e^{i\theta} + e^{-i\theta} + e^{i\theta} + 2e^{-i\theta} + e^{-3i\theta}]$$

$$= \frac{1}{8}[e^{3i\theta} + e^{-3i\theta} + 3e^{i\theta} + 3e^{-i\theta}]$$

$$2\cos 3\theta = e^{3i\theta} + e^{-3i\theta}$$

$$6\cos \theta = 3e^{i\theta} + 3e^{-i\theta}$$

$$= \frac{1}{8}[2\cos 3\theta + 6\cos \theta]$$

$$\boxed{\cos^3 \theta = \frac{1}{4}\cos 3\theta + \frac{3}{4}\cos \theta}$$

2-37

 $\omega_0^2 - \gamma^2$ is very small

$$\omega_1 = (\omega_0^2 - \gamma^2)^{1/2}$$

$$(2.133) \quad x = A e^{-\gamma t} \cos(\omega_1 t + \theta)$$

$$x = A e^{-\gamma t} \cos([\omega_0^2 - \gamma^2]^{1/2} t + \theta)$$

$$\cos(A+B) = \cos A \cos B - \sin A \sin B$$

$$= A e^{-\gamma t} [\cos \omega_1 t \cos \theta - \sin \omega_1 t \sin \theta]$$

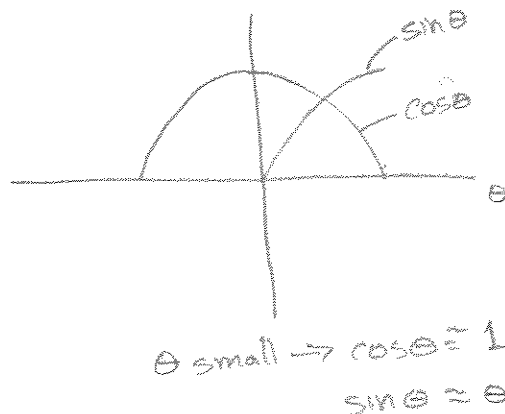
$$= A e^{-\gamma t} [\cos \theta - \omega_1 t \sin \theta]$$

$$= A \cos \theta e^{-\gamma t} - A \omega_1 t e^{-\gamma t} \sin \theta$$

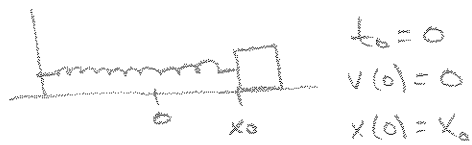
$$x = (C_1 + C_2 t) e^{-\gamma t}$$

$$C_1 = A \cos \theta$$

$$C_2 = -A \omega_1 \sin \theta$$



2-39.



i) underdamped, $\omega_0 > \gamma$

$$p = -\gamma \pm i\omega_1$$

$$\begin{aligned}
 x &= C_1 e^{-\gamma t + i\omega_1 t} + C_2 e^{-\gamma t - i\omega_1 t} \\
 &= e^{-\gamma t} (C_1 e^{i\omega_1 t} + C_2 e^{-i\omega_1 t}) \\
 &= e^{-\gamma t} (B_1 \cos \omega_1 t + B_2 \sin \omega_1 t)
 \end{aligned}$$

$$x_0 = x(0) = B_1$$

$$v = \dot{x} = -\gamma e^{-\gamma t} (B_1 \cos \omega_1 t + B_2 \sin \omega_1 t) + e^{-\gamma t} (-\omega_1 B_1 \sin \omega_1 t + \omega_1 B_2 \cos \omega_1 t)$$

$$0 = v(0) = -\gamma B_1 + \omega_1 B_2$$

$$\begin{aligned}
 B_2 &= \frac{\gamma B_1}{\omega_1} \\
 &= \frac{x_0 \gamma}{\omega_1}
 \end{aligned}$$

$$x = e^{-\gamma t} x_0 \left(\cos \omega_1 t + \frac{\gamma}{\omega_1} \sin \omega_1 t \right)$$

ii) critically damped, $\omega_0 = \gamma$

$$x = (C_1 + C_2 t) e^{-\gamma t}$$

$$x_0 = x(0) = C_1$$

$$v = \dot{x} = -\gamma e^{-\gamma t} (C_1 + C_2 t) + e^{-\gamma t} (C_2)$$

$$0 = v(0) = -\gamma C_1 + C_2$$

$$C_2 = \gamma C_1$$

$$C_2 = -\gamma x_0$$

$$x = (x_0 - \gamma x_0 t) e^{-\gamma t}$$

$$x = x_0 (1 - \gamma t) e^{-\gamma t}$$

iii) overdamped $\omega_0 < \gamma$

$$x = C_1 e^{-\gamma_1 t} + C_2 e^{-\gamma_2 t}$$

$$-\gamma_1 = -\gamma - (\gamma^2 - \omega_0^2)^{1/2}$$

$$-\gamma_2 = -\gamma + (\gamma^2 - \omega_0^2)^{1/2}$$

$$x_0 = x(0) = C_1 + C_2$$

$$v = \dot{x} = -\gamma_1 C_1 e^{-\gamma_1 t} - \gamma_2 C_2 e^{-\gamma_2 t}$$

$$0 = v(0) = -\gamma_1 C_1 - \gamma_2 C_2$$

$$C_1 = -\frac{\gamma_2}{\gamma_1} C_2$$

$$x_0 = -\frac{\gamma_2}{\gamma_1} C_2 + C_2$$

$$= \left(\frac{\gamma_2}{\gamma_1} + 1 \right) C_2$$

$$= \frac{-\gamma_2 + \gamma_1}{\gamma_1} C_2$$

$$\frac{x_0 \gamma_1}{-\gamma_2 + \gamma_1} = C_2$$

$$C_1 = \frac{-\gamma_2}{\gamma_1} \left(\frac{x_0 \gamma_1}{-\gamma_2 + \gamma_1} \right)$$

$$C_1 = \frac{-x_0 \gamma_2}{-\gamma_2 + \gamma_1}$$

$$x = \frac{-x_0 \gamma_2}{\gamma_1 - \gamma_2} e^{-\gamma_1 t} + \frac{x_0 \gamma_1}{\gamma_1 - \gamma_2} e^{-\gamma_2 t}$$

$$x = \frac{x_0}{\gamma_1 - \gamma_2} (\gamma_1 e^{-\gamma_2 t} - \gamma_2 e^{-\gamma_1 t})$$

2-41. $x(0) = X_0 \quad v(0) = -V_0$

i) underdamped, $\omega_0 > \gamma$

$$p = -\gamma \pm i\omega_1$$

$$x = e^{-\gamma t} (B_1 \cos \omega_1 t + B_2 \sin \omega_1 t)$$

$$X_0 = x(0) = B_1$$

$$-V_0 = v(0) = -\gamma B_1 + \omega_1 B_2$$

$$-V_0 = -\gamma X_0 + \omega_1 B_2$$

$$\frac{\gamma X_0 - V_0}{\omega_1} = B_2$$

$$x = e^{-\gamma t} \left(X_0 \cos \omega_1 t + \frac{\gamma X_0 - V_0}{\omega_1} \sin \omega_1 t \right)$$

ii) critically damped, $\omega_0 = \gamma$

$$x = (C_1 + C_2 t) e^{-\gamma t}$$

$$X_0 = x(0) = C_1$$

$$-V_0 = v(0) = -\gamma C_1 + C_2$$

$$-V_0 = -X_0 \gamma + C_2$$

$$X_0 \gamma - V_0 = C_2$$

$$x = (X_0 + (X_0 \gamma - V_0) t) e^{-\gamma t}$$

iii) overdamped, $\omega_0 < \gamma$

$$x = C_1 e^{-\gamma_1 t} + C_2 e^{-\gamma_2 t}$$

$$X_0 = x(0) = C_1 + C_2$$

$$-V_0 = v(0) = -\gamma_1 C_1 - \gamma_2 C_2$$

$$\gamma_2 C_2 - V_0 = -\gamma_1 C_1$$

$$\frac{V_0 - \gamma_2 C_2}{\gamma_1} = C_1$$

$$C_1 + C_2 = X_0$$

$$\frac{V_0 - \gamma_2 C_2}{\gamma_1} + C_2 = X_0$$

$$\frac{V_0 - \gamma_2 C_2}{\gamma_1} + C_2 = X_0$$

$$C_2 \left(1 + \frac{\gamma_2}{\gamma_1}\right) = X_0 - \frac{V_0}{\gamma_1}$$

$$C_2 \left(\frac{\gamma_1 + \gamma_2}{\gamma_1}\right) = \frac{X_0 \gamma_1 - V_0}{\gamma_1}$$

$$C_2 = \frac{X_0 \gamma_1 - V_0}{\gamma_1 + \gamma_2}$$

$$C_1 + \frac{X_0 \gamma_1 - V_0}{\gamma_1 + \gamma_2} = X_0$$

$$C_1 = \frac{X_0(\gamma_1 + \gamma_2) - X_0 \gamma_1 + V_0}{\gamma_1 + \gamma_2}$$

$$= \frac{X_0 \gamma_2 + V_0}{\gamma_1 + \gamma_2}$$

$$= \frac{V_0 - X_0 \gamma_2}{\gamma_1 - \gamma_2}$$

$$X = \frac{V_0 - X_0 \gamma_2}{\gamma_1 - \gamma_2} e^{-\gamma_1 t} + \frac{X_0 \gamma_1 - V_0}{\gamma_1 + \gamma_2} e^{-\gamma_2 t}$$

$$X = (\gamma_1 - \gamma_2)^{-1} \left([V_0 - X_0 \gamma_2] e^{-\gamma_1 t} + [X_0 \gamma_1 - V_0] e^{-\gamma_2 t} \right) \quad (V_0 > 0)$$

$$X = (\gamma_1 - \gamma_2)^{-1} \left([X_0 \gamma_1 + V_0] e^{-\gamma_2 t} - [X_0 \gamma_2 + V_0] e^{-\gamma_1 t} \right) \quad (V_0 < 0)$$

2-43

critically damped

$$x = (x_0 + (x_0\gamma - v_0)t) e^{-\gamma t}$$

$$x = (0.2 + 0t) e^{-70t}$$

$$x = 0.2 e^{-70t}$$

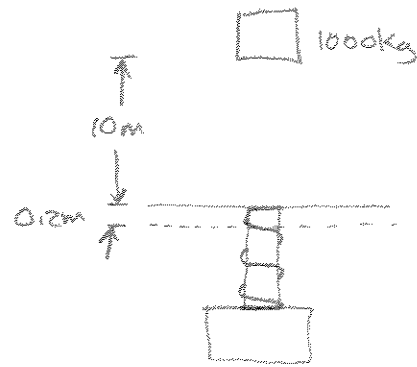
$$.001 = 0.2 e^{-70t}$$

$$\frac{.001}{0.2} = e^{-70t}$$

$$.005 = e^{-70t}$$

$$\ln(.005) = -70t$$

$$.076s = t$$



$$v_0: \frac{1}{2}mv^2 = mgh$$

$$v^2 = 2gh$$

$$v = \sqrt{2gh} = 14 \text{ m/s}$$

$$kx = mg$$

$$k = \frac{mg}{x}$$

$$= \frac{(1000 \text{ kg})(9.81 \text{ m/s}^2)}{0.2 \text{ m}}$$

$$k = 4.9 \times 10^4 \frac{\text{kg}}{\text{s}^2}$$

To avoid overshoot!

$$x_0\gamma - v_0 = 0$$

$$\gamma = \frac{v_0}{x_0}$$

$$= \frac{14 \text{ m/s}}{0.2 \text{ m}}$$

$$\gamma = 70 \text{ s}^{-1}$$

$$\frac{b}{2m} = \gamma$$

$$b = 82 \text{ m}$$

$$b = 1.4 \times 10^5 \frac{\text{kg}}{\text{s}}$$

2-45

$$a) \quad m\ddot{x} + b\dot{x} + Kx = F_0$$

$$x_h: \ddot{x} + \frac{b}{m}\dot{x} + \frac{K}{m}x = 0 \quad x = e^{pt}$$

$$p^2 + \frac{b}{m}p + \frac{K}{m} = 0$$

$$p = -\frac{b}{2m} \pm \sqrt{\left(\frac{b}{2m}\right)^2 - \frac{K}{m}} \quad \gamma = \frac{b}{2m} \quad \omega_0 = \sqrt{\frac{K}{m}}$$

$$\omega_1^2 = \omega_0^2 - \gamma^2$$

$$p = -\gamma \pm i\omega_1$$

$$x_h = C_1 e^{-\gamma t + i\omega_1 t} + C_2 e^{-\gamma t - i\omega_1 t}$$

$$= e^{-\gamma t} [C_1 e^{i\omega_1 t} + C_2 e^{-i\omega_1 t}] \quad C_2 = C_1^* = \frac{1}{2} A e^{-i\theta}$$

$$= e^{-\gamma t} \left[\frac{1}{2} A e^{i(\omega_1 t + \theta)} + \frac{1}{2} A e^{-i(\omega_1 t + \theta)} \right]$$

$$x_h = A e^{-\gamma t} \cos(\omega_1 t + \theta) \quad \left\{ \cos x = \frac{e^{ix} + e^{-ix}}{2} \right\}$$

$$x_p = C$$

$$\dot{x}_p = \ddot{x}_p = 0$$

$$KC = F_0$$

$$C = \frac{F_0}{K}$$

$$x_p = \frac{F_0}{K}$$

$$x = x_h + x_p$$

$$x = A e^{-\gamma t} \cos(\omega_1 t + \theta) + \frac{F_0}{K}$$

2-47

$$m\ddot{x} + kx = F_0 \sin \omega t, \quad v(0) = 0, \quad x(0) = 0$$

$$x_h: \ddot{x} + \frac{k}{m}x = 0$$

$$p^2 + \frac{k}{m} = 0 \quad x = e^{pt}$$

$$p^2 = -\frac{k}{m}$$

$$p = \pm i\sqrt{\frac{k}{m}}$$

$$p = \pm i\omega_0 \quad \omega_0 = \sqrt{\frac{k}{m}}$$

$$x_h = C_1 e^{i\omega_0 t} + C_2 e^{-i\omega_0 t} \quad C_1 = \frac{A}{2} e^{i\theta} \quad C_2 = C_1^* = \frac{A}{2} e^{-i\theta}$$

$$= \frac{A}{2} e^{i(\omega_0 t + \theta)} + \frac{A}{2} e^{-i(\omega_0 t + \theta)}$$

$$x_h = A \cos(\omega_0 t + \theta)$$

$$x_p = C_3 \sin(\omega t + \theta_1)$$

$$\dot{x}_p = \omega C_3 \cos(\omega t + \theta_1)$$

$$\ddot{x}_p = -\omega^2 C_3 \sin(\omega t + \theta_1)$$

$$-\omega^2 C_3 \sin(\omega t + \theta_1) + \frac{k}{m} C_3 \sin(\omega t + \theta_1) = \frac{F_0}{m} \sin \omega t$$

$$C_3 \left[\frac{k}{m} - \omega^2 \right] \sin(\omega t + \theta_1) = F_0 \sin \omega t$$

$$C_3 \left[\frac{k - m\omega^2}{m} \right] = \frac{F_0}{m} \quad \sin(\omega t + \theta_1) = \sin \omega t$$

$$C_3 = \frac{F_0}{k - m\omega^2} \quad \theta_1 = 0$$

$$x_p = \frac{F_0}{k - m\omega^2} \sin \omega t$$

$$x(t) = x_h(t) + x_p(t)$$

$$= A \cos(\omega_0 t + \theta) + \frac{F_0}{k - m\omega^2} \sin \omega t$$

$$0 = x(0) = A \cos \theta$$

$$v(t) = \dot{x}(t) = -A\omega_0 \sin(\omega_0 t + \theta) + \frac{F_0 \omega}{k - m\omega^2} \cos \omega t$$

$$0 = v(0) = -A\omega_0 \sin \theta + \frac{F_0 \omega}{k - m\omega^2}$$

$$A \cos \theta = 0$$

$$\theta = \frac{\pi}{2}$$

$$A \omega_0 \sin \theta = \frac{F_0 \omega}{k - m \omega^2}$$

$$A = \frac{F_0 \omega}{\omega_0 (k - m \omega^2)}$$

$$x(t) = \frac{F_0 \omega}{\omega_0 (k - m \omega^2)} \cos(\omega_0 t + \frac{\pi}{2}) + \frac{F_0}{k - m \omega^2} \sin \omega t$$

$$= \frac{-F_0 \omega}{\omega_0 (k - m \omega^2)} \sin \omega_0 t + \frac{F_0}{k - m \omega^2} \sin \omega t$$

$$= \frac{F_0}{\omega_0 (k - m \omega^2)} [\omega \sin \omega t - \omega_0 \sin \omega_0 t]$$

$$x(t) = \frac{F_0}{m \omega_0 (\omega_0^2 - \omega^2)} [\omega_0 \sin \omega t - \omega \sin \omega_0 t]$$

2-49

$$\ddot{x} + 2\gamma\dot{x} + \omega_0^2 x = \frac{F_0}{m} \cos \omega t, \quad x(0) = x_0, \quad \dot{x}(0) = v_0, \quad \omega_0 = \gamma$$

$$\ddot{x} + 2\omega_0 \dot{x} + \omega_0^2 x = \frac{F_0}{m} \cos \omega t$$

 $x_h:$

$$\ddot{x} + 2\omega_0 \dot{x} + \omega_0^2 x = 0 \quad x = e^{pt}$$

$$p^2 + 2\omega_0 p + \omega_0^2 = 0$$

$$p = \frac{-2\omega_0 \pm \sqrt{4\omega_0^2 - 4\omega_0^2}}{2}$$

$$= -\omega_0 = -\gamma$$

$$x_h = (C_1 + C_2 t) e^{-\gamma t}$$

 $x_p:$

$$x_p = A \cos \omega t + B \sin \omega t$$

$$\dot{x} = -\omega A \sin \omega t + \omega B \cos \omega t$$

$$\ddot{x} = -\omega^2 A \cos \omega t - \omega^2 B \sin \omega t$$

$$\ddot{x} + 2\omega_0 \dot{x} + \omega_0^2 x = \frac{F_0}{m} \cos \omega t$$

$$-\omega^2 A \cos \omega t - \omega^2 B \sin \omega t + 2\omega_0 (-\omega A \sin \omega t + \omega B \cos \omega t) + \omega_0^2 (A \cos \omega t + B \sin \omega t) = \frac{F_0}{m} \cos \omega t$$

$$-\omega^2 A \cos \omega t + 2\omega_0 \omega B \cos \omega t + \omega_0^2 A \cos \omega t = \frac{F_0}{m} \cos \omega t$$

$$-\omega^2 A + 2\omega_0 \omega B + \omega_0^2 A = \frac{F_0}{m}$$

$$-\omega^2 B \sin \omega t - 2\omega_0 \omega A \sin \omega t + \omega_0^2 B \sin \omega t = 0$$

$$-\omega^2 B - 2\omega_0 \omega A + \omega_0^2 B = 0$$

$$A(\omega_0^2 - \omega^2) + 2\omega_0 \omega B = \frac{F_0}{m} \quad B(\omega_0^2 - \omega^2) - 2\omega_0 \omega A = 0$$

$$A(\omega_0^2 - \omega^2) + \frac{(2\omega_0 \omega)^2 A}{(\omega_0^2 - \omega^2)} = \frac{F_0}{m}$$

$$B = \frac{2\omega_0 \omega A}{(\omega_0^2 - \omega^2)}$$

$$A \left[\frac{(\omega_0^2 - \omega^2)^2 + 4\omega_0^2 \omega^2}{\omega_0^2 - \omega^2} \right] = \frac{F_0}{m}$$

$$\begin{aligned} A &= \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 - \omega^2)^2 + 4\omega_0^2 \omega^2} \\ &= \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{\omega_0^4 - 2\omega_0^2 \omega^2 + \omega^4 + 4\omega_0^2 \omega^2} \\ &= \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{\omega_0^4 + 2\omega_0^2 \omega^2 + \omega^4} \\ &= \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 + \omega^2)^2} \end{aligned}$$

$$\begin{aligned} B &= \frac{2\omega_0 \omega}{\omega_0^2 - \omega^2} \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 + \omega^2)^2} \\ &= \frac{F_0}{m} \frac{2\omega_0 \omega}{(\omega_0^2 + \omega^2)^2} \end{aligned}$$

$$X_p = \frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} \left[(\omega_0^2 - \omega^2) \cos \omega t + 2\omega_0 \omega \sin \omega t \right]$$

$$x(t) = x_h(t) + x_p(t)$$

$$= (C_1 + C_2 t) e^{-\gamma t} + \frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} \left[(\omega_0^2 - \omega^2) \cos \omega t + 2\gamma \omega \sin \omega t \right]$$

$$x_0 = x(0) = C_1 + \frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} \left[(\omega_0^2 - \omega^2) \right]$$

$$C_1 = x_0 - \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 + \omega^2)^2}$$

$$\dot{x} = -\gamma (C_1 + C_2 t) e^{-\gamma t} + C_2 e^{-\gamma t} + \frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} \left[-\omega (\omega_0^2 - \omega^2) \sin \omega t + 2\gamma \omega^2 \cos \omega t \right]$$

$$v_0 = v(0) = -\gamma C_1 + C_2 + \frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} \left[2\gamma \omega^2 \right]$$

$$v_0 = -\gamma \left[x_0 - \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 + \omega^2)^2} \right] + C_2 + \frac{F_0}{m} \frac{2\gamma \omega^2}{(\omega_0^2 + \omega^2)^2}$$

$$C_2 = V_0 + \gamma \left[X_0 - \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 + \omega^2)^2} \right] - \frac{F_0}{m} \frac{2\gamma\omega^2}{(\omega_0^2 + \omega^2)^2}$$

$$= V_0 + \gamma X_0 - \gamma \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 + \omega^2)^2} - \frac{F_0}{m} \frac{2\gamma\omega^2}{(\omega_0^2 + \omega^2)^2}$$

$$= V_0 + \gamma X_0 - \frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} \left[\gamma(\omega_0^2 - \omega^2) - 2\gamma\omega^2 \right]$$

$$X(t) = \left(X_0 - \frac{F_0}{m} \frac{\omega_0^2 - \omega^2}{(\omega_0^2 + \omega^2)^2} + \left[V_0 + \gamma X_0 - \frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} [\gamma\omega_0^2 - 3\gamma\omega^2] \right] t \right) e^{-\gamma t} +$$

$$\frac{F_0}{m} \frac{1}{(\omega_0^2 + \omega^2)^2} \left[(\omega_0^2 - \omega^2) \cos \omega t + 2\gamma\omega \sin \omega t \right]$$

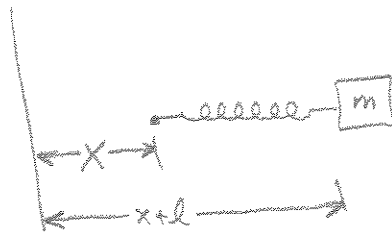
$$= \frac{F_0}{m(\omega_0^2 + \omega^2)^2} \left[(\omega_0^2 - \omega^2 + [\gamma\omega_0^2 + 3\gamma\omega^2]t) e^{-\gamma t} + (\omega_0^2 - \omega^2) \cos \omega t + 2\gamma\omega \sin \omega t \right]$$

$$+ (X_0 + [V_0 + \gamma X_0]t) e^{-\gamma t}$$

$$X(t) = \frac{F_0}{m(\gamma^2 + \omega^2)^2} \left[(\gamma^2 - \omega^2) \cos \omega t + 2\gamma\omega \sin \omega t - (\gamma^2 - \omega^2 + \gamma^3 t - 3\gamma\omega^2 t) e^{-\gamma t} \right]$$

$$+ (X_0 + V_0 t + \gamma X_0 t) e^{-\gamma t}$$

2-51



$l = \text{relaxed length}$

$$X = a \sin \omega t$$

$$m\ddot{x} = -b\dot{x} - kx' \quad x' = x+l-X$$

$$m\ddot{x} = -b\dot{x} - k(x+l-X)$$

$$= -b\dot{x} - kx - kl + kX$$

$$= -b\dot{x} - kx - kl + k a \sin \omega t$$

$$m\ddot{x} + b\dot{x} + kx = -kl + k a \sin \omega t \quad kl = 0$$

$$\boxed{m\ddot{x} + b\dot{x} + kx = k a \sin \omega t}$$

If $f = -b(\dot{x} - \dot{X})$ then

$$f = -b\dot{x} + \omega b a \cos \omega t$$

So,

$$m\ddot{x} = -b(\dot{x} - \dot{X}) + k a \sin \omega t - kx - kl$$

$$= -b\dot{x} + \omega b a \cos \omega t + k a \sin \omega t - kx$$

$$\boxed{m\ddot{x} + b\dot{x} + kx = \omega b a \cos \omega t + k a \sin \omega t}$$

2-53

$$0 < t < \frac{3\pi}{2\omega_0} \quad m\ddot{x} + kx = 0 \quad x(0) = 0, \quad \dot{x}(0) = V_0$$

$$\ddot{x} + \frac{k}{m}x = 0$$

$$\ddot{x} + \omega_0^2 x = 0 \quad x = e^{pt}$$

$$p^2 + \omega_0^2 = 0$$

$$p = \pm j\omega_0$$

$$x = C_1 \cos \omega_0 t + C_2 \sin \omega_0 t$$

$$0 = x(0) = C_1$$

$$\dot{x} = -\omega_0 C_1 \sin \omega_0 t + \omega_0 C_2 \cos \omega_0 t$$

$$V_0 = \dot{x}(0) = \omega_0 C_2$$

$$C_2 = \frac{V_0}{\omega_0}$$

$$x = \frac{V_0}{\omega_0} \sin \omega_0 t, \quad 0 < t < \frac{3\pi}{2\omega_0}$$

$$t \geq \frac{3\pi}{2\omega_0} \quad m\ddot{x} + kx = B \cos(\omega t + \theta)$$

$$\ddot{x} + \omega_0^2 x = \frac{B}{m} \cos(\omega t + \theta)$$

$$x_h = K_1 \cos \omega_0 t + K_2 \sin \omega_0 t$$

$$x_p = C_3 \cos(\omega t + \theta) + C_4 \sin(\omega t + \theta)$$

$$\dot{x}_p = -\omega C_3 \sin(\omega t + \theta) + \omega C_4 \cos(\omega t + \theta)$$

$$\ddot{x}_p = -\omega^2 C_3 \cos(\omega t + \theta) - \omega^2 C_4 \sin(\omega t + \theta)$$

$$-\omega^2 C_3 \cos(\omega t + \theta) - \omega^2 C_4 \sin(\omega t + \theta) + \omega_0^2 C_3 \cos(\omega t + \theta) + \omega_0^2 C_4 \sin(\omega t + \theta) = \frac{B}{m} \cos(\omega t + \theta)$$

$$C_3(\omega_0^2 - \omega^2) = \frac{B}{m}$$

$$C_4(\omega_0^2 - \omega^2) = 0$$

$$C_3 = \frac{B}{m(\omega_0^2 - \omega^2)}$$

$$C_4 = 0$$

initial conditions

$$x\left(\frac{3\pi}{2\omega_0}\right) = \frac{V_0}{\omega_0} \sin\left(\frac{3\pi}{2}\right) = -\frac{V_0}{\omega_0}$$

$$\dot{x} = V_0 \cos \omega_0 t$$

$$\dot{x}\left(\frac{3\pi}{2\omega_0}\right) = 0$$

$$X = X_h + X_p$$

$$X = K_1 \cos \omega_0 t + K_2 \sin \omega_0 t + \frac{B}{m} (\omega_0^2 - \omega^2)^{-1} \cos(\omega t + \theta)$$

$$\frac{-V_0}{\omega_0} = X\left(\frac{3\pi}{2\omega_0}\right) = -K_2 + \frac{B}{m} (\omega_0^2 - \omega^2)^{-1} \cos \alpha \quad \alpha = \frac{3\pi\omega}{2\omega_0} + \theta$$

$$K_2 = \frac{V_0}{\omega_0} + \frac{B}{m} (\omega_0^2 - \omega^2)^{-1} \cos \alpha$$

$$\dot{X} = -\omega_0 K_1 \sin \omega_0 t + \omega_0 K_2 \cos \omega_0 t - \frac{B\omega}{m} (\omega_0^2 - \omega^2)^{-1} \sin(\omega t + \theta)$$

$$0 = \dot{X}\left(\frac{3\pi}{2\omega_0}\right) = \omega_0 K_1 - \frac{B\omega}{m} (\omega_0^2 - \omega^2)^{-1} \sin \alpha$$

$$K_1 = \frac{B\omega}{m\omega_0} (\omega_0^2 - \omega^2)^{-1} \sin \alpha$$

$$X = \frac{B}{m} (\omega_0^2 - \omega^2)^{-1} \frac{\omega}{\omega_0} \sin \alpha \cos \omega_0 t + \left[\frac{V_0}{\omega_0} + \frac{B}{m} (\omega_0^2 - \omega^2)^{-1} \cos \alpha \right] \sin \omega_0 t + \frac{B}{m} (\omega_0^2 - \omega^2)^{-1} \cos(\omega t + \theta)$$

$$X = \frac{B}{m} (\omega_0^2 - \omega^2)^{-1} \left[\frac{\omega}{\omega_0} \sin \alpha \cos \omega_0 t + \cos \alpha \sin \omega_0 t + \cos(\omega t + \theta) \right] + \frac{V_0}{\omega_0} \sin \omega_0 t, \quad t \geq \frac{3\pi}{2\omega_0}$$

$$\alpha = \frac{3\pi\omega}{2\omega_0} + \theta$$

2-55

$$\ddot{x} + \frac{K}{m}x = F(t) \quad F(t) = \begin{cases} 0, & t < t_0 \\ P_0/\delta t, & t_0 \leq t \leq t_0 + \delta t \\ 0, & t > t_0 + \delta t \end{cases}$$

$$x(0) = 0$$

$$v(0) = 0$$

a) i) $t < t_0$

$$\ddot{x} + \omega_0^2 x = 0$$

$$x = C_1 \cos \omega_0 t + C_2 \sin \omega_0 t$$

$$0 = x(0) = C_1$$

$$\dot{x} = -\omega_0 C_1 \sin \omega_0 t + \omega_0 C_2 \cos \omega_0 t$$

$$0 = v(0) = C_2$$

$$\boxed{x = 0 \quad t < t_0}$$

ii) $t_0 \leq t \leq t_0 + \delta t$

$$\ddot{x} + \omega_0^2 x = \frac{P_0}{m \delta t} \quad x(t_0) = 0$$

$$v(t_0) = 0$$

$$x_h = C_1 \cos \omega_0(t - t_0) + C_2 \sin \omega_0(t - t_0)$$

$$x_p = K_1$$

$$\frac{K}{m} K_1 = \frac{P_0}{\delta t m}$$

$$K_1 = \frac{m}{K} \frac{P_0}{\delta t}$$

$$x_p = \frac{P_0}{K \delta t}$$

$$x = x_h + x_p$$

$$= C_1 \cos \omega_0(t - t_0) + C_2 \sin \omega_0(t - t_0) + \frac{P_0}{K \delta t}$$

$$0 = x(t_0) = C_1 \cos(0) + C_2 \sin(0) + \frac{P_0}{K \delta t}$$

$$C_1 = -\frac{P_0}{K \delta t}$$

$$\dot{x} = -\omega_0 C_1 \sin \omega_0(t - t_0) + \omega_0 C_2 \cos \omega_0(t - t_0)$$

$$0 = \dot{x}(t_0) = \omega_0 C_2$$

$$C_2 = 0$$

$$X = \frac{-P_0}{k\delta t} \cos \omega_0(t-t_0) + \frac{P_0}{k\delta t}$$

$$X = \frac{P_0}{k\delta t} [1 - \cos \omega_0(t-t_0)], \quad t_0 \leq t \leq t_0 + \delta t$$

iii) $t > t_0 + \delta t$

$$\ddot{X} + \omega_0^2 X = 0$$

$$X = C_1 \cos \omega_0(t - (t_0 + \delta t)) + C_2 \sin \omega_0(t - (t_0 + \delta t))$$

initial conditions:

$$X(t_0 + \delta t) = \frac{P_0}{k\delta t} [1 - \cos \omega_0(\delta t)]$$

$$\dot{X} = \frac{P_0 \omega_0}{k\delta t} \sin \omega_0(t - t_0)$$

$$\dot{X}(t_0 + \delta t) = \frac{P_0 \omega_0}{k\delta t} \sin \omega_0(\delta t)$$

$$X(t_0 + \delta t) = C_1 \cos(0) + C_2 \sin(0)$$

$$\frac{P_0}{k\delta t} [1 - \cos \omega_0(\delta t)] = C_1$$

$$\dot{X} = -C_1 \omega_0 \sin \omega_0(t - (t_0 + \delta t)) + C_2 \omega_0 \cos \omega_0(t - (t_0 + \delta t))$$

$$\dot{X}(t_0 + \delta t) = C_2 \omega_0$$

$$\sin \omega_0(\delta t) \frac{P_0 \omega_0}{k\delta t} = C_2 \omega_0$$

$$C_2 = \frac{P_0}{k\delta t} \sin \omega_0(\delta t)$$

$$X = \frac{P_0}{k\delta t} \left[(1 - \cos \omega_0(\delta t)) \cos \omega_0(t - (t_0 + \delta t)) + \sin \omega_0(\delta t) \sin \omega_0(t - (t_0 + \delta t)) \right]$$

$$= \frac{P_0}{k\delta t} \left[(1 - \cos \omega_0(\delta t)) \cos \omega_0([t - t_0] - \delta t) + \sin \omega_0(\delta t) \sin \omega_0([t - t_0] - \delta t) \right]$$

$$\cos \omega_0([t-t_0]-\delta t) = \cos \omega_0(t-t_0) \cos \omega_0 \delta t + \sin \omega_0(t-t_0) \sin \omega_0 \delta t$$

$$\sin \omega_0([t-t_0]-\delta t) = \sin \omega_0(t-t_0) \cos \omega_0 \delta t - \cos \omega_0(t-t_0) \sin \omega_0 \delta t$$

$$- \cos \omega_0 \delta t \cos \omega_0([t-t_0]-\delta t) = -\cos^2 \omega_0 \delta t \cos \omega_0(t-t_0) - \sin \omega_0 \delta t \cos \omega_0 \delta t \sin \omega_0(t-t_0)$$

$$\sin \omega_0 \delta t \sin \omega_0([t-t_0]-\delta t) = \sin \omega_0 \delta t \cos \omega_0 \delta t \sin \omega_0(t-t_0) - \sin^2 \omega_0 \delta t \cos \omega_0(t-t_0)$$

$$- \cos \omega_0 \delta t \cos \omega_0([t-t_0]-\delta t) + \sin \omega_0 \delta t \sin \omega_0([t-t_0]-\delta t) =$$

$$- \cos \omega_0(t-t_0) (\cos^2 \omega_0 \delta t + \sin^2 \omega_0 \delta t) = -\cos \omega_0(t-t_0)$$

$$X = \frac{P_0}{K \delta t} [\cos \omega_0([t-t_0]-\delta t) - \cos \omega_0(t-t_0)], \quad t > t_0 + \delta t$$

$$2-57 \quad m\ddot{x} + b\dot{x} + kx = F, \quad \gamma = \frac{\omega_0}{3}, \quad x(0) = 0, \quad v(0) = 0, \quad F = A \sin \omega_0 t + B \sin 3\omega_0 t$$

$$a) \quad m\ddot{x}_n + b\dot{x}_n + kx_n = F_n(t)$$

$$F_1 = A \sin \omega_0 t$$

$$x_h = 0 \quad (x(0) = 0, v(0) = 0)$$

$$x_{p1} = K_{11} \cos \omega_0 t + K_{21} \sin \omega_0 t$$

$$\dot{x}_{p1} = -\omega_0 K_{11} \sin \omega_0 t + \omega_0 K_{21} \cos \omega_0 t$$

$$\ddot{x}_{p1} = -\omega_0^2 K_{11} \cos \omega_0 t - \omega_0^2 K_{21} \sin \omega_0 t$$

$$\ddot{x}_{p1} + \frac{b}{m} \dot{x}_{p1} + \omega_0^2 x_{p1} = \frac{A}{m} \sin \omega_0 t$$

$$\cos \omega_0 t: -\omega_0^2 K_{11} + \frac{b}{m} \omega_0 K_{21} + K_{11} \omega_0^2 = 0$$

$$\sin \omega_0 t: -\omega_0^2 K_{21} - \frac{b}{m} \omega_0 K_{11} + K_{21} \omega_0^2 = \frac{A}{m}$$

$$\cos 3\omega_0 t: -\omega_0^2 K_{11} + \frac{2\omega_0^2}{3} K_{21} + \omega_0^2 K_{11} = 0$$

$$\frac{2\omega_0^2}{3} K_{21} = 0$$

$$K_{21} = 0$$

$$\sin \omega_0 t: -\omega_0^2 K_{21} - \frac{2\omega_0^2}{3} K_{11} + \omega_0^2 K_{21} = \frac{A}{m}$$

$$-\frac{2\omega_0^2}{3} K_{11} = \frac{A}{m}$$

$$K_{11} = -\frac{3A}{2m\omega_0^2}$$

$$x_{p1} = \frac{-3A}{2m\omega_0^2} \cos \omega_0 t$$

$$F_2 = B \sin 3\omega_0 t$$

$$x_h = 0 \quad (x(0) = 0, v(0) = 0)$$

$$x_{p2} = K_{12} \cos 3\omega_0 t + K_{22} \sin 3\omega_0 t$$

$$\dot{x}_{p2} = -3\omega_0 K_{12} \sin 3\omega_0 t + 3\omega_0 K_{22} \cos 3\omega_0 t$$

$$\ddot{x}_{p2} = -9\omega_0^2 K_{12} \cos 3\omega_0 t - 9\omega_0^2 K_{22} \sin 3\omega_0 t$$

$$\ddot{x}_{p2} + \frac{b}{m} \dot{x}_{p2} + \omega_0^2 x_{p2} = \frac{B}{m} \sin 3\omega_0 t$$

$$\cos 3\omega_0 t: -9\omega_0^2 K_{12} + \frac{b}{m} 3\omega_0 K_{22} + \omega_0^2 K_{12} = 0$$

$$-9\omega_0^2 K_{12} + 2\omega_0^2 K_{22} + \omega_0^2 K_{12} = 0$$

$$-8\omega_0^2 K_{12} + 2\omega_0^2 K_{22} = 0$$

$$\sin 3\omega_0 t: -9\omega_0^2 K_{22} - 2\omega_0^2 K_{12} + \omega_0^2 K_{22} = \frac{B}{m}$$

$$-8\omega_0^2 K_{22} - 2\omega_0^2 K_{12} = \frac{B}{m}$$

$$-8\omega_0^2 K_{12} + 2\omega_0^2 K_{22} = 0$$

$$-2\omega_0^2 K_{12} - 8\omega_0^2 K_{22} = \frac{B}{m}$$

$$-8\omega_0^2 K_{12} + 2\omega_0^2 K_{22} = 0$$

$$8\omega_0^2 K_{12} + 32\omega_0^2 K_{22} = -4B/m$$

$$34\omega_0^2 K_{22} = -4B/m$$

$$K_{22} = \frac{-2B}{17\omega_0^2 m}$$

$$-8\omega_0^2 K_{12} + 2\omega_0^2 \left(\frac{-2B}{17\omega_0^2 m} \right) = 0$$

$$-8\omega_0^2 K_{12} - \frac{4B}{17m} = 0$$

$$-8\omega_0^2 K_{12} = \frac{4B}{17m}$$

$$K_{12} = \frac{-B}{34m\omega_0^2}$$

$$x_{p1} = \frac{-3A}{2m\omega^2} \cos \omega t$$

$$x_{p2} = \frac{-B}{34m\omega^2} \cos 3\omega t - \frac{2B}{17m\omega^2} \sin 3\omega t$$

$$= \frac{-B}{34m\omega^2} [\cos 3\omega t - 4 \sin 3\omega t]$$

$$x_p(t) = \sum_n x_{pn}(t)$$

$$= \frac{-3A}{2m\omega^2} \cos \omega t - \frac{B}{34m\omega^2} [\cos 3\omega t - 4 \sin 3\omega t]$$

$$= \frac{1}{m\omega^2} \left[-\frac{3A}{2} \cos \omega t - \frac{B}{34} (\cos 3\omega t - 4 \sin 3\omega t) \right]$$

$$x_h: \ddot{x} + 2\gamma \dot{x} + \omega_0^2 x = 0$$

$$\ddot{x} + \frac{2\omega_0}{3} \dot{x} + \omega_0^2 x = 0 \quad x = e^{pt}$$

$$p^2 + \frac{2}{3}\omega_0 p + \omega_0^2 = 0$$

$$p = \frac{-\frac{2}{3}\omega_0 \pm \left(\frac{4}{9}\omega_0^2 - 4\omega_0^2\right)^{1/2}}{2}$$

$$p = \frac{-\omega_0}{3} \pm \left(\frac{1}{9}\omega_0^2 - \omega_0^2\right)^{1/2}$$

$$= \frac{-\omega_0}{3} \pm \left(-\frac{8}{9}\omega_0^2\right)^{1/2}$$

$$= \frac{-\omega_0}{3} \pm i \frac{2\sqrt{2}}{3} \omega_0$$

$$x_h = e^{\frac{-\omega_0}{3}t} \left(C_1 \cos\left(\frac{2\sqrt{2}}{3}\omega_0 t\right) + C_2 \sin\left(\frac{2\sqrt{2}}{3}\omega_0 t\right) \right)$$

$$x(t) = e^{\frac{-\omega_0}{3}t} \left(C_1 \cos\left(\frac{2\sqrt{2}}{3}\omega_0 t\right) + C_2 \sin\left(\frac{2\sqrt{2}}{3}\omega_0 t\right) \right) - \frac{1}{m\omega^2} \left[\frac{3A}{2} \cos \omega t + \frac{B}{34} (\cos 3\omega t - 4 \sin 3\omega t) \right]$$

$$0 = x(0) = C_1 - \frac{1}{m\omega^2} \left[\frac{3A}{2} + \frac{B}{34} \right]$$

$$C_1 = \frac{1}{m\omega^2} \left[\frac{3A}{2} + \frac{B}{34} \right]$$

$$\dot{x}(t) = -\frac{\omega_0}{3} e^{-\frac{\omega_0}{3}t} \left(C_1 \cos \frac{2\sqrt{2}}{3} \omega_0 t + C_2 \sin \frac{2\sqrt{2}}{3} \omega_0 t \right) + e^{-\frac{\omega_0}{3}t} \left(-\frac{2\sqrt{2}A\omega_0}{3} \sin \frac{2\sqrt{2}}{3} \omega_0 t + \frac{2\sqrt{2}B\omega_0}{3} \cos \frac{2\sqrt{2}}{3} \omega_0 t \right) - \frac{1}{m\omega_0^2} \left[-\frac{3A\omega_0}{2} \sin \omega_0 t - \frac{3B\omega_0}{34} \sin 3\omega_0 t + \frac{12B\omega_0}{34} \cos 3\omega_0 t \right]$$

$$0 = \dot{x}(0) = -\frac{\omega_0}{3} C_1 + \frac{2\sqrt{2}}{3} \omega_0 C_2 - \frac{1}{m\omega_0^2} \frac{12B\omega_0}{34}$$

$$\frac{C_1}{3} + \frac{1}{m\omega_0^2} \frac{12B}{34} = \frac{2\sqrt{2}}{3} C_2$$

$$\frac{1}{3} \left(\frac{1}{m\omega_0^2} \left[\frac{3A}{2} + \frac{B}{34} \right] \right) + \frac{1}{m\omega_0^2} \frac{12B}{34} = \frac{2\sqrt{2}}{3} C_2$$

$$\frac{1}{m\omega_0^2} \left[\frac{A}{2} + \frac{B}{102} + \frac{12B}{34} \right] = \frac{2\sqrt{2}}{3} C_2$$

$$\frac{1}{m\omega_0^2} \frac{3}{2\sqrt{2}} \left[\frac{A}{2} + \frac{B}{102} + \frac{12B}{34} \right] = C_2$$

$$\frac{1}{m\omega_0^2} \frac{3\sqrt{2}}{4} \left[\frac{A}{2} + \frac{B}{102} + \frac{12B}{34} \right] = C_2$$

$$\frac{1}{m\omega_0^2} \left[\frac{3\sqrt{2}}{8} A + \frac{\sqrt{2}}{136} B + \frac{36\sqrt{2}}{136} B \right] = C_2$$

$$\frac{1}{m\omega_0^2} \left[\frac{3\sqrt{2}}{8} A + \frac{37\sqrt{2}}{136} B \right] = C_2$$

$$x(t) = \frac{1}{m\omega_0^2} \left[e^{-\frac{\omega_0}{3}t} \left[\left(\frac{3}{2} A + \frac{B}{34} \right) \cos \frac{2\sqrt{2}}{3} \omega_0 t + \left(\frac{3\sqrt{2}}{8} A + \frac{37\sqrt{2}}{136} B \right) \sin \frac{2\sqrt{2}}{3} \omega_0 t \right] - \frac{3A}{2} \cos \omega_0 t - \frac{B}{34} \cos 3\omega_0 t - \frac{2B}{17} \sin 3\omega_0 t \right]$$

$$b) x(t) = \frac{1}{m\omega_b^2} \left[-\frac{3A}{2} \cos \omega t - \frac{B}{34} (\cos 3\omega t + 4 \sin 3\omega t) \right], t > 0$$

$$\frac{3A}{2} \cos \omega t = \frac{B}{34} (\cos 3\omega t + 4 \sin 3\omega t)$$

$$\frac{B}{A} = \frac{51 \cos \omega t}{\cos 3\omega t + 4 \sin 3\omega t}$$

2-59

$$m\ddot{x} + b\dot{x} + kx = F_0 - F_0 e^{-at}, \quad k = ma^2, b = 2ma$$

$$\ddot{x} + \frac{b}{m}\dot{x} + \frac{k}{m}x = \frac{F_0}{m} - \frac{F_0}{m}e^{-at}$$

$$\ddot{x} + 2a\dot{x} + a^2x = \frac{F_0}{m} - \frac{F_0}{m}e^{-at}$$

$$x_h: \ddot{x} + 2a\dot{x} + a^2x = 0 \quad x = e^{pt}$$

$$p^2 + 2ap + a^2 = 0$$

$$p = \frac{-2a \pm \sqrt{4a^2 - 4a^2}}{2}$$

$$= -a$$

$$x_h = C_1 e^{-at} + C_2 t e^{-at}$$

$$x_p = K_1$$

$$a^2 K_1 = \frac{F_0}{m}$$

$$K_1 = \frac{F_0}{ma^2}$$

$$x_1 = (C_1 + C_2 t) e^{-at} + \frac{F_0}{ma^2}$$

$$0 = x(0) = C_1 + \frac{F_0}{ma^2}$$

$$C_1 = -\frac{F_0}{ma^2}$$

$$\dot{x}_1 = -a(C_1 + C_2 t) e^{-at} + C_2 e^{-at}$$

$$0 = \dot{x}(0) = -aC_1 + C_2$$

$$C_2 = aC_1$$

$$= -\frac{F_0}{ma}$$

$$x_1 = -\frac{F_0}{ma} \left(\frac{1}{a} + t \right) e^{-at} + \frac{F_0}{ma^2}$$

$$x_1 = K_1 e^{-at} + K_2 t e^{-at}$$

$$x_{p2} = K_3 t^2 e^{-at} \quad \{\text{guess method}\}$$

$$\dot{x}_{p2} = -a K_3 t^2 e^{-at} + 2 K_3 t e^{-at}$$

$$\begin{aligned} \ddot{x}_{p2} &= a^2 K_3 t^2 e^{-at} - 2a K_3 t e^{-at} - 2a K_3 t e^{-at} + 2 K_3 e^{-at} \\ &= a^2 K_3 t^2 e^{-at} - 4a K_3 t e^{-at} + 2 K_3 e^{-at} \end{aligned}$$

$$\ddot{x} + 2a\dot{x} + a^2 x = -\frac{F_0}{m} e^{-at}$$

$$a^2 K_3 t^2 - 4a K_3 t + 2 K_3 + 2a(-a K_3 t^2 e^{-at} + 2 K_3 t e^{-at}) + a^2 K_3 t^2 = -\frac{F_0}{m}$$

$$t^2(a^2 K_3 - 2a^2 K_3 + a^2 K_3) + t(-4a K_3 + 4a K_3) + 2 K_3 = -\frac{F_0}{m}$$

$$K_3 = -\frac{F_0}{2m}$$

$$x_2 = K_1 e^{-at} + K_2 t e^{-at} - \frac{F_0}{2m} t^2 e^{-at}$$

$$0 = x_2(0) = K_1$$

$$\dot{x}_2 = -a K_2 t e^{-at} + K_2 e^{-at} + \frac{F_0 a}{2m} t^2 e^{-at} - \frac{F_0 t}{2m} e^{-at}$$

$$0 = \dot{x}_2(0) = K_2$$

$$x_2 = -\frac{F_0}{2m} t^2 e^{-at}$$

$$x = x_1 + x_2$$

$$= -\frac{F_0}{ma} \left(\frac{1}{a} + t \right) e^{-at} + \frac{F_0}{ma^2} - \frac{F_0}{2m} t^2 e^{-at}$$

$$= -\frac{F_0}{ma^2} e^{-at} - \frac{F_0}{ma} t e^{-at} + \frac{F_0}{ma^2} - \frac{F_0}{2m} t^2 e^{-at}$$

$$x = \frac{F_0}{ma^2} \left[1 - \left(1 + at + \frac{a^2}{2} t^2 \right) e^{-at} \right]$$

2-61

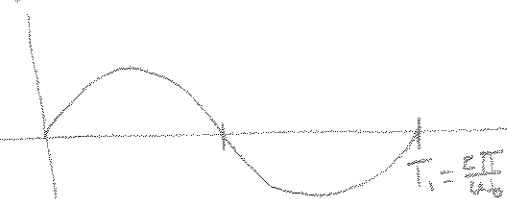
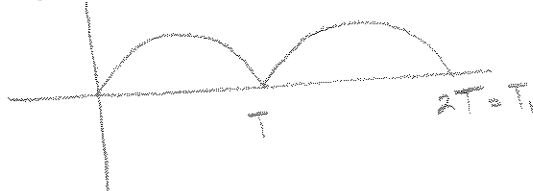
$$\ddot{x} + \omega_0^2 x = F_0 |\sin \omega_0 t|$$

$$F(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos \frac{n\pi t}{a} \quad \left\{ \begin{array}{l} \text{period} = 2a \\ b_n = 0 \text{ } \{ \text{even function} \} \end{array} \right.$$

$$a_n = \frac{1}{a} \int_{-a}^a F(t) \cos \frac{n\pi t}{a} dt, \quad \text{period of rectified sine is one half of sine}$$

$$= \frac{2F_0}{T} \int_0^T \sin \frac{\pi t}{T} \cos \frac{2n\pi t}{T} dt$$

$$T = \frac{T_1}{2} = \frac{\pi}{\omega_0} = 2a$$

sin $\omega_0 t$ |sin $\omega_0 t$ |

$$= \frac{2F_0}{T} \int_0^T \left(\frac{e^{i\pi t/T} - e^{-i\pi t/T}}{2i} \right) \left(\frac{e^{i2n\pi t/T} + e^{-i2n\pi t/T}}{2} \right) dt$$

$$= \frac{F_0}{2Ti} \int_0^T \left[e^{i\pi t/T(1+2n)} - e^{i\pi t/T(2n-1)} + e^{i\pi t/T(1-2n)} - e^{-i\pi t/T(1+2n)} \right] dt$$

$$= \frac{F_0}{2Ti} \left[\frac{e^{i\pi t/T(1+2n)}}{i\pi(1+2n)/T} - \frac{e^{i\pi t/T(2n-1)}}{i\pi(2n-1)/T} + \frac{e^{i\pi t/T(1-2n)}}{i\pi(1-2n)/T} + \frac{e^{-i\pi t/T(1+2n)}}{i\pi(1+2n)/T} \right] \Big|_0^T$$

$$= -\frac{F_0}{2i\pi} \left[\frac{e^{i\pi(1+2n)}}{1+2n} - \frac{e^{i\pi(2n-1)}}{2n-1} + \frac{e^{i\pi(1-2n)}}{1-2n} + \frac{e^{-i\pi(1+2n)}}{1+2n} \right]$$

$$\left(\frac{1}{1+2n} - \frac{1}{2n-1} + \frac{1}{1-2n} + \frac{1}{1+2n} \right), \quad \begin{array}{l} e^{-i\pi} = -1 = e^{-i\pi} \\ e^{i2\pi n} = 1 = e^{-i2\pi n} \end{array}$$

$$= -\frac{F_0}{2i\pi} \left[\frac{-1}{1+2n} + \frac{1}{2n-1} - \frac{1}{1-2n} - \frac{1}{1+2n} - \frac{1}{1+2n} + \frac{1}{2n-1} - \frac{1}{1-2n} - \frac{1}{1+2n} \right]$$

$$= -\frac{F_0}{2i\pi} \left[\frac{-2}{1+2n} + \frac{2}{2n-1} - \frac{2}{1-2n} - \frac{2}{1+2n} \right]$$

$$= -\frac{F_0}{2i\pi} \left[\frac{-4}{1+2n} - \frac{4}{1-2n} \right]$$

$$= \frac{2F_0}{i\pi} \left[\frac{1}{1+2n} + \frac{1}{1-2n} \right]$$

$$= \frac{2F_0}{i\pi} \left[\frac{1-2n+1+2n}{4n^2-1} \right]$$

$$= -\frac{2F_0}{\pi} \left[\frac{2}{4n^2-1} \right]$$

$$a_n = -\frac{4F_0}{\pi} \frac{1}{4n^2-1}$$

$$a_0 = \frac{1}{2a} \int_{-a}^a f(t) dt \quad a = \frac{T}{2}$$

$$= \frac{F_0}{T} \int_0^T \sin \frac{\pi t}{T} dt$$

$$= \frac{F_0}{T} \left[-\frac{T}{\pi} \cos \frac{\pi t}{T} \right]_0^T$$

$$= -\frac{F_0}{\pi} [\cos \pi - \cos 0]$$

$$= -\frac{F_0}{\pi} [-1 - 1]$$

$$= \frac{2F_0}{\pi}$$

$$F(t) = \frac{2F_0}{\pi} - \frac{4F_0}{\pi} \sum_{n=1}^{\infty} \frac{1}{4n^2-1} \cos \frac{2\pi n t}{T}$$

$$x(t) = A_0 + \sum_{n=1}^{\infty} A_n \cos \frac{2\pi n t}{T} + B_n \sin \frac{2\pi n t}{T}$$

$$\dot{x}(t) = \sum_{n=1}^{\infty} -\frac{2\pi n}{T} A_n \sin \frac{2\pi n t}{T} + \frac{2\pi n}{T} B_n \cos \frac{2\pi n t}{T}$$

$$\ddot{x}(t) = \sum_{n=1}^{\infty} -\left(\frac{2\pi n}{T}\right)^2 A_n \cos \frac{2\pi n t}{T} - \left(\frac{2\pi n}{T}\right)^2 B_n \sin \frac{2\pi n t}{T}$$

$$\ddot{x} + \omega_0^2 x = F(t)$$

$$\sum_{n=1}^{\infty} \left(-\left(\frac{2\pi n}{T}\right)^2 A_n \cos \frac{2\pi n t}{T} - \left(\frac{2\pi n}{T}\right)^2 B_n \sin \frac{2\pi n t}{T} \right) + \omega_0^2 \left(\sum_{n=1}^{\infty} A_n \cos \frac{2\pi n t}{T} + B_n \sin \frac{2\pi n t}{T} \right) + A_0 =$$

$$\frac{2F_0}{\pi} - \frac{4F_0}{\pi} \sum_{n=1}^{\infty} \frac{1}{4n^2-1} \cos \frac{2\pi n t}{T}$$

Equating terms!

$$\omega_0^2 A_0 = \frac{2F_0}{\pi} \rightarrow A_0 = \frac{2F_0}{\pi \omega_0^2}$$

$$-\left(\frac{2\pi n}{T}\right)^2 A_n + \omega_0^2 A_n = -\frac{4F_0}{\pi} \frac{1}{4n^2-1}$$

$$\omega_0 = \frac{\pi}{T}$$

$$-(2\omega_0)^2 A_n + \omega_0^2 A_n = -\frac{4F_0}{\pi} \frac{1}{4n^2-1}$$

$$-4\omega_0^2 n^2 A_n + \omega_0^2 A_n = -\frac{4F_0}{\pi} \frac{1}{4n^2-1}$$

$$A_n \omega_0^2 (4n^2-1) = \frac{4F_0}{\pi} \frac{1}{4n^2-1}$$

$$A_n = \frac{4F_0}{\pi \omega_0^2} \frac{1}{(4n^2-1)^2}$$

$$x(t) = A_0 + \sum_{n=1}^{\infty} A_n \cos \frac{2\pi n t}{T}$$

$$x(t) = \frac{2F_0}{\pi \omega_0^2} + \frac{4F_0}{\pi \omega_0^2} \sum_{n=1}^{\infty} \frac{\cos 2n\omega_0 t}{(4n^2-1)^2}$$

3-1

a) Prove: $c(\vec{A} + \vec{B}) = c\vec{A} + c\vec{B}$

$$\vec{A} = A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$$

$$\vec{B} = B_x \hat{x} + B_y \hat{y} + B_z \hat{z}$$

$$\vec{A} + \vec{B} = (A_x + B_x) \hat{x} + (A_y + B_y) \hat{y} + (A_z + B_z) \hat{z}$$

$$c(\vec{A} + \vec{B}) = c(A_x + B_x) \hat{x} + c(A_y + B_y) \hat{y} + c(A_z + B_z) \hat{z}$$

$$= cA_x \hat{x} + cA_y \hat{y} + cA_z \hat{z} + cB_x \hat{x} + cB_y \hat{y} + cB_z \hat{z}$$

$$= c(A_x \hat{x} + A_y \hat{y} + A_z \hat{z}) + c(B_x \hat{x} + B_y \hat{y} + B_z \hat{z})$$

$$c(\vec{A} + \vec{B}) = c\vec{A} + c\vec{B}$$

b) $\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$

$$\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot ((B_x + C_x) \hat{x} + (B_y + C_y) \hat{y} + (B_z + C_z) \hat{z})$$

$$= (A_x \hat{x} + A_y \hat{y} + A_z \hat{z}) \cdot ((B_x + C_x) \hat{x} + (B_y + C_y) \hat{y} + (B_z + C_z) \hat{z})$$

$$= A_x(B_x + C_x) + A_y(B_y + C_y) + A_z(B_z + C_z)$$

$$= A_x B_x + A_y B_y + A_z B_z + A_x C_x + A_y C_y + A_z C_z$$

$$\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$$

c) $\vec{A} \times (\vec{B} + \vec{C}) = (\vec{A} \times \vec{B}) + (\vec{A} \times \vec{C})$

$$\vec{A} \times (\vec{B} + \vec{C}) = \vec{A} \times ((B_x + C_x) \hat{x} + (B_y + C_y) \hat{y} + (B_z + C_z) \hat{z})$$

$$= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ B_x + C_x & B_y + C_y & B_z + C_z \end{vmatrix}$$

$$= \hat{x}(A_y(B_z + C_z) - A_z(B_y + C_y)) + \hat{y}(A_z(B_x + C_x) - A_x(B_z + C_z)) + \hat{z}(A_x(B_y + C_y) - A_y(B_x + C_x))$$

$$= \hat{x}(A_y B_z - A_z B_y + A_y C_z - A_z C_y) +$$

$$\hat{y}(A_z B_x - A_x B_z + A_z C_x - A_x C_z) +$$

$$\hat{z}(A_x B_y - A_y B_x + A_x C_y - A_y C_x)$$

$$= \hat{x}(A_y B_z - A_z B_y) + \hat{y}(A_z B_x - A_x B_z) + \hat{z}(A_x B_y - A_y B_x) + \\ \hat{x}(A_y C_z - A_z C_y) + \hat{y}(A_z C_x - A_x C_z) + \hat{z}(A_x C_y - A_y C_x)$$

$$\vec{A} \times (\vec{B} + \vec{C}) = \vec{A} \times \vec{B} + \vec{A} \times \vec{C}$$

$$d) \vec{A} \times (\vec{B} \times \vec{C}) = \vec{B}(\vec{A} \cdot \vec{C}) - \vec{C}(\vec{A} \cdot \vec{B})$$

$$\vec{A} \times (\vec{B} \times \vec{C}) = \vec{A} \times ((B_y C_z - B_z C_y)\hat{x} + (B_z C_x - B_x C_z)\hat{y} + (B_x C_y - B_y C_x)\hat{z})$$

$$= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ (B_y C_z - B_z C_y) & (B_z C_x - B_x C_z) & (B_x C_y - B_y C_x) \end{vmatrix}$$

$$= \hat{x} [A_y (B_x C_y - B_y C_x) - A_z (B_z C_x - B_x C_z)] + \\ \hat{y} [A_z (B_y C_z - B_z C_y) - A_x (B_x C_y - B_y C_x)] + \\ \hat{z} [A_x (B_z C_x - B_x C_z) - A_y (B_y C_z - B_z C_y)]$$

$$= \hat{x} [B_x (A_y C_y) - C_x (A_y B_y) - C_x (A_z B_z) + B_x (A_z C_z)] + \\ \hat{y} [B_y (A_z C_z) - C_y (A_z B_z) - C_y (A_x B_x) + B_y (A_x C_x)] + \\ \hat{z} [B_z (A_x C_x) - C_z (A_x B_x) - C_z (A_y B_y) + B_z (A_y C_y)]$$

$$= \hat{x} [B_x (A_y C_y + A_z C_z) - C_x (A_y B_y + A_z B_z)] + \\ \hat{y} [B_y (A_z C_z + A_x C_x) - C_y (A_z B_z + A_x B_x)] + \\ \hat{z} [B_z (A_x C_x + A_y C_y) - C_z (A_x B_x + A_y B_y)]$$

$$= \hat{x} [B_x (A_x C_x + A_y C_y + A_z C_z - A_x C_x) - C_x (A_x B_x + A_y B_y + A_z B_z - A_x B_x)] + \\ \hat{y} [B_y (A_x C_x + A_y C_y + A_z C_z - A_y C_y) - C_y (A_x B_x + A_y B_y + A_z B_z - A_y B_y)] + \\ \hat{z} [B_z (A_x C_x + A_y C_y + A_z C_z - A_z C_z) - C_z (A_x B_x + A_y B_y + A_z B_z - A_z B_z)]$$

$$= \hat{x} [B_x(\vec{A} \cdot \vec{C}) - A_x C_x] - C_x[(\vec{A} \cdot \vec{B}) + A_x B_x] + \\
\hat{y} [B_y(\vec{A} \cdot \vec{C}) - A_y C_y] - C_y[(\vec{A} \cdot \vec{B}) + A_y B_y] + \\
\hat{z} [B_z(\vec{A} \cdot \vec{C}) - A_z C_z] - C_z[(\vec{A} \cdot \vec{B}) + A_z B_z]$$

$$= \hat{x} [B_x(\vec{A} \cdot \vec{C}) - A_x B_x C_x - C_x(\vec{A} \cdot \vec{B}) + A_x B_x C_x] + \\
\hat{y} [B_y(\vec{A} \cdot \vec{C}) - A_y B_y C_y - C_y(\vec{A} \cdot \vec{B}) + A_y B_y C_y] + \\
\hat{z} [B_z(\vec{A} \cdot \vec{C}) - A_z B_z C_z - C_z(\vec{A} \cdot \vec{B}) + A_z B_z C_z]$$

$$\vec{A} \times (\vec{B} \times \vec{C}) = \vec{B}(\vec{A} \cdot \vec{C}) - \vec{C}(\vec{A} \cdot \vec{B})$$

3-3 Prove $\vec{A} \times \vec{B} = (A_y B_z - A_z B_y, A_z B_x - A_x B_z, A_x B_y - A_y B_x)$

$$\vec{A} = A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$$

$$\vec{B} = B_x \hat{x} + B_y \hat{y} + B_z \hat{z}$$

$$\vec{A} \times \vec{B} = \vec{A} \times (B_x \hat{x} + B_y \hat{y} + B_z \hat{z})$$

$$= \vec{A} \times B_x \hat{x} + \vec{A} \times B_y \hat{y} + \vec{A} \times B_z \hat{z}$$

$$= (A_x \hat{x} + A_y \hat{y} + A_z \hat{z}) \times B_x \hat{x} + (A_x \hat{x} + A_y \hat{y} + A_z \hat{z}) \times B_y \hat{y} + (A_x \hat{x} + A_y \hat{y} + A_z \hat{z}) \times B_z \hat{z}$$

$$= A_x \hat{x} \times B_x \hat{x} + A_y \hat{y} \times B_x \hat{x} + A_z \hat{z} \times B_x \hat{x} + \{ \vec{A} \times (\vec{B} + \vec{C}) = \vec{A} \times \vec{B} + \vec{A} \times \vec{C} \}$$

$$+ A_x \hat{x} \times B_y \hat{y} + A_y \hat{y} \times B_y \hat{y} + A_z \hat{z} \times B_y \hat{y} +$$

$$+ A_x \hat{x} \times B_z \hat{z} + A_y \hat{y} \times B_z \hat{z} + A_z \hat{z} \times B_z \hat{z}$$

$$= \vec{0} + A_y B_x (\hat{y} \times \hat{x}) + A_z B_x (\hat{z} \times \hat{x}) + \{ |\vec{A} \times \vec{B}| = AB, (\vec{A}) \times \vec{B} = \vec{A} \times (c\vec{B}) =$$

$$+ A_x B_y (\hat{x} \times \hat{y}) + \vec{0} + A_z B_y (\hat{z} \times \hat{y}) + c(\vec{A} \times \vec{B}) \}$$

$$+ A_x B_z (\hat{x} \times \hat{z}) + A_y B_z (\hat{y} \times \hat{z}) + \vec{0}$$

$$= -A_y B_x \hat{z} + A_z B_x \hat{y} + \{ \vec{A} \times \vec{B} = -\vec{B} \times \vec{A}, \hat{x} \times \hat{x} = \hat{y} \times \hat{y} = \hat{z} \times \hat{z} = \vec{0},$$

$$+ A_x B_y \hat{z} - A_z B_y \hat{x} +$$

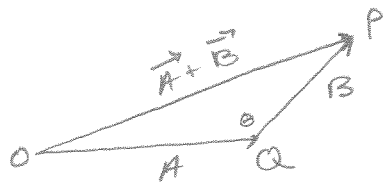
$$- A_x B_z \hat{y} + A_y B_z \hat{x}$$

$$= (A_y B_z - A_z B_y) \hat{x} + (A_z B_x - A_x B_z) \hat{y} + (A_x B_y - A_y B_x) \hat{z}$$

$$\vec{A} \times \vec{B} = (A_y B_z - A_z B_y, A_z B_x - A_x B_z, A_x B_y - A_y B_x)$$

3-5 a) Prove $|\vec{A} + \vec{B}| \leq |\vec{A}| + |\vec{B}|$

Geometric Proof:



The shortest distance between O and P is a straight line.
The length $|\vec{A} + \vec{B}|$ is the shortest distance. Any other path,
O-Q-P has a length of $|\vec{A}| + |\vec{B}|$. If Q is on $\vec{OP}$ then
 $|\vec{A}| + |\vec{B}| = |\vec{A} + \vec{B}|$ otherwise $|\vec{A}| + |\vec{B}| > |\vec{A} + \vec{B}|$.

Algebraic Proof:

$$|\vec{A}| = \sqrt{A_x^2 + A_y^2}$$

$$|\vec{B}| = \sqrt{B_x^2 + B_y^2}$$

$$|\vec{A} + \vec{B}| = \sqrt{(A_x + B_x)^2 + (A_y + B_y)^2}$$

$$|\vec{A}| + |\vec{B}| = \sqrt{A_x^2 + A_y^2} + \sqrt{B_x^2 + B_y^2}$$

$$(|\vec{A} + \vec{B}|)^2 = (A_x + B_x)^2 + (A_y + B_y)^2$$

$$(|\vec{A}| + |\vec{B}|)^2 = A_x^2 + A_y^2 + B_x^2 + B_y^2 + 2\sqrt{(A_x^2 + A_y^2)(B_x^2 + B_y^2)}$$

$$\begin{aligned} (|\vec{A} + \vec{B}|)^2 &= A_x^2 + 2A_x B_x + B_x^2 + A_y^2 + 2A_y B_y + B_y^2 \\ &= A_x^2 + A_y^2 + B_x^2 + B_y^2 + 2A_x B_x + 2A_y B_y \end{aligned}$$

$$\begin{aligned} (|\vec{A}| + |\vec{B}|)^2 - (|\vec{A} + \vec{B}|)^2 &= 2\sqrt{(A_x^2 + A_y^2)(B_x^2 + B_y^2)} - 2(A_x B_x + A_y B_y) \\ &= 2\sqrt{(A_x B_x)^2 + (A_x B_y)^2 + (A_y B_x)^2 + (A_y B_y)^2} - 2(A_x B_x + A_y B_y) \end{aligned}$$

Compare the difference terms:

$$2\sqrt{(A_x B_x)^2 + (A_x B_y)^2 + (A_y B_x)^2 + (A_y B_y)^2} \stackrel{?}{=} 2(A_x B_x + A_y B_y)$$

$$\begin{aligned} (A_x B_x)^2 + (A_x B_y)^2 + (A_y B_x)^2 + (A_y B_y)^2 &\stackrel{?}{=} (A_x B_x + A_y B_y)^2 \\ &\stackrel{?}{=} (A_x B_x)^2 + 2(A_x A_y B_x B_y) + (A_y B_y)^2 \end{aligned}$$

$$(A_x B_y)^2 + (A_y B_x)^2 \stackrel{?}{=} 2A_x A_y B_x B_y$$

$$\frac{(A_x B_y)^2 + (A_y B_x)^2}{A_x A_y B_x B_y} \stackrel{?}{=} 2$$

$$\frac{A_x B_y}{A_y B_x} + \frac{A_y B_x}{A_x B_y} \stackrel{?}{=} 2$$

(2)

Let $B_x = \alpha A_x$ and $B_y = \gamma A_y$

$$\frac{A_x \gamma A_y}{A_y \alpha A_x} + \frac{A_y \alpha A_x}{A_x \gamma A_y} \stackrel{?}{=} 2$$

$$\frac{\gamma}{\alpha} + \frac{\alpha}{\gamma} \stackrel{?}{=} 2$$

$$\gamma^2 + \alpha^2 \stackrel{?}{=} 2\alpha\gamma$$

$$\gamma^2 - 2\alpha\gamma + \alpha^2 \stackrel{?}{=} 0$$

$$(\gamma - \alpha)^2 \stackrel{?}{=} 0$$

$$(\gamma - \alpha)^2 \geq 0$$

So,

$$\gamma^2 - 2\alpha\gamma + \alpha^2 \geq 0$$

$$\frac{\gamma^2 + \alpha^2}{\alpha\gamma} \geq 2$$

$$\frac{\gamma}{\alpha} + \frac{\alpha}{\gamma} \geq 2$$

Therefore,

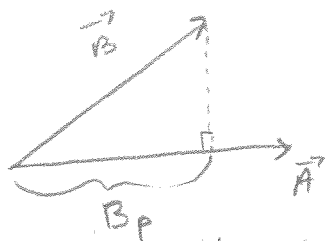
$$(|\vec{A}| + |\vec{B}|)^2 - (|\vec{A} + \vec{B}|)^2 \geq 0$$

and

$$|\vec{A}| + |\vec{B}| \geq |\vec{A} + \vec{B}|.$$

b) $|\vec{A} \cdot \vec{B}| \leq |\vec{A}| |\vec{B}|$

Geometric Proof:



$|\vec{A} \cdot \vec{B}| = |\vec{A}| |B_p|$ where B_p is the projection of $\vec{B}$ on $\vec{A}$. $B_p \leq |\vec{B}|$ since B_p is a leg of a right triangle with hypotenuse $|\vec{B}|$. So, $|\vec{A}| |B_p| \leq |\vec{A}| |\vec{B}|$.
Using substitution $|\vec{A} \cdot \vec{B}| \leq |\vec{A}| |\vec{B}|$

Algebraic Proof:

3

$$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta$$

$$|\vec{A} \cdot \vec{B}| = |\vec{A}| |\vec{B}| |\cos \theta|$$

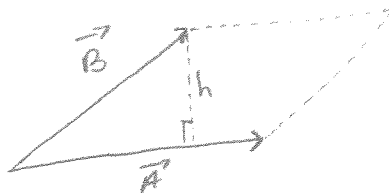
$$|\cos \theta| \leq 1 \rightarrow |\vec{A}| |\vec{B}| |\cos \theta| \leq |\vec{A}| |\vec{B}|$$

Therefore, by substitution

$$|\vec{A} \cdot \vec{B}| \leq |\vec{A}| |\vec{B}|$$

c) $|\vec{A} \times \vec{B}| \leq |\vec{A}| |\vec{B}|$

Geometric Proof:



$|\vec{A} \times \vec{B}| = h |\vec{A}|$. Since h is a leg of a right triangle with hypotenuse $|\vec{B}|$ then

$h \leq |\vec{B}|$. So, $h |\vec{A}| \leq |\vec{A}| |\vec{B}|$. Using substitution

$$|\vec{A} \times \vec{B}| \leq |\vec{A}| |\vec{B}|$$

Algebraic Proof:

$$\vec{A} \times \vec{B} = |\vec{A}| |\vec{B}| \sin \theta$$

$$|\vec{A} \times \vec{B}| = |\vec{A}| |\vec{B}| |\sin \theta|$$

$$|\sin \theta| \leq 1 \rightarrow |\vec{A}| |\vec{B}| |\sin \theta| \leq |\vec{A}| |\vec{B}|$$

Therefore, by substitution

$$|\vec{A} \times \vec{B}| \leq |\vec{A}| |\vec{B}|$$

3-7 i) Prove

$$\frac{d}{dt}(\vec{A} + \vec{B}) = \frac{d\vec{A}}{dt} + \frac{d\vec{B}}{dt}$$

Defn: $\frac{d\vec{A}}{dt} = \lim_{\Delta t \rightarrow 0} \frac{\vec{A}(t+\Delta t) - \vec{A}(t)}{\Delta t}$

$$\begin{aligned} \frac{d}{dt}(\vec{A} + \vec{B}) &= \lim_{\Delta t \rightarrow 0} \frac{(\vec{A}(t+\Delta t) + \vec{B}(t+\Delta t)) - [\vec{A}(t) + \vec{B}(t)]}{\Delta t} \\ &= \lim_{\Delta t \rightarrow 0} \frac{\vec{A}(t+\Delta t) - \vec{A}(t) + \vec{B}(t+\Delta t) - \vec{B}(t)}{\Delta t} \\ &= \lim_{\Delta t \rightarrow 0} \frac{\vec{A}(t+\Delta t) - \vec{A}(t)}{\Delta t} + \lim_{\Delta t \rightarrow 0} \frac{\vec{B}(t+\Delta t) - \vec{B}(t)}{\Delta t} \end{aligned}$$

$$\frac{d}{dt}(\vec{A} + \vec{B}) = \frac{d\vec{A}}{dt} + \frac{d\vec{B}}{dt}$$

ii) Prove

$$\frac{d}{dt}(f\vec{A}) = \frac{df}{dt}\vec{A} + f\frac{d\vec{A}}{dt}$$

Defn: $\frac{d\vec{A}}{dt} = \lim_{\Delta t \rightarrow 0} \frac{\vec{A}(t+\Delta t) - \vec{A}(t)}{\Delta t}$

$$\begin{aligned} \frac{d}{dt}(f\vec{A}) &= \lim_{\Delta t \rightarrow 0} \frac{f(t+\Delta t)\vec{A}(t+\Delta t) - f(t)\vec{A}(t)}{\Delta t} \\ &= \lim_{\Delta t \rightarrow 0} \frac{f(t+\Delta t)\vec{A}(t+\Delta t) - f(t+\Delta t)\vec{A}(t) + f(t+\Delta t)\vec{A}(t) - f(t)\vec{A}(t)}{\Delta t} \\ &= \lim_{\Delta t \rightarrow 0} \frac{f(t+\Delta t)[\vec{A}(t+\Delta t) - \vec{A}(t)] + \vec{A}(t)[f(t+\Delta t) - f(t)]}{\Delta t} \\ &= \lim_{\Delta t \rightarrow 0} \frac{f(t+\Delta t)[\vec{A}(t+\Delta t) - \vec{A}(t)]}{\Delta t} + \lim_{\Delta t \rightarrow 0} \frac{\vec{A}(t)[f(t+\Delta t) - f(t)]}{\Delta t} \\ &= \lim_{\Delta t \rightarrow 0} f(t+\Delta t) \lim_{\Delta t \rightarrow 0} \frac{\vec{A}(t+\Delta t) - \vec{A}(t)}{\Delta t} + \lim_{\Delta t \rightarrow 0} \vec{A}(t) \lim_{\Delta t \rightarrow 0} \frac{f(t+\Delta t) - f(t)}{\Delta t} \end{aligned}$$

$$\frac{d}{dt}(f\vec{A}) = f\frac{d\vec{A}}{dt} + \vec{A}\frac{df}{dt}$$

3-9

Defn: $\int_{t_1}^{t_2} \vec{A}(t) dt = \lim_{n \rightarrow \infty} \sum_{i=1}^n \vec{A}(t_i) \Delta t_i, \quad \Delta t_i = \frac{t_2 - t_1}{n}$

$$\int_{t_1}^{t_2} \vec{A}(t) dt = \hat{x} \int_{t_1}^{t_2} A_x dt + \hat{y} \int_{t_1}^{t_2} A_y dt + \hat{z} \int_{t_1}^{t_2} A_z dt$$

Analogous equations (3.54) - (3.57):

$$\begin{aligned} 3.54: \int_{t_1}^{t_2} (\vec{A} + \vec{B}) dt &= \lim_{n \rightarrow \infty} \sum_{i=1}^n (\vec{A}(t_i) + \vec{B}(t_i)) \Delta t_i \\ &= \lim_{n \rightarrow \infty} \sum_{i=1}^n \vec{A}(t_i) \Delta t_i + \lim_{n \rightarrow \infty} \sum_{i=1}^n \vec{B}(t_i) \Delta t_i \\ &= \int_{t_1}^{t_2} \vec{A}(t) dt + \int_{t_1}^{t_2} \vec{B}(t) dt \end{aligned}$$

$$3.55: \int_{t_1}^{t_2} f \vec{A} dt = \lim_{n \rightarrow \infty} \sum_{i=1}^n f(t_i) \vec{A}(t_i) \Delta t_i$$

$$\text{Let } \vec{G}(t) = f \vec{A}(t)$$

$$\begin{aligned} \int_{t_1}^{t_2} f \vec{A} dt &= \lim_{n \rightarrow \infty} \sum_{i=1}^n \vec{G}(t_i) \Delta t_i \\ &= \int_{t_1}^{t_2} \vec{G}(t) dt = \hat{x} \int_{t_1}^{t_2} f A_x dt + \hat{y} \int_{t_1}^{t_2} f A_y dt + \hat{z} \int_{t_1}^{t_2} f A_z dt \end{aligned}$$

$$3.56: \int_{t_1}^{t_2} (\vec{A} \cdot \vec{B}) dt = \int_{t_1}^{t_2} A_x B_x dt + \int_{t_1}^{t_2} A_y B_y dt + \int_{t_1}^{t_2} A_z B_z dt$$

$$3.57: \int_{t_1}^{t_2} (\vec{A} \times \vec{B}) dt = \int_{t_1}^{t_2} \vec{C} dt = \hat{x} \int_{t_1}^{t_2} (A_y B_z - B_y A_z) dt + \hat{y} \int_{t_1}^{t_2} (A_z B_x - A_x B_z) dt + \hat{z} \int_{t_1}^{t_2} (A_x B_y - A_y B_x) dt$$

Prove: $\frac{d}{dt} \int_0^t \vec{A}(t) dt = \vec{A}(t)$

$\vec{A}(t)$ is continuous. Then

$$\vec{a}(t) = \int_0^t \vec{A}(t) dt$$

Must show

$$\frac{d\vec{a}}{dt} = \vec{A}(t).$$

$$\vec{a}(t+\Delta t) = \int_0^{t+\Delta t} \vec{A}(t) dt$$

$$\begin{aligned}\vec{a}(t+\Delta t) - \vec{a}(t) &= \int_0^{t+\Delta t} \vec{A}(t) dt - \int_0^t \vec{A}(t) dt \\ &= \int_t^{t+\Delta t} \vec{A}(t) dt\end{aligned}$$

The Mean Value Theorem states

$$\int_t^{t+\Delta t} \vec{A}(t) dt = \vec{A}(c) \Delta t \quad (\text{a value } A(c) \text{ is between } A(t+\Delta t) \text{ and } A(t))$$

$$\vec{a}(t+\Delta t) - \vec{a}(t) = \vec{A}(c) \Delta t$$

$$\frac{\vec{a}(t+\Delta t) - \vec{a}(t)}{\Delta t} = \vec{A}(c)$$

$$\lim_{\Delta t \rightarrow 0} \frac{\vec{a}(t+\Delta t) - \vec{a}(t)}{\Delta t} = \lim_{\Delta t \rightarrow 0} \vec{A}(c)$$

$$\frac{d\vec{a}}{dt} = \lim_{\Delta t \rightarrow 0} \vec{A}(c)$$

Since c is between t and $t+\Delta t$, and

$$\lim_{\Delta t \rightarrow 0} t = t, \quad \lim_{\Delta t \rightarrow 0} t+\Delta t = t$$

then

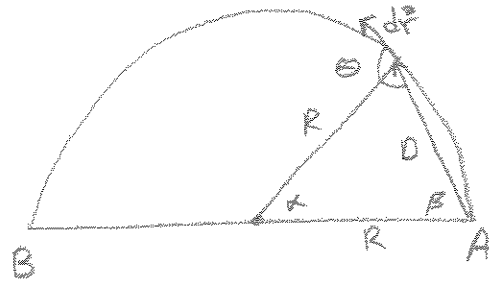
$$\lim_{\Delta t \rightarrow 0} c = t \quad \{ \text{squeeze theorem} \}$$

Finally,

$$\frac{d\vec{a}}{dt} = \lim_{\Delta t \rightarrow 0} \vec{A}(c)$$

$$\frac{d}{dt} \int_0^t \vec{A}(t) dt = \vec{A}(t)$$

3-11



$$F = -kD$$

$$D^2 = R^2 + R^2 - 2R^2 \cos \alpha$$

$$= 2R^2(1 - \cos \alpha)$$

$$D = \sqrt{2}R(1 - \cos \alpha)^{1/2}$$

$$= 2R \sin \frac{\alpha}{2}$$

$$\text{At } D = 2R \quad F = F_0$$

$$F_0 = -k2R$$

$$-k = \frac{F_0}{2R}$$

$$F = -\frac{F_0}{2R} D$$

$$= -\frac{F_0}{2R} 2R \sin \frac{\alpha}{2}$$

$$F = -F_0 \sin \frac{\alpha}{2}$$

$$W = \int_C \vec{F} \cdot d\vec{r}$$

$$= \int F \cos \theta ds$$

$$= -F_0 \int_0^\pi \sin \frac{\alpha}{2} \cos(\pi - \frac{\alpha}{2}) R d\alpha$$

$$= +F_0 R \int_0^\pi \sin \frac{\alpha}{2} \cos \frac{\alpha}{2} d\alpha$$

$$= F_0 R \left[\sin^2 \frac{\alpha}{2} \right]_0^\pi$$

$$W = F_0 R$$

$$\theta = \beta + \frac{\pi}{2}$$

$$2\beta + \alpha = \pi$$

$$\beta = \frac{\pi}{2} - \frac{\alpha}{2}$$

$$\theta = \pi - \frac{\alpha}{2}$$

$$d\vec{s} = \hat{r} dr$$

$$ds = R d\alpha$$

$$\sin^2 \gamma = \frac{1}{2}(1 - \cos 2\gamma)$$

$$\sin \gamma = \frac{1}{\sqrt{2}}(1 - \cos 2\gamma)^{1/2}$$

$$\sqrt{2} \sin \frac{\gamma}{2} = (1 - \cos \gamma)^{1/2}$$

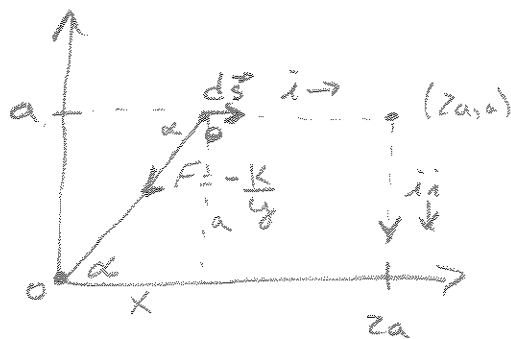
$$\int \sin \frac{\alpha}{2} \cos \frac{\alpha}{2} d\alpha = 2 \int u du$$

$$u = \sin \frac{\alpha}{2} = u^2 + C$$

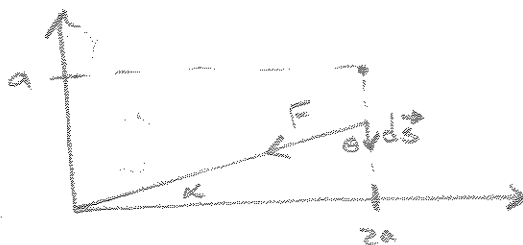
$$du = \frac{1}{2} \cos \frac{\alpha}{2} d\alpha$$

$$2du = \cos \frac{\alpha}{2} d\alpha$$

3-13 a)



$$\theta = \pi - \alpha \quad 0 \leq x \leq 2a, y = a$$



$$\theta = \frac{\pi}{2} - \alpha \quad a \leq y \leq 2a, x = 2a$$

$$\begin{aligned} i) \quad W &= \int \vec{F} \cdot d\vec{s} = \int |\vec{F}| \cos \theta ds \quad F = \frac{K}{y} \\ &= +K \int \frac{\cos \alpha}{y} ds \quad \cos \theta = \cos(\pi - \alpha) = \cos \pi \cos \alpha + \sin \pi \sin \alpha \\ &= -K \int_0^{2a} \frac{x dx}{y(a^2 + x^2)^{3/2}} \quad \{y = a\} \quad = -\cos \alpha \\ &= -\frac{K}{a} \int_0^{2a} \frac{x dx}{(a^2 + x^2)^{3/2}} \quad \cos \alpha = \frac{x}{(a^2 + x^2)^{1/2}} \\ &= -\frac{K}{a} (a^2 + x^2)^{1/2} \Big|_0^{2a} \quad \begin{aligned} u &= a^2 + x^2 \\ du &= 2x dx \\ \frac{du}{2} &= x dx \end{aligned} \quad \begin{aligned} \int \frac{x dx}{(a^2 + x^2)^{3/2}} &= \frac{1}{2} \int \frac{du}{u^{3/2}} \\ &= \frac{1}{2} \int u^{-3/2} du \\ &= -u^{-1/2} + C \end{aligned} \\ &= -\frac{K}{a} \left[(a^2 + 4a^2)^{1/2} - a \right] \\ &= -\frac{K}{a} (\sqrt{5}a - a) \\ &= -K(\sqrt{5} - 1) \\ &= K(1 - \sqrt{5}) \end{aligned}$$

$$ii) W = \int \vec{F} \cdot d\vec{z}$$

$$= \int F \cos \theta dy$$

$$= \int F \sin \alpha dy$$

$$= K \int_a^0 \frac{dy}{(4a^2 + y^2)^{1/2}}$$

$$= -K \ln \left| \frac{\sqrt{4a^2 + y^2}}{2a} + \frac{y}{2a} \right| \Big|_a^0$$

$$= K \left[\ln |1| - \ln \left| \frac{\sqrt{5a^2 + a^2}}{2a} \right| \right]$$

$$= K \ln \left(\frac{\sqrt{5a^2 + a^2}}{2a} \right)$$

$$= K \ln \frac{1}{2} (1 + \sqrt{5})$$

$$W = W_i + W_{ii}$$

$$W = K \left[1 - \sqrt{5} + \ln \frac{1}{2} (1 + \sqrt{5}) \right]$$

$$\cos \theta = \cos \left(\frac{\pi}{2} - \alpha \right)$$

$$= \cos \frac{\pi}{2} \cos \alpha + \sin \frac{\pi}{2} \sin \alpha$$

$$= \sin \alpha$$

$$\sin \alpha = \frac{y}{(4a^2 + y^2)^{1/2}}$$

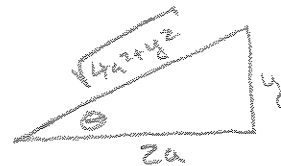
$$\int \frac{dy}{(4a^2 + y^2)^{1/2}} = \int \frac{2a \sec^2 \theta d\theta}{(4a^2 + 4a^2 \tan^2 \theta)^{1/2}}$$

$$y^2 = 4a^2 \tan^2 \theta = \int \frac{\sec^2 \theta d\theta}{(1 + \tan^2 \theta)^{1/2}}$$

$$y = 2a \tan \theta$$

$$dy = 2a \sec^2 \theta d\theta = \int \sec \theta d\theta$$

$$= \ln |\sec \theta + \tan \theta| + C$$

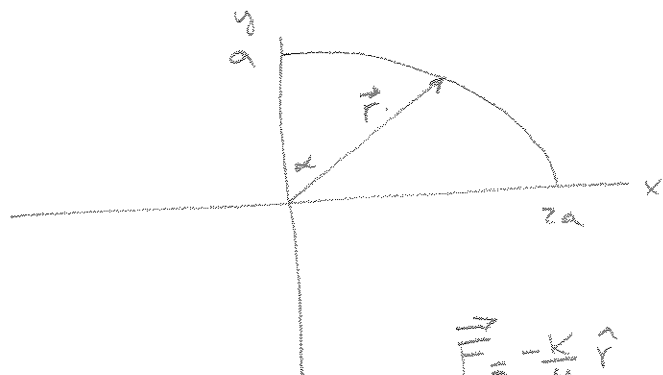


$$\tan \theta = \frac{y}{2a}$$

$$\sec \theta = \frac{\sqrt{4a^2 + y^2}}{2a}$$

$$= \ln \left| \frac{\sqrt{4a^2 + y^2}}{2a} + \frac{y}{2a} \right| + C$$

b)



$$\vec{r} = 2a \sin \alpha \hat{x} + a \cos \alpha \hat{y}$$

$$\vec{F} = -\frac{K}{y} \hat{r}$$

$$\hat{r} = \frac{\vec{r}}{|\vec{r}|}$$

$$\vec{F} = -\frac{K}{a \cos \alpha} \frac{2 \sin \alpha \hat{x} + \cos \alpha \hat{y}}{(4 \sin^2 \alpha + \cos^2 \alpha)^{1/2}}$$

$$= \frac{2a \sin \alpha \hat{x} + a \cos \alpha \hat{y}}{(4a^2 \sin^2 \alpha + a^2 \cos^2 \alpha)^{1/2}}$$

$$\frac{d\vec{r}}{d\alpha} = 2a \cos \alpha \hat{x} - a \sin \alpha \hat{y}$$

$$= \frac{2 \sin \alpha \hat{x} + \cos \alpha \hat{y}}{(4 \sin^2 \alpha + \cos^2 \alpha)^{1/2}}$$

$$W = \int \vec{F} \cdot \left(\frac{d\vec{r}}{d\alpha} \right) d\alpha$$

$$= -\frac{K}{a} \int_0^{\pi/2} \frac{2 \sin \alpha \cdot 2a \cos \alpha - a \sin \alpha \cos \alpha}{\cos \alpha (4 \sin^2 \alpha + \cos^2 \alpha)^{1/2}} d\alpha$$

$$= -\frac{K}{a} \int_0^{\pi/2} \frac{3a \sin \alpha}{(4 \sin^2 \alpha + \cos^2 \alpha)^{1/2}} d\alpha$$

$$= -3K \int_0^{\pi/2} \frac{\sin \alpha d\alpha}{(4 \sin^2 \alpha + \cos^2 \alpha)^{1/2}}$$

$$= -3K \int_0^{\pi/2} \frac{\sin \alpha d\alpha}{(4(1 - \cos^2 \alpha) + \cos^2 \alpha)^{1/2}}$$

$$= -3K \int_0^{\pi/2} \frac{\sin \alpha d\alpha}{(4 - 3 \cos^2 \alpha)^{1/2}}$$

$$= -3K \int_0^{\pi/2} \frac{\sin \alpha d\alpha}{\sqrt{3} \left(\frac{4}{3} - \cos^2 \alpha \right)^{1/2}}$$

$$= -\frac{3K}{\sqrt{3}} \int_0^{\pi/2} \frac{\sin \alpha d\alpha}{\left(\frac{4}{3} - \cos^2 \alpha \right)^{1/2}}$$

$$\frac{4}{3} u^2 = \cos^2 \alpha$$

$$\frac{2}{\sqrt{3}} u = \cos \alpha$$

$$\frac{2}{\sqrt{3}} du = -\sin \alpha d\alpha$$

$$-\frac{2}{\sqrt{3}} du = \sin \alpha d\alpha$$

$$= -\frac{2}{\sqrt{3}} \int \frac{du}{\left(\frac{4}{3} - \frac{4}{3} u^2 \right)^{1/2}}$$

$$= -\frac{2}{\sqrt{3}} \int \frac{du}{\frac{2}{\sqrt{3}} (1 - u^2)^{1/2}}$$

$$= - \int \frac{du}{(1 - u^2)^{1/2}}$$

$$W = \frac{3K}{\sqrt{3}} \sin^{-1}\left(\frac{\sqrt{3}}{2} \cos \alpha\right) \Big|_0^{\pi/2}$$

$$= \frac{3K}{\sqrt{3}} \left(-\sin^{-1}\left(\frac{\sqrt{3}}{2}\right)\right)$$

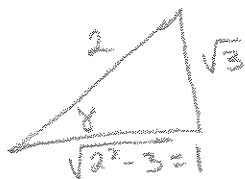
$$= -\frac{3K}{\sqrt{3}} \sin^{-1}\left(\frac{\sqrt{3}}{2}\right)$$

$$= -\frac{3K}{\sqrt{3}} \left(\frac{\pi}{3}\right)$$

$$W = -\frac{\pi K}{\sqrt{3}}$$

$$y = \sin^{-1}\left(\frac{\sqrt{3}}{2}\right)$$

$$\sin y = \frac{\sqrt{3}}{2}$$



$$\cos y = \frac{1}{2}$$

$$y = \frac{\pi}{3}$$

$$-\int \frac{du}{(1-u^2)^{1/2}} = -\int \frac{\cos \beta d\beta}{(1-\sin^2 \beta)^{1/2}}$$

$$u = \sin \beta$$

$$du = \cos \beta d\beta$$

$$= -\int d\beta$$

$$= -\beta + C$$

$$= -\sin^{-1}(u) + C$$

$$= -\sin^{-1}\left(\frac{\sqrt{3}}{2} \cos \alpha\right) + C$$

3-15

$$\vec{A} = A_r \hat{r} + A_\theta \hat{\theta} + A_z \hat{z}$$

$$\frac{d\hat{r}}{d\theta} = \hat{\theta}, \quad \frac{d\hat{\theta}}{d\theta} = -\hat{r}$$

$$\frac{d\vec{A}}{dt} = \frac{dA_r}{dt} \hat{r} + A_r \frac{d\hat{r}}{dt} + \frac{dA_\theta}{dt} \hat{\theta} + A_\theta \frac{d\hat{\theta}}{dt} + \frac{dA_z}{dt} \hat{z} + A_z \frac{d\hat{z}}{dt}$$

$$\frac{d\hat{r}}{dt} = \frac{d\hat{r}}{d\theta} \frac{d\theta}{dt} = \dot{\theta} \hat{\theta}$$

$$\frac{d\hat{\theta}}{dt} = \frac{d\hat{\theta}}{d\theta} \frac{d\theta}{dt} = -\dot{\theta} \hat{r}$$

$$= \frac{dA_r}{dt} \hat{r} + A_r \dot{\theta} \hat{\theta} + \frac{dA_\theta}{dt} \hat{\theta} - A_\theta \dot{\theta} \hat{r} + \frac{dA_z}{dt} \hat{z} + A_z \frac{d\hat{z}}{dt}$$

$$= \left(\frac{dA_r}{dt} - A_\theta \dot{\theta} \right) \hat{r} + \left(A_r \dot{\theta} + \frac{dA_\theta}{dt} \right) \hat{\theta} + \frac{dA_z}{dt} \hat{z} + A_z \frac{d\hat{z}}{dt}$$

$$\frac{d^2\vec{A}}{dt^2} = \left(\frac{dA_r}{dt} - A_\theta \dot{\theta} \right) \frac{d\hat{r}}{dt} + \left(\frac{d^2A_r}{dt^2} - \frac{dA_\theta}{dt} \dot{\theta} - A_\theta \ddot{\theta} \right) \hat{r} + \left(A_r \ddot{\theta} + \frac{dA_\theta}{dt} \dot{\theta} \right) \frac{d\hat{\theta}}{dt} + \left(\frac{dA_z}{dt} \dot{\theta} + A_r \ddot{\theta} + \frac{dA_\theta}{dt} \dot{\theta} \right) \hat{\theta} + \frac{d^2A_z}{dt^2} \hat{z} + \frac{dA_z}{dt} \frac{d\hat{z}}{dt} + \frac{dA_z}{dt} \frac{d\hat{z}}{dt} + A_z \frac{d^2\hat{z}}{dt^2}$$

$$= (\dot{A}_r \dot{\theta} - A_\theta \dot{\theta}^2) \hat{\theta} + (\ddot{A}_r - \dot{A}_\theta \dot{\theta} - A_\theta \ddot{\theta}) \hat{r} - (A_r \ddot{\theta} + \dot{A}_\theta \dot{\theta}) \hat{r} +$$

$$(\dot{A}_r \dot{\theta} + A_r \ddot{\theta} + \dot{A}_\theta \dot{\theta}) \hat{\theta} + \ddot{A}_z \hat{z} + 2\dot{A}_z \frac{d\hat{z}}{dt} + A_z \frac{d^2\hat{z}}{dt^2}$$

$$= (\ddot{A}_r - \dot{A}_\theta \dot{\theta} - A_\theta \ddot{\theta} - A_r \dot{\theta}^2 - \dot{A}_\theta \dot{\theta}) \hat{r} + (\dot{A}_r \dot{\theta} - A_\theta \dot{\theta}^2 + \dot{A}_r \dot{\theta} + A_r \ddot{\theta} + \dot{A}_\theta \dot{\theta}) \hat{\theta} +$$

$$\ddot{A}_z \hat{z} + 2\dot{A}_z \frac{d\hat{z}}{dt} + A_z \frac{d^2\hat{z}}{dt^2}$$

$$\frac{d^2\vec{A}}{dt^2} = (\ddot{A}_r - 2\dot{A}_\theta \dot{\theta} - A_\theta \ddot{\theta} - A_r \dot{\theta}^2) \hat{r} + (\ddot{A}_\theta + 2\dot{A}_r \dot{\theta} + A_r \ddot{\theta} - A_\theta \dot{\theta}^2) \hat{\theta} + \ddot{A}_z \hat{z}$$

$$\left\{ \frac{d\hat{z}}{dt} = \frac{d^2\hat{z}}{dt^2} = 0 \right\}$$

3-17

a) $x = f - h \quad y = 2(fh)^{1/2}$

$$y^2 = 4fh$$

$$h = \frac{y^2}{4f}$$

$$x = f - \frac{y^2}{4f}$$

$$4xf = 4f^2 - y^2$$

$$4f^2 - 4xf = y^2$$

$$f^2 - xf = \frac{y^2}{4}$$

$$f^2 - xf + \frac{x^2}{4} = \frac{y^2 + x^2}{4}$$

$$\left(f - \frac{x}{2}\right)^2 = \frac{y^2 + x^2}{4}$$

$$f - \frac{x}{2} = \pm \frac{(y^2 + x^2)^{1/2}}{2}$$

$$\boxed{f = \frac{x \pm (x^2 + y^2)^{1/2}}{2} \quad h = \frac{-x \pm (x^2 + y^2)^{1/2}}{2}}$$

$$y^2 = 4fh$$

$$f = \frac{y^2}{4h}$$

$$x = \frac{y^2}{4h} - h$$

$$4xh = y^2 - 4h^2$$

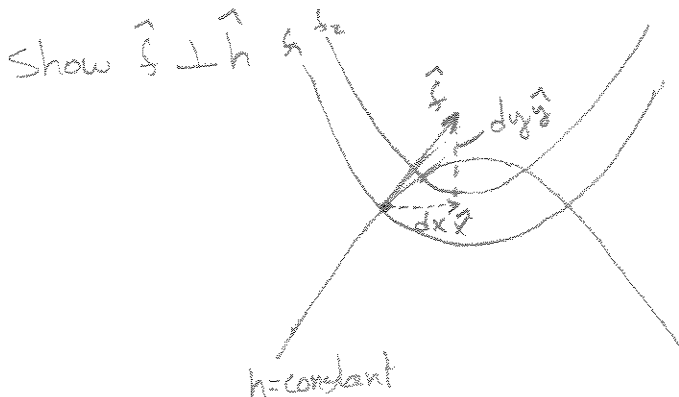
$$4h^2 + 4xh = y^2$$

$$h^2 + xh = \frac{y^2}{4}$$

$$h^2 + xh + \frac{x^2}{4} = \frac{y^2 + x^2}{4}$$

$$\left(h + \frac{x}{2}\right)^2 = \frac{y^2 + x^2}{4}$$

$$h + \frac{x}{2} = \pm \frac{(y^2 + x^2)^{1/2}}{2}$$



$$\hat{f} = \frac{(dx\hat{x} + dy\hat{y})}{((dx)^2 + (dy)^2)^{1/2}}$$

$$\hat{f}) \quad x = f - h, \quad df > 0, \quad dh = 0$$

$$dx = df - dh \quad \& \quad dh = 0, \quad h = \text{constant}$$

$$dx = df$$

$$y = 2(fh)^{1/2}$$

$$dy = (fh)^{-1/2} [f dh + h df]$$

$$dy = \frac{h df}{(fh)^{1/2}}$$

$$\hat{f} = \frac{dx \hat{x} + dy \hat{y}}{\left[(df)^2 + \frac{(h df)^2}{fh} \right]^{1/2}}$$

$$= \frac{df \hat{x} + \frac{h df}{(fh)^{1/2}} \hat{y}}{D_1}$$

$$\hat{f} \cdot \hat{h} = \frac{df}{D_1} \cdot \frac{-dh}{D_2} + \frac{\frac{h df}{(fh)^{1/2}}}{D_1 D_2} \cdot \frac{f dh}{(fh)^{1/2}}$$

$$= \frac{-df dh + \frac{h df \cdot f dh}{fh}}{D_1 D_2}$$

$$= \frac{-df dh + df dh}{D_1 D_2}$$

$$\hat{f} \cdot \hat{h} = 0 \rightarrow \hat{f} \perp \hat{h}$$

$$\hat{h}) \quad x = f - h, \quad dh > 0, \quad df = 0$$

$$dx = df - dh$$

$$dx = -dh$$

$$dy = (fh)^{1/2} [f dh + h df]$$

$$dy = \frac{f dh}{(fh)^{1/2}}$$

$$\hat{h} = \frac{dx \hat{x} + dy \hat{y}}{\left[(dh)^2 + \frac{(f dh)^2}{fh} \right]^{1/2}}$$

$$= \frac{-dh \hat{x} + \frac{f dh}{(fh)^{1/2}} \hat{y}}{D_2}$$

b) Express $\hat{f}$ and $\hat{h}$ in terms of f and h .

$$x = f - h \quad y = 2(fh)^{1/2}$$

The unit tangent vector is

$$\hat{T} = \frac{d\vec{R}}{ds} = \frac{dx}{ds} \hat{x} + \frac{dy}{ds} \hat{y} \quad ds^2 = dx^2 + dy^2$$

$\hat{f} = \hat{T}_f$ when $df > 0$ and $h = \text{constant}$ or $dh = 0$

$$dx = df, \quad dy = \frac{h df}{(fh)^{1/2}}$$

$$ds^2 = df^2 + \frac{h^2 df^2}{fh}$$

$$= df^2 \left(1 + \frac{h}{f}\right)$$

$$ds = df \left(\frac{f+h}{f}\right)^{1/2}$$

$$\hat{f} = \frac{df}{df \left(\frac{f+h}{f}\right)^{1/2}} \hat{x} + \frac{h df}{(fh)^{1/2} df \left(\frac{f+h}{f}\right)^{1/2}} \hat{y}$$

$$\boxed{\hat{f} = \left(\frac{f}{f+h}\right)^{1/2} \hat{x} + \left(\frac{h}{f+h}\right)^{1/2} \hat{y}}$$

$\hat{h} = \hat{T}_h$ when $dh > 0$ and $f = \text{constant}$ or $df = 0$

$$\hat{h} = \frac{-dh}{dh \left(\frac{f+h}{h}\right)^{1/2}} \hat{x} + \frac{f dh}{(fh)^{1/2} dh \left(\frac{f+h}{h}\right)^{1/2}} \hat{y}$$

$$\boxed{\hat{h} = -\left(\frac{h}{f+h}\right)^{1/2} \hat{x} + \left(\frac{f}{f+h}\right)^{1/2} \hat{y}}$$

$$dx = -dh, \quad dy = \frac{f dh}{(fh)^{1/2}}$$

$$ds^2 = dh^2 + \frac{f^2 dh^2}{fh}$$

$$ds^2 = dh^2 \left(\frac{f+h}{h}\right)$$

$$ds = dh \left(\frac{f+h}{h}\right)^{1/2}$$

$$\begin{aligned}
\frac{\partial \hat{f}}{\partial f} &= \frac{1}{2} \left(\frac{f}{f+h} \right)^{-1/2} \left(\frac{f+h-f}{(f+h)^2} \right) \hat{x} + \frac{1}{2} \left(\frac{h}{f+h} \right)^{-1/2} \left(\frac{0-h}{(f+h)^2} \right) \hat{y} \\
&= \frac{1}{2} \left(\frac{f+h}{f} \right)^{1/2} \left(\frac{h}{(f+h)^2} \right) \hat{x} - \frac{1}{2} \left(\frac{f+h}{h} \right)^{1/2} \left(\frac{h}{(f+h)^2} \right) \hat{y} \\
&= -\frac{1}{2} \frac{1}{f+h} \left[\frac{-1}{f^{1/2}} \left(\frac{h}{(f+h)^{1/2}} \right) \hat{x} + \frac{h^{1/2}}{(f+h)^{1/2}} \hat{y} \right] \\
&= -\frac{1}{2} \frac{1}{f+h} \left[\left(\frac{h}{f} \right)^{1/2} \frac{-h^{1/2}}{(f+h)^{1/2}} \hat{x} + \left(\frac{h}{f} \right)^{1/2} \frac{f^{1/2}}{(f+h)^{1/2}} \hat{y} \right] \\
&= -\frac{1}{2} \left(\frac{h}{f} \right)^{1/2} \frac{1}{f+h} \left[-\left(\frac{h}{f+h} \right)^{1/2} \hat{x} + \left(\frac{f}{f+h} \right)^{1/2} \hat{y} \right]
\end{aligned}$$

$$\boxed{\frac{\partial \hat{f}}{\partial f} = -\frac{1}{2} \left(\frac{h}{f} \right)^{1/2} \frac{\hat{h}}{f+h}}$$

$$\begin{aligned}
\frac{\partial \hat{f}}{\partial h} &= \frac{1}{2} \left(\frac{f}{f+h} \right)^{-1/2} \left(\frac{-f}{(f+h)^2} \right) \hat{x} + \frac{1}{2} \left(\frac{h}{f+h} \right)^{-1/2} \left(\frac{f+h-h}{(f+h)^2} \right) \hat{y} \\
&= \frac{1}{2} \left(\frac{f+h}{f} \right)^{1/2} \left(\frac{-f}{(f+h)^2} \right) \hat{x} + \frac{1}{2} \left(\frac{f+h}{h} \right)^{1/2} \left(\frac{f}{(f+h)^2} \right) \hat{y} \\
&= \frac{1}{2} \frac{1}{f+h} \left[\frac{-f^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{1}{h^{1/2}} \frac{f}{(f+h)^{1/2}} \hat{y} \right] \\
&= \frac{1}{2} \frac{1}{f+h} \left[\frac{h^{1/2}}{h^{1/2}} \frac{-f^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{f^{1/2}}{h^{1/2}} \frac{f^{1/2}}{(f+h)^{1/2}} \hat{y} \right] \\
&= \frac{1}{2} \left(\frac{f}{h} \right)^{1/2} \frac{1}{f+h} \left[\frac{-h^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{f^{1/2}}{(f+h)^{1/2}} \hat{y} \right]
\end{aligned}$$

$$\boxed{\frac{\partial \hat{f}}{\partial h} = \frac{1}{2} \left(\frac{f}{h} \right)^{1/2} \frac{\hat{h}}{f+h}}$$

$$\begin{aligned}
\frac{\partial \hat{h}}{\partial f} &= -\frac{1}{2} \left(\frac{h}{f+h} \right)^{-\frac{1}{2}} \left(\frac{-h}{(f+h)^2} \right) \hat{x} + \frac{1}{2} \left(\frac{f}{f+h} \right)^{-\frac{1}{2}} \left(\frac{f+h-f}{(f+h)^2} \right) \hat{y} \\
&= \frac{1}{2} \left(\frac{f+h}{h} \right)^{1/2} \left(\frac{h}{(f+h)^2} \right) \hat{x} + \frac{1}{2} \left(\frac{f+h}{f} \right)^{1/2} \left(\frac{h}{(f+h)^2} \right) \hat{y} \\
&= \frac{1}{2} \frac{1}{f+h} \left[\frac{h^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{h^{1/2}}{f^{1/2} (f+h)^{1/2}} \hat{y} \right] \\
&= \frac{1}{2} \frac{1}{f+h} \left[\frac{f^{1/2}}{f^{1/2}} \frac{h^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{h^{1/2}}{f^{1/2}} \frac{h^{1/2}}{(f+h)^{1/2}} \hat{y} \right] \\
&= \frac{1}{2} \left(\frac{h}{f} \right)^{1/2} \frac{1}{f+h} \left[\frac{f^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{h^{1/2}}{(f+h)^{1/2}} \hat{y} \right]
\end{aligned}$$

$$\boxed{\frac{\partial \hat{h}}{\partial f} = \frac{1}{2} \left(\frac{h}{f} \right)^{1/2} \frac{\hat{f}}{f+h}}$$

$$\begin{aligned}
\frac{\partial \hat{h}}{\partial h} &= -\frac{1}{2} \left(\frac{h}{f+h} \right)^{-\frac{1}{2}} \left(\frac{f+h-h}{(f+h)^2} \right) \hat{x} + \frac{1}{2} \left(\frac{f}{f+h} \right)^{-\frac{1}{2}} \left(\frac{-f}{(f+h)^2} \right) \hat{y} \\
&= -\frac{1}{2} \left(\frac{f+h}{h} \right)^{1/2} \left(\frac{f}{(f+h)^2} \right) \hat{x} - \frac{1}{2} \left(\frac{f+h}{f} \right)^{1/2} \left(\frac{f}{(f+h)^2} \right) \hat{y} \\
&= -\frac{1}{2} \frac{1}{f+h} \left[\frac{f^{1/2}}{h^{1/2} (f+h)^{1/2}} \hat{x} + \frac{f^{1/2}}{(f+h)^{1/2}} \hat{y} \right] \\
&= -\frac{1}{2} \frac{1}{f+h} \left[\frac{f^{1/2}}{h^{1/2}} \frac{f^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{f^{1/2}}{h^{1/2}} \frac{h^{1/2}}{(f+h)^{1/2}} \hat{y} \right]
\end{aligned}$$

$$\boxed{\frac{\partial \hat{h}}{\partial h} = -\frac{1}{2} \left(\frac{f}{h} \right)^{1/2} \frac{\hat{f}}{f+h}}$$

$$\vec{r} = x \hat{x} + y \hat{y}$$

$$\vec{r} = (f-h) \hat{x} + 2(sh)^{1/2} \hat{y}$$

$$= (f-h) \left[\frac{f^{1/2} \hat{x} - h^{1/2} \hat{h}}{(f+h)^{1/2}} \right] + 2(sh)^{1/2} \left[\frac{h^{1/2} \hat{x} + f^{1/2} \hat{h}}{(f+h)^{1/2}} \right]$$

$$= \frac{(f-h)f^{1/2} + 2(sh)^{1/2}h^{1/2}}{(f+h)^{1/2}} \hat{x} + \frac{-(f-h)h^{1/2} + 2(sh)^{1/2}f^{1/2}}{(f+h)^{1/2}} \hat{h}$$

$$= \frac{(f-h)f^{1/2} + 2f^{1/2}h}{(f+h)^{1/2}} \hat{x} + \frac{-(f-h)h^{1/2} + 2h^{1/2}f}{(f+h)^{1/2}} \hat{h}$$

$$= \frac{f^{1/2}(f-h+2h)}{(f+h)^{1/2}} \hat{x} + \frac{h^{1/2}(h-f+2f)}{(f+h)^{1/2}} \hat{h}$$

$$\boxed{\vec{r} = f^{1/2}(f+h)^{1/2} \hat{x} + h^{1/2}(f+h)^{1/2} \hat{h}}$$

$$x = f-h \quad y = 2(sh)^{1/2}$$

$$\hat{s} = \left(\frac{f}{f+h} \right)^{1/2} \hat{x} + \left(\frac{h}{f+h} \right)^{1/2} \hat{y}$$

$$\hat{h} = -\left(\frac{h}{f+h} \right)^{1/2} \hat{x} + \left(\frac{f}{f+h} \right)^{1/2} \hat{y}$$

$$(f+h)^{1/2} \hat{s} = f^{1/2} \hat{x} + h^{1/2} \hat{y}$$

$$(f+h)^{1/2} \hat{h} = -h^{1/2} \hat{x} + f^{1/2} \hat{y}$$

$$h^{1/2}(f+h)^{1/2} \hat{s} = h^{1/2}f^{1/2} \hat{x} + h \hat{y}$$

$$f^{1/2}(f+h)^{1/2} \hat{h} = -h^{1/2}f^{1/2} \hat{x} + f \hat{y}$$

$$(f+h)^{1/2}(h^{1/2}\hat{s} + f^{1/2}\hat{h}) = (f+h) \hat{y}$$

$$\boxed{\hat{y} = \frac{h^{1/2}\hat{s} + f^{1/2}\hat{h}}{(f+h)^{1/2}}}$$

$$f^{1/2}(f+h)^{1/2} \hat{s} = f \hat{x} + f^{1/2}h^{1/2} \hat{y}$$

$$-h^{1/2}(f+h)^{1/2} \hat{h} = h \hat{x} - f^{1/2}h^{1/2} \hat{y}$$

$$(f+h)^{1/2}(f^{1/2}\hat{s} - h^{1/2}\hat{h}) = (f+h) \hat{x}$$

$$\boxed{\hat{x} = \frac{f^{1/2}\hat{s} - h^{1/2}\hat{h}}{(f+h)^{1/2}}}$$

$$\vec{v} = \frac{d\vec{r}}{dt} = \frac{d}{dt}(x\hat{x} + y\hat{y})$$

$$= \frac{dx}{dt} \hat{x} + x \frac{d\hat{x}}{dt} + \frac{dy}{dt} \hat{y} + y \frac{d\hat{y}}{dt}$$

$$\frac{d\hat{x}}{dt} = \frac{d\hat{y}}{dt} = 0$$

$$= \left(\frac{dx}{dt} - \frac{dh}{dt} \right) \hat{x} + (fh)^{1/2} \left(\frac{d\hat{s}}{dt} + \frac{d\hat{h}}{dt} \right) \hat{y}$$

$$= (\dot{f} - \dot{h}) \hat{x} + (fh)^{1/2} (\dot{f}\hat{s} + \dot{h}\hat{h}) \hat{y}$$

$$= (\dot{s} - \dot{h}) \frac{s^{1/2} \hat{f} - h^{1/2} \hat{h}}{(s+h)^{1/2}} + (sh)^{-1/2} (s\dot{h} + h\dot{s}) \frac{h^{1/2} \hat{f} + s^{1/2} \hat{h}}{(s+h)^{1/2}}$$

$$= \left[\frac{(\dot{s} - \dot{h}) s^{1/2} + (sh)^{-1/2} (s\dot{h} + h\dot{s}) h^{1/2}}{(s+h)^{1/2}} \right] \hat{f} + \left[\frac{(\dot{h} - \dot{s}) h^{1/2} + (sh)^{-1/2} (s\dot{h} + h\dot{s}) s^{1/2}}{(s+h)^{1/2}} \right] \hat{h}$$

$$= \frac{1}{(s+h)^{1/2}} \left(\left[(\dot{s} - \dot{h}) s^{1/2} + \frac{(s\dot{h} + h\dot{s})}{s^{1/2}} \right] \hat{f} + \left[(\dot{h} - \dot{s}) h^{1/2} + \frac{(s\dot{h} + h\dot{s})}{h^{1/2}} \right] \hat{h} \right)$$

$$= \frac{1}{(s+h)^{1/2}} \left(\left[s^{1/2} \dot{s} - s^{1/2} \dot{h} + s^{1/2} \dot{h} + \frac{h}{s^{1/2}} \dot{s} \right] \hat{f} + \left[h^{1/2} \dot{h} - h^{1/2} \dot{s} + \frac{s}{h^{1/2}} \dot{h} + h^{1/2} \dot{s} \right] \hat{h} \right)$$

$$= \frac{1}{(s+h)^{1/2}} \left(\left[s^{1/2} (\dot{s} - \dot{h} + \dot{h}) + \frac{h}{s^{1/2}} \dot{s} \right] \hat{f} + \left[h^{1/2} (\dot{h} - \dot{s} + \dot{s}) + \frac{s}{h^{1/2}} \dot{h} \right] \hat{h} \right)$$

$$= \frac{1}{(s+h)^{1/2}} \left(\left[s^{1/2} \dot{s} + \frac{h}{s^{1/2}} \dot{s} \right] \hat{f} + \left[h^{1/2} \dot{h} + \frac{s}{h^{1/2}} \dot{h} \right] \hat{h} \right)$$

$$= \frac{1}{(s+h)^{1/2}} \left(\dot{s} \left(s^{1/2} + \frac{h}{s^{1/2}} \right) \hat{f} + \dot{h} \left(h^{1/2} + \frac{s}{h^{1/2}} \right) \hat{h} \right)$$

$$= \frac{1}{(s+h)^{1/2}} \left(\dot{s} \left(\frac{s+h}{s^{1/2}} \right) \hat{f} + \dot{h} \left(\frac{h+s}{h^{1/2}} \right) \hat{h} \right)$$

$$= \frac{s+h}{(s+h)^{1/2}} \left(\frac{\dot{s}}{s^{1/2}} \hat{f} + \frac{\dot{h}}{h^{1/2}} \hat{h} \right)$$

$$\boxed{\dot{\vec{r}} = (s+h)^{1/2} \left(\frac{\dot{s}}{s^{1/2}} \hat{f} + \frac{\dot{h}}{h^{1/2}} \hat{h} \right)}$$

$$\ddot{\vec{r}} = \vec{a} = \frac{d\vec{v}}{dt} = \frac{d}{dt} \left(\frac{dx}{dt} \hat{x} + x \frac{d\hat{x}}{dt} + \frac{dy}{dt} \hat{y} + y \frac{d\hat{y}}{dt} \right)$$

$$= \frac{d}{dt} \left(\frac{dx}{dt} \hat{x} + \frac{dy}{dt} \hat{y} \right) \quad \left\{ \frac{d\hat{x}}{dt} = \frac{d\hat{y}}{dt} = 0 \right\}$$

$$= \frac{d^2x}{dt^2} \hat{x} + \frac{dx}{dt} \frac{d\hat{x}}{dt} + \frac{d^2y}{dt^2} \hat{y} + \frac{dy}{dt} \frac{d\hat{y}}{dt}$$

$$= \frac{d^2x}{dt^2} \hat{x} + \frac{d^2y}{dt^2} \hat{y}$$

$$x = s - h$$

$$\frac{dx}{dt} = \dot{s} - \dot{h}$$

$$\frac{d^2x}{dt^2} = \ddot{s} - \ddot{h}$$

$$y = 2(sh)^{1/2}$$

$$\frac{dy}{dt} = (sh)^{-1/2} (\dot{s}h + h\dot{s})$$

$$\frac{d^2y}{dt^2} = (sh)^{-1/2} [\ddot{s}h + \dot{s}\dot{h} + h\ddot{s} + \dot{h}\dot{s}] + (sh + h\dot{s})(-\frac{1}{2})(sh)^{-3/2}(\dot{s}h + h\dot{s})$$

$$= (sh)^{-1/2} [\ddot{s}h + \dot{s}\dot{h} + h\ddot{s} + \dot{h}\dot{s}] - \frac{1}{2}(\dot{s}h + h\dot{s})^2 (sh)^{-3/2}$$

$$= (sh)^{-1/2} [\ddot{s}h + 2\dot{s}\dot{h} + h\ddot{s}] - \frac{1}{2}(\dot{s}h + h\dot{s})^2 (sh)^{-3/2}$$

$$(\ddot{s} - \ddot{h}) \hat{x} = (\ddot{s} - \ddot{h}) \frac{s^{1/2} \hat{s} - h^{1/2} \hat{h}}{(s+h)^{1/2}}$$

$$= \frac{(\ddot{s} - \ddot{h}) s^{1/2}}{(s+h)^{1/2}} \hat{s} - \frac{(\ddot{s} - \ddot{h}) h^{1/2}}{(s+h)^{1/2}} \hat{h}$$

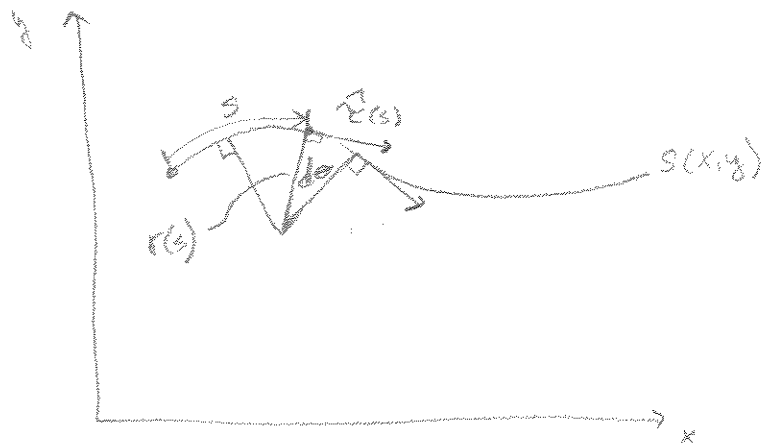
$$\hat{y} \text{ term: } \left[(sh)^{-1/2} (\ddot{s}h + 2\dot{s}\dot{h} + h\ddot{s}) - \frac{1}{2}(\dot{s}h + h\dot{s})^2 (sh)^{-3/2} \right] \frac{h^{1/2} \hat{s} + s^{1/2} \hat{h}}{(s+h)^{1/2}} = \frac{1}{2}(\dot{s}h + h\dot{s})^2 (sh)^{-3/2}$$

$$\left[\frac{s^{-1/2} (\ddot{s}h + 2\dot{s}\dot{h} + h\ddot{s}) - \frac{h^{1/2} (\dot{s}h + h\dot{s})^2}{2s^{3/2} h^{1/2}}}{(s+h)^{1/2}} \right] \hat{s} +$$

$$\left[\frac{h^{-1/2} (\ddot{s}h + 2\dot{s}\dot{h} + h\ddot{s}) - \frac{s^{1/2} (\dot{s}h + h\dot{s})^2}{2s^{3/2} h^{1/2}}}{(s+h)^{1/2}} \right] \hat{h}$$

$$\ddot{\vec{r}} = \frac{1}{(s+h)^{1/2}} \left[\left[(\ddot{s} - \ddot{h}) s^{1/2} + \frac{s^{-1/2} (\ddot{s}h + 2\dot{s}\dot{h} + h\ddot{s}) - (\dot{s}h + h\dot{s})^2}{2s^{3/2} h} \right] \hat{s} - \left[(\ddot{s} - \ddot{h}) h^{1/2} - \frac{h^{1/2} (\ddot{s}h + 2\dot{s}\dot{h} + h\ddot{s}) + (\dot{s}h + h\dot{s})^2}{2h^{3/2} s} \right] \hat{h} \right]$$

3-19



$$r d\theta = ds$$

$$r \frac{d\theta}{dt} = \frac{ds}{dt} = V(s)$$

$$r\omega = V(s)$$

$$V(s) \hat{t}(s) = \vec{V}(s)$$

$$r\omega \hat{t}(s) = \vec{V}(s)$$

$$\hat{t}(s) = \frac{\vec{V}(s)}{r\omega}$$

$$\frac{d\hat{t}}{ds} = \frac{\vec{V}}{r\omega} \frac{1}{ds}$$

$$= \frac{1}{r} \frac{\vec{V}}{\omega ds} \quad \omega ds = |\vec{V}|$$

$$= \frac{1}{r} \frac{\vec{V}}{|\vec{V}|}$$

$$\boxed{\frac{d\hat{t}}{ds} = \frac{\hat{V}}{r}}$$

$$V(s) \hat{t} = \vec{V}$$

$$\boxed{\dot{s} \hat{t} = \vec{V}}$$

$$r d\theta = ds$$

$$r\omega = \frac{ds}{dt} = \dot{s} = V(s)$$

$$\vec{a} = \frac{d\vec{V}}{dt}$$

$$= \frac{d}{dt}(\dot{s} \hat{t})$$

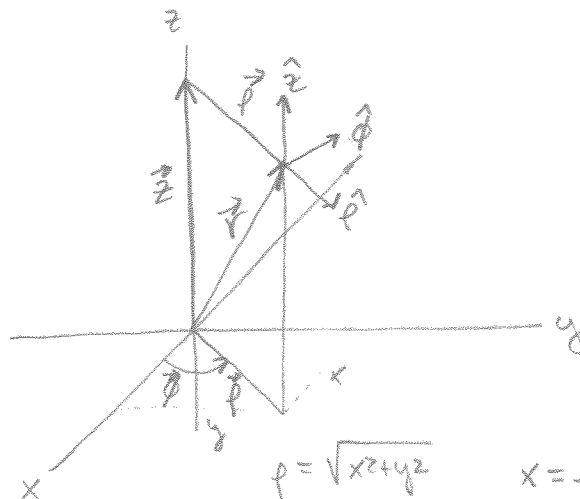
$$= \ddot{s} \hat{t} + \dot{s} \frac{d\hat{t}}{dt}$$

$$\vec{a} = \ddot{s} \hat{e} + \dot{s} \frac{d\hat{e}}{ds} \cdot \frac{ds}{dt}$$

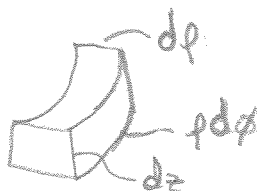
$$= \ddot{s} \hat{e} + \dot{s}^2 \frac{d\hat{e}}{ds} \quad \left\{ \frac{d\hat{e}}{ds} = \frac{\hat{v}}{r} \right\}$$

$$\boxed{\vec{a} = \ddot{s} \hat{e} + \frac{\dot{s}^2}{r} \hat{v}}$$

3-21

curl $\vec{A}$ in cylindrical coordinates

Del operator



$$\vec{\nabla} = \frac{\partial}{\partial s_1} \hat{e}_1 + \frac{\partial}{\partial s_2} \hat{e}_2 + \frac{\partial}{\partial s_3} \hat{e}_3$$

$$ds_1 = d\rho, ds_2 = \rho d\phi, ds_3 = dz, \hat{e}_1 = \hat{\rho}, \hat{e}_2 = \hat{\phi}, \hat{e}_3 = \hat{z}$$

$$\vec{\nabla} = \frac{\partial}{\partial \rho} \hat{\rho} + \frac{1}{\rho} \frac{\partial}{\partial \phi} \hat{\phi} + \frac{\partial}{\partial z} \hat{z}$$

$$\vec{A} = A_\rho \hat{\rho} + A_\phi \hat{\phi} + A_z \hat{z}$$

$$\vec{\nabla} \times \vec{A} = \hat{\rho} \times \frac{\partial \vec{A}}{\partial \rho} + \frac{\hat{\phi}}{\rho} \times \frac{\partial \vec{A}}{\partial \phi} + \hat{z} \times \frac{\partial \vec{A}}{\partial z}$$

$$= \hat{\rho} \times \left[\frac{\partial A_\rho}{\partial \rho} \hat{\rho} + \frac{\partial A_\phi}{\partial \rho} \hat{\phi} + \frac{\partial A_z}{\partial \rho} \hat{z} + A_\rho \frac{\partial \hat{\rho}}{\partial \rho} + A_\phi \frac{\partial \hat{\phi}}{\partial \rho} + A_z \frac{\partial \hat{z}}{\partial \rho} \right] +$$

$$\frac{\hat{\phi}}{\rho} \times \left[\frac{\partial A_\rho}{\partial \phi} \hat{\rho} + \frac{\partial A_\phi}{\partial \phi} \hat{\phi} + \frac{\partial A_z}{\partial \phi} \hat{z} + A_\rho \frac{\partial \hat{\rho}}{\partial \phi} + A_\phi \frac{\partial \hat{\phi}}{\partial \phi} + A_z \frac{\partial \hat{z}}{\partial \phi} \right] +$$

$$\hat{z} \times \left[\frac{\partial A_\rho}{\partial z} \hat{\rho} + \frac{\partial A_\phi}{\partial z} \hat{\phi} + \frac{\partial A_z}{\partial z} \hat{z} + A_\rho \frac{\partial \hat{\rho}}{\partial z} + A_\phi \frac{\partial \hat{\phi}}{\partial z} + A_z \frac{\partial \hat{z}}{\partial z} \right]$$

$$z = z$$

$$\hat{\rho} = \frac{\vec{r}}{\rho} = \frac{x\hat{x} + y\hat{y}}{\rho} = \frac{\rho \cos \phi \hat{x} + \rho \sin \phi \hat{y}}{\rho}$$

$$\hat{\rho} = \cos \phi \hat{x} + \sin \phi \hat{y}$$

$$\begin{aligned} \hat{\phi} &= \hat{z} \times \hat{\rho} = \hat{z} \times (\cos \phi \hat{x} + \sin \phi \hat{y}) \\ &= \cos \phi \hat{y} - \sin \phi \hat{x} \\ &= -\sin \phi \hat{x} + \cos \phi \hat{y} \end{aligned}$$

$$\hat{z} = \hat{z}$$

The rectangular unit vectors, $\hat{x}$, $\hat{y}$, and $\hat{z}$, are not functions of position. So,

$$\frac{\partial \hat{\rho}}{\partial \rho} = 0, \frac{\partial \hat{\phi}}{\partial \rho} = 0, \frac{\partial \hat{z}}{\partial \rho} = 0$$

$$\frac{\partial \hat{\rho}}{\partial \phi} = -\sin \phi \hat{x} + \cos \phi \hat{y} = \hat{\phi}$$

$$\frac{\partial \hat{\phi}}{\partial \phi} = -\cos \phi \hat{x} - \sin \phi \hat{y} = -\hat{\rho}$$

$$\frac{\partial \hat{z}}{\partial \phi} = 0$$

$$\frac{\partial \hat{\rho}}{\partial z} = 0, \frac{\partial \hat{\phi}}{\partial z} = 0, \frac{\partial \hat{z}}{\partial z} = 0$$

$$\vec{\nabla} \times \vec{A} = \hat{r} \times \left[\frac{\partial A_\phi}{\partial r} \hat{r} + \frac{\partial A_\phi}{\partial \phi} \hat{\phi} + \frac{\partial A_z}{\partial z} \hat{z} + 0 + 0 + 0 \right] +$$

$$\frac{\hat{\phi}}{r} \times \left[\frac{\partial A_\phi}{\partial \phi} \hat{r} + \frac{\partial A_\phi}{\partial \phi} \hat{\phi} + \frac{\partial A_z}{\partial \phi} \hat{z} + A_\phi \hat{\phi} - A_\phi \hat{r} + 0 \right] +$$

$$\hat{z} \times \left[\frac{\partial A_\phi}{\partial z} \hat{r} + \frac{\partial A_\phi}{\partial z} \hat{\phi} + \frac{\partial A_z}{\partial z} \hat{z} + 0 + 0 + 0 \right]$$

$$= \frac{\partial A_\phi}{\partial z} \hat{z} - \frac{\partial A_z}{\partial r} \hat{\phi} - \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} \hat{z} + \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} A_\phi \hat{z} +$$

$$\frac{\partial A_\phi}{\partial z} \hat{\phi} - \frac{\partial A_\phi}{\partial z} \hat{r}$$

$$\begin{aligned} \hat{r} \times \hat{\phi} &= \hat{z} & \hat{\phi} \times \hat{r} &= -\hat{z} & \hat{z} \times \hat{r} &= \hat{\phi} \\ \hat{r} \times \hat{z} &= -\hat{\phi} & \hat{\phi} \times \hat{z} &= \hat{r} & \hat{z} \times \hat{\phi} &= -\hat{r} \end{aligned}$$

$$\boxed{\vec{\nabla} \times \vec{A} = \left(\frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) \hat{r} + \left(\frac{\partial A_\phi}{\partial z} - \frac{\partial A_z}{\partial r} \right) \hat{\phi} + \left(\frac{\partial A_\phi}{\partial r} + \frac{A_\phi}{r} - \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} \right) \hat{z}}$$

Alternate Method:

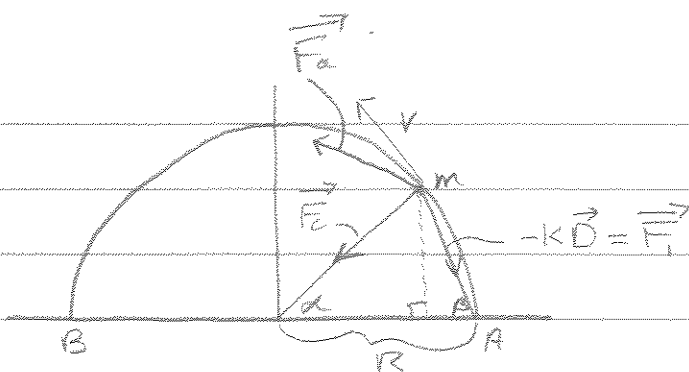
$$\vec{\nabla} \times \vec{A} = \begin{vmatrix} \hat{r} & \hat{\phi} & \hat{z} \\ \frac{\partial}{\partial r} & \frac{1}{r} \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_r & A_\phi & A_z \end{vmatrix}$$

$$= \hat{r} \left(\frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial A_\phi}{\partial z} - \frac{\partial A_z}{\partial r} \right) + \hat{z} \left(\frac{\partial A_\phi}{\partial r} - \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} \right)$$

$$= \hat{r} \left(\frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial A_\phi}{\partial z} - \frac{\partial A_z}{\partial r} \right) + \hat{z} \frac{1}{r} \left(\frac{\partial r A_\phi}{\partial r} - \frac{\partial A_\phi}{\partial \phi} \right)$$

$$\boxed{\vec{\nabla} \times \vec{A} = \hat{r} \left(\frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \hat{\phi} \left(\frac{\partial A_\phi}{\partial z} - \frac{\partial A_z}{\partial r} \right) + \hat{z} \left(\frac{\partial A_\phi}{\partial r} + \frac{A_\phi}{r} - \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} \right)}$$

3-23



$$\vec{F}_c = \vec{F}_l + \vec{F}_a$$

$$\vec{F}_a = \vec{F}_c - \vec{F}_l$$

$$\vec{F}_c = -\frac{mv^2}{R} \cos \alpha \hat{x} - \frac{mv^2}{R} \sin \alpha \hat{y}$$

$$F_{ax} = -\frac{mv^2}{R} \cos \alpha - \left(\frac{F_0}{2} - \frac{F_0}{2} \cos \alpha \right)$$

$$= -\frac{F_0}{2} + \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \cos \alpha$$

$$F_{ay} = -\frac{mv^2}{R} \sin \alpha - \left(-\frac{F_0}{2} \sin \alpha \right)$$

$$= \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \sin \alpha$$

$$\vec{F}_a = -\frac{F_0}{2} + \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \cos \alpha \hat{x} + \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \sin \alpha \hat{y}$$

$$F_l = -kD$$

$$F_0 = -k(2R)$$

$$\frac{F_0}{2R} = -k$$

$$F_l = \frac{F_0}{2R} D$$

$$\vec{F}_l = -\frac{F_0}{2R} \vec{D}$$

$$D^2 = R^2 + R^2 - 2R^2 \cos \alpha$$

$$= 2R^2 - 2R^2 \cos \alpha$$

$$= 2R^2(1 - \cos \alpha)$$

$$D_y = R \sin \alpha$$

$$\vec{D}_y = R \sin \alpha \hat{y}$$

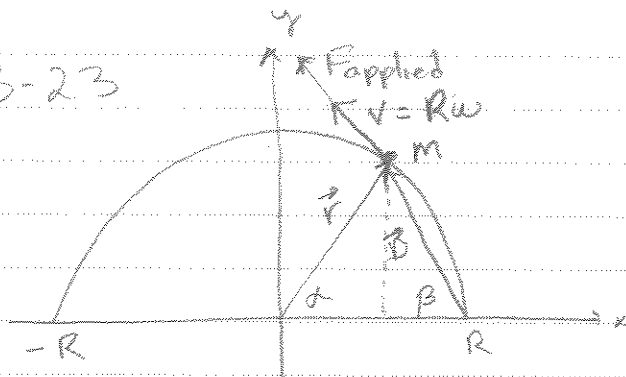
$$D_x = R - R \cos \alpha$$

$$\vec{D}_x = R(1 - \cos \alpha) \hat{x}$$

$$\vec{F}_l = -\frac{F_0}{2R} (-R(1 - \cos \alpha) \hat{x} + R \sin \alpha \hat{y})$$

$$\vec{F}_l = \left(\frac{F_0}{2} - \frac{F_0}{2} \cos \alpha \right) \hat{x} - \frac{F_0}{2} \sin \alpha \hat{y}$$

3-23



a) $\vec{F}_c = -\frac{mv^2}{R} \hat{r}$

$\vec{F}_1 = -kD$

$F_1 = -kD$

$F_0 = -k2R$

$\frac{F_0}{2R} = -k$

$-\hat{r} = -\cos\alpha \hat{x} - \sin\alpha \hat{y}$

$D_x = R - R\cos\alpha$

$= R(1 - \cos\alpha)$

$D_y = R\sin\alpha$

$F_{1x} = kD_x$

$= kR(1 - \cos\alpha) = \frac{F_0}{2}(1 - \cos\alpha)$

$F_{1y} = -kR\sin\alpha = -\frac{F_0}{2}\sin\alpha$

$F_{cx} = -\frac{mv^2}{R} \cos\alpha$

$F_{cy} = -\frac{mv^2}{R} \sin\alpha$

$F_{ay} = F_{cy} - F_{1y}$

$= -\frac{mv^2}{R} \sin\alpha + \frac{F_0}{2} \sin\alpha$

$F_y = \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \sin\left(\frac{vR}{R}\right)$

$\vec{F}_c = \vec{F}_1 + \vec{F}_{\text{applied}}$

$= \vec{F}_1 + \vec{F}_{\text{a}}$

$\vec{F}_a = \vec{F}_c - \vec{F}_1$

$F_a = -F_{ax} = -F_{cx} + F_{1x}$

$= \frac{mv^2}{R} \cos\alpha + \frac{F_0}{2}(1 - \cos\alpha)$

$= -\frac{F_0}{2} \cos\alpha + \frac{F_0}{2} + \frac{mv^2}{R} \cos\alpha$

$v = R\omega = R \frac{d\alpha}{dt}$

$\frac{vR}{R} = \alpha$

$F_x = \frac{F_0}{2} + \left(\frac{mv^2}{R} - \frac{F_0}{2} \right) \cos\left(\frac{vR}{R}\right)$

$$b) \vec{I} = \int_{t_1}^{t_2} \vec{F} dt$$

$$\vec{F} = F_x \hat{x} + F_y \hat{y}$$

$$= \left(\frac{F_0}{2} + \left(\frac{mv^2}{R} - \frac{F_0}{2} \right) \cos\left(\frac{Vt}{R}\right) \right) \hat{x} + \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \sin\left(\frac{Vt}{R}\right) \hat{y}$$

$$\vec{I} = \int_{t_1}^{t_2} \left[\frac{F_0}{2} + \left(\frac{mv^2}{R} - \frac{F_0}{2} \right) \cos\left(\frac{Vt}{R}\right) \right] \hat{x} dt + \int_{t_1}^{t_2} \left[\left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \sin\left(\frac{Vt}{R}\right) \right] \hat{y} dt$$

$$t_1 = 0 \quad t_2 = \frac{\pi R}{V}$$

$$I_x = \frac{F_0}{2} \Big|_0^{\frac{\pi R}{V}} + \frac{R}{V} \left(\frac{mv^2}{R} - \frac{F_0}{2} \right) \sin\left(\frac{Vt}{R}\right) \Big|_0^{\frac{\pi R}{V}}$$

$$= \frac{\pi F_0 R}{2V} + \frac{R}{V} \left(\frac{mv^2}{R} - \frac{F_0}{2} \right) (0 - 0)$$

$$I_x = \frac{\pi F_0 R}{2V}$$

$$I_y = -\frac{R}{V} \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) \cos\left(\frac{Vt}{R}\right) \Big|_0^{\frac{\pi R}{V}}$$

$$= -\frac{R}{V} \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) (-1 - 1)$$

$$= -\frac{R}{V} \left(\frac{F_0}{2} - \frac{mv^2}{R} \right) (-2)$$

$$I_y = \frac{F_0 R}{V} - 2mv$$

$$\boxed{\vec{I} = \frac{\pi F_0 R}{2V} \hat{x} + \left(\frac{F_0 R}{V} - 2mv \right) \hat{y}}$$

3-25

$$x = x_0 + at^2$$

$$y = bt^3$$

$$z = ct$$

$$\vec{L} = \vec{r} \times \vec{p}$$

$$= m(\vec{r} \times \vec{v})$$

$$\vec{r} = (x_0 + at^2)\hat{x} + bt^3\hat{y} + ct\hat{z}$$

$$\vec{v} = \frac{d\vec{r}}{dt} = 2at\hat{x} + 3bt^2\hat{y} + c\hat{z}$$

$$= m \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ x_0 + at^2 & bt^3 & ct \\ 2at & 3bt^2 & c \end{vmatrix}$$

$$= m[(bct^3 - 3bct^3)\hat{x} + (2act^2 - x_0c - act^2)\hat{y} + (3x_0bt^2 + 3abt^4 - 2abt^4)\hat{z}]$$

$$\vec{L} = m[-2bct^3\hat{x} + (act^2 - x_0c)\hat{y} + (3x_0bt^2 + abt^4)\hat{z}]$$

$$\vec{F} = m\vec{a} \quad \vec{a} = \frac{d\vec{v}}{dt} = 2a\hat{x} + 6bt\hat{y}$$

$$\vec{F} = 2ma\hat{x} + 6mbt\hat{y}$$

$$\vec{N} = \frac{d\vec{L}}{dt} = \vec{r} \times \vec{F}$$

$$= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ x_0 + at^2 & bt^3 & ct \\ 2ma & 6mbt & 0 \end{vmatrix}$$

$$= (0 - 6mbct^3)\hat{x} + (2mact - 0)\hat{y} + (6x_0mbt + 6mbt^3 - 2mabt^3)\hat{z}$$

$$\vec{N} = -6mbct^3\hat{x} + 2mact\hat{y} + (6x_0mbt + 4abt^3)\hat{z}$$

$$\frac{d\vec{L}}{dt} = m[-6bct^2 \hat{x} + 2act \hat{y} + (6x_0bt + 4abt^3) \hat{z}]$$

$$\vec{N} = \frac{d\vec{L}}{dt}$$

3-27

$$\vec{r} = r \hat{r}(\theta, \phi)$$

$$\vec{v} = \frac{d\vec{r}}{dt} = \dot{r} \hat{r} + r \dot{\theta} \hat{\theta} + r \dot{\phi} \sin \theta \hat{\phi} \quad \left\{ \text{see } \frac{d\hat{r}}{dt} \text{ below} \right\}$$

$$\begin{aligned} \vec{a} = \frac{d\vec{v}}{dt} &= \ddot{r} \hat{r} + \dot{r} \frac{d\hat{r}}{dt} + \\ &\quad \dot{r} \dot{\theta} \hat{\theta} + r \ddot{\theta} \hat{\theta} + r \dot{\theta} \frac{d\hat{\theta}}{dt} + \\ &\quad \dot{r} \dot{\phi} \sin \theta \hat{\phi} + r \ddot{\phi} \sin \theta \hat{\phi} + \\ &\quad r \dot{\phi} \dot{\theta} \cos \theta \hat{\phi} + r \dot{\phi} \sin \theta \frac{d\hat{\phi}}{dt} \end{aligned}$$

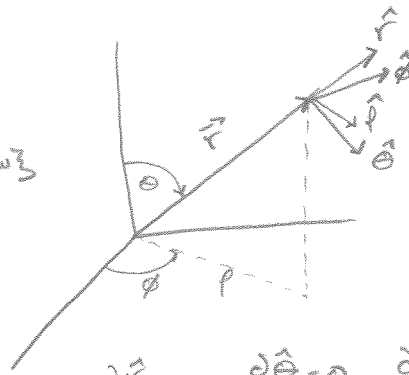
$$\begin{aligned} \frac{d\hat{r}}{dt} &= \frac{\partial \hat{r}}{\partial r} \frac{dr}{dt} + \frac{\partial \hat{r}}{\partial \theta} \frac{d\theta}{dt} + \frac{\partial \hat{r}}{\partial \phi} \frac{d\phi}{dt} \\ &= 0 + \dot{\theta} \hat{\theta} + \dot{\phi} \sin \theta \hat{\phi} \end{aligned}$$

$$\begin{aligned} \frac{d\hat{\theta}}{dt} &= \frac{\partial \hat{\theta}}{\partial r} \frac{dr}{dt} + \frac{\partial \hat{\theta}}{\partial \theta} \frac{d\theta}{dt} + \frac{\partial \hat{\theta}}{\partial \phi} \frac{d\phi}{dt} \\ &= 0 - \dot{\theta} \hat{r} + \dot{\phi} \cos \theta \hat{\phi} \end{aligned}$$

$$\begin{aligned} \frac{d\hat{\phi}}{dt} &= \frac{\partial \hat{\phi}}{\partial r} \frac{dr}{dt} + \frac{\partial \hat{\phi}}{\partial \theta} \frac{d\theta}{dt} + \frac{\partial \hat{\phi}}{\partial \phi} \frac{d\phi}{dt} \\ &= 0 + 0 - \dot{\phi} \sin \theta \hat{r} - \dot{\phi} \cos \theta \hat{\theta} \end{aligned}$$

$$\begin{aligned} \vec{a} &= \ddot{r} \hat{r} + \dot{r} [\dot{\theta} \hat{\theta} + \dot{\phi} \sin \theta \hat{\phi}] + \dot{r} \dot{\theta} \hat{\theta} + r \ddot{\theta} \hat{\theta} + r \dot{\theta} [-\dot{\theta} \hat{r} + \dot{\phi} \cos \theta \hat{\phi}] + \\ &\quad r \dot{\phi} \sin \theta \hat{\phi} + r \ddot{\phi} \sin \theta \hat{\phi} + r \dot{\phi} \dot{\theta} \cos \theta \hat{\phi} + r \dot{\phi} \sin \theta [-\dot{\phi} \sin \theta \hat{r} - \dot{\phi} \cos \theta \hat{\theta}] \\ &= \ddot{r} \hat{r} - r \dot{\theta}^2 \hat{r} - r \dot{\phi}^2 \sin^2 \theta \hat{r} + \\ &\quad r \ddot{\theta} \hat{\theta} + \dot{r} \dot{\theta} \hat{\theta} + r \ddot{\theta} \hat{\theta} - r \dot{\phi}^2 \sin \theta \cos \theta \hat{\theta} + \\ &\quad r \dot{\phi} \sin \theta \hat{\phi} + r \dot{\theta} \dot{\phi} \cos \theta \hat{\phi} + r \dot{\phi} \sin \theta \hat{\phi} + r \ddot{\phi} \sin \theta \hat{\phi} + r \dot{\phi} \dot{\theta} \cos \theta \hat{\phi} \end{aligned}$$

$$\begin{aligned} \vec{a} &= (\ddot{r} - r \dot{\theta}^2 - r \dot{\phi}^2 \sin^2 \theta) \hat{r} + \\ &\quad (r \ddot{\theta} + 2 \dot{r} \dot{\theta} - r \dot{\phi}^2 \sin \theta \cos \theta) \hat{\theta} + \\ &\quad (r \ddot{\phi} \sin \theta + 2 \dot{r} \dot{\phi} \sin \theta + 2 r \dot{\theta} \dot{\phi} \cos \theta) \hat{\phi} \end{aligned}$$



$$\hat{\rho} = \hat{r} \sin \theta + \hat{\theta} \cos \theta$$

$\hat{\rho}$ is in the $\hat{r}$ - $\hat{\theta}$ plane $\hat{z}$

$$\frac{\partial \hat{r}}{\partial r} = 0, \frac{\partial \hat{\theta}}{\partial r} = 0, \frac{\partial \hat{\phi}}{\partial r} = 0$$

$$\frac{\partial \hat{r}}{\partial \theta} = \hat{\theta}, \frac{\partial \hat{\theta}}{\partial \theta} = -\hat{r}, \frac{\partial \hat{\phi}}{\partial \theta} = 0$$

$$\frac{\partial \hat{r}}{\partial \phi} = \sin \theta \hat{\phi}, \frac{\partial \hat{\theta}}{\partial \phi} = \cos \theta \hat{\phi}$$

$$\frac{\partial \hat{\phi}}{\partial \phi} = -\hat{\rho} = -\sin \theta \hat{r} - \cos \theta \hat{\theta}$$

(c)

$$\vec{L}_0 = \vec{r} \times m\vec{v}$$

$$= r\hat{r} \times m(\dot{r}\hat{r} + r\dot{\theta}\hat{\theta} + r\dot{\phi}\sin\theta\hat{\phi})$$

$$= r\hat{r} \times m r \dot{\theta} \hat{\theta} + r\hat{r} \times r \dot{\phi} \sin\theta \hat{\phi}$$

$$\hat{r} \times \hat{\theta} = \hat{\phi}$$

$$\hat{r} \times \hat{\phi} = -\hat{\theta}$$

$$\vec{L}_0 = m r^2 \dot{\theta} \hat{\phi} - r^2 \dot{\phi} \sin\theta \hat{\theta}$$

$$\vec{F}_r = m\vec{a}_r$$

$$= m(\ddot{r} - r\dot{\theta}^2 - r\dot{\phi}^2 \sin\theta)\hat{r}$$

$$\vec{F}_\theta = m\vec{a}_\theta$$

$$= m(r\ddot{\theta} + 2\dot{r}\dot{\theta} - r\dot{\phi}^2 \sin\theta \cos\theta)\hat{\theta}$$

$$\vec{F}_\phi = m\vec{a}_\phi$$

$$= m(r\dot{\phi} \sin\theta + 2\dot{r}\dot{\phi} \sin\theta + 2r\dot{\theta}\dot{\phi} \cos\theta)\hat{\phi}$$

$$\vec{N} = \vec{r} \times \vec{F}$$

$$= \vec{r} \times (\vec{F}_r + \vec{F}_\theta + \vec{F}_\phi)$$

$$= r\hat{r} \times \vec{F}_r + r\hat{r} \times \vec{F}_\theta + r\hat{r} \times \vec{F}_\phi$$

$$= 0 + m(r^2\ddot{\theta} + 2r\dot{r}\dot{\theta} - r^2\dot{\phi}^2 \sin\theta \cos\theta)\hat{\phi} - m(r^2\dot{\phi} \sin\theta + 2r\dot{r}\dot{\phi} \sin\theta + 2r^2\dot{\theta}\dot{\phi} \cos\theta)\hat{\theta}$$

$$\frac{d\vec{L}_0}{dt} = \frac{d}{dt}(\vec{r} \times m\vec{v})$$

$$= \vec{r} \times \frac{d}{dt}(m\vec{v}) + \frac{d\vec{r}}{dt} \times m\vec{v}$$

$$= \vec{r} \times m \frac{d\vec{v}}{dt} + \vec{v} \times m\vec{v}$$

$$= \vec{r} \times m \frac{d\vec{v}}{dt}$$

$$= r\hat{r} \times m\vec{a}$$

$$= r\hat{r} \times m[(\ddot{r} - r\dot{\theta}^2 - r\dot{\phi}^2 \sin\theta)\hat{r} + (r\ddot{\theta} + 2\dot{r}\dot{\theta} - r\dot{\phi}^2 \sin\theta \cos\theta)\hat{\theta} + (r\dot{\phi} \sin\theta + 2\dot{r}\dot{\phi} \sin\theta + 2r\dot{\theta}\dot{\phi} \cos\theta)\hat{\phi}]$$

$$= 0 + m(r^2\ddot{\theta} + 2r\dot{r}\dot{\theta} - r^2\dot{\phi}^2 \sin\theta \cos\theta)\hat{\phi} - m(r^2\dot{\phi} \sin\theta + 2r\dot{r}\dot{\phi} \sin\theta + 2r^2\dot{\theta}\dot{\phi} \cos\theta)\hat{\theta}$$

$$\frac{d\vec{L}_0}{dt} = \vec{N}$$

3-29

$$x_m = (mV_{x0}/b)(1-\delta) \quad \delta \ll 1, \quad \frac{bV_{x0}}{mg} \gg 1$$

$$z = \left(\frac{mg}{bV_{x0}} + \frac{V_{z0}}{V_{x0}} \right) x - \frac{m^2 g}{b^2} \ln \left(\frac{mV_{x0}}{mV_{x0} - bx} \right)$$

$$0 = \left(\frac{mg}{bV_{x0}} + \frac{V_{z0}}{V_{x0}} \right) \left(\frac{mV_{x0}}{b} \right) (1-\delta) - \frac{m^2 g}{b^2} \ln \left(\frac{mV_{x0}}{mV_{x0} - mV_{x0}(1-\delta)} \right)$$

$$= \frac{m^2 g}{b^2} + \frac{mV_{x0}}{b} - \frac{mg}{bV_{x0}} \delta - \frac{V_{z0}}{V_{x0}} \delta + \frac{m^2 g}{b^2} \ln(1 - (1-\delta))$$

$$= \frac{m^2 g}{b^2} + \frac{mV_{x0}}{b} + \frac{m^2 g}{b^2} \ln \delta \quad \{ \delta \ll 1 \}$$

$$-\frac{m^2 g}{b^2} \ln \delta = \frac{m^2 g}{b^2} + \frac{mV_{x0}}{b}$$

$$\ln \delta = -1 - \frac{bV_{x0}}{mg}$$

V_{x0} is of same order as V_{z0}

$$\ln \delta = -\frac{bV_{x0}}{mg}$$

$$\ln \delta = -\frac{bV_{x0}}{mg}$$

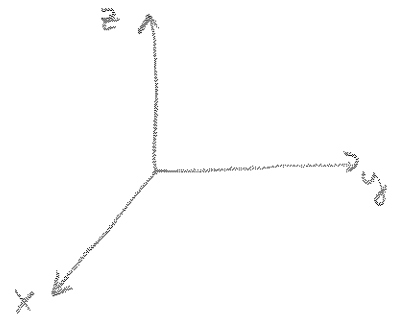
$$\delta = e^{-\frac{bV_{x0}}{mg}}$$

3-31

$$\vec{v}_0 = (v_{x0}, v_{y0}, v_{z0}) \quad \vec{v}_w = w \hat{y}$$

$$m \frac{d\vec{r}}{dt} = -mg\hat{z} - b\left(\frac{d\vec{r}}{dt} - \vec{v}_w\right)$$

$$= -mg\hat{z} - b\frac{d\vec{r}}{dt} + bw\hat{y}$$



$$m \frac{dz}{dt} = -bv_z$$

$$m \frac{dz}{dt} = -bv_z + bw$$

$$m \frac{dz}{dt} = -mg - bv_z$$

$$m \frac{dv_x}{dt} = -bv_x$$

$$m \frac{dv_x}{dt} = -bv_x + bw$$

(next page)

$$\int_{v_{x0}}^v \frac{dv_x}{v_x} = \int_0^t -\frac{b}{m} dt$$

$$\frac{dv_y}{dt} = -\frac{b}{m}(v_y - w)$$

$$\ln v - \ln v_{x0} = -\frac{b}{m}t$$

$$\int_{v_{y0}}^v \frac{dv_y}{(v_y - w)} = -\frac{b}{m}t$$

$$\ln\left(\frac{v}{v_{x0}}\right) = -\frac{b}{m}t$$

$$\ln\left(\frac{v_y - w}{v_{y0} - w}\right) = -\frac{b}{m}t$$

$$\frac{v}{v_{x0}} = e^{-\frac{b}{m}t}$$

$$\frac{v_y - w}{v_{y0} - w} = e^{-\frac{b}{m}t}$$

$$v = v_{x0} e^{-\frac{b}{m}t}$$

$$v_y - w = (v_{y0} - w) e^{-\frac{b}{m}t}$$

$$\frac{dv}{dt} = -v_{x0} e^{-\frac{b}{m}t}$$

$$v_y = (v_{y0} - w) e^{-\frac{b}{m}t} + w$$

$$x(0) = 0 \quad \int_0^x dx = \int_0^t v_{x0} e^{-\frac{b}{m}t} dt$$

$$\frac{dy}{dt} = (v_{y0} - w) e^{-\frac{b}{m}t} + w$$

$$x = -\frac{v_{x0}m}{b} e^{-\frac{b}{m}t} + \frac{v_{x0}m}{b}$$

$$\int_0^y dy = \int_0^t \left[(v_{y0} - w) e^{-\frac{b}{m}t} + w \right] dt$$

$$x = \frac{mv_{x0}}{b} (1 - e^{-\frac{b}{m}t})$$

$$y = -\frac{m}{b}(v_{y0} - w) e^{-\frac{b}{m}t} + wt + \frac{m}{b}(v_{y0} - w)$$

$$y = \frac{m}{b}(v_{y0} - w)(1 - e^{-\frac{b}{m}t}) + wt$$

$$m \frac{d^2 z}{dt^2} = -mg - b v_z$$

$$m \frac{dv_z}{dt} = -mg - b v_z$$

$$\begin{aligned} \frac{dv_z}{dt} &= -g - \frac{b}{m} v_z \\ &= -g \left(1 + \frac{b}{mg} v_z \right) \end{aligned}$$

$$\frac{dv_z}{\left(1 + \frac{b}{mg} v_z \right)} = -g dt$$

$$\int_{v_{z0}}^{v_z} \frac{dv_z}{\left(1 + \frac{b}{mg} v_z \right)} = - \int_0^t g dt$$

$$\frac{mg}{b} \ln \left(1 + \frac{b}{mg} v_z \right) \Big|_{v_{z0}}^{v_z} = -gt$$

$$\frac{mg}{b} \ln \left(\frac{mg + b v_z}{mg} \right) \Big|_{v_{z0}}^{v_z} = -gt$$

$$\ln \left(\frac{mg + b v_z}{mg + b v_{z0}} \right) = -\frac{b}{m} t$$

$$\frac{mg + b v_z}{mg + b v_{z0}} = e^{-\frac{b}{m} t}$$

$$mg + b v_z = (mg + b v_{z0}) e^{-\frac{b}{m} t}$$

$$v_z = \left(\frac{mg}{b} + v_{z0} \right) e^{-\frac{b}{m} t} - \frac{mg}{b}$$

$$\frac{dz}{dt} = \left(\frac{mg}{b} + v_{z0} \right) e^{-\frac{b}{m} t} - \frac{mg}{b}$$

$$\int_0^t dz = \int_0^t \left[\left(\frac{mg}{b} + v_{z0} \right) e^{-\frac{b}{m} t} - \frac{mg}{b} \right] dt$$

$$z = -\frac{m}{b} \left(\frac{mg}{b} + v_{z0} \right) e^{-\frac{b}{m} t} - \frac{mg}{b} t + \frac{m}{b} \left(\frac{mg}{b} + v_{z0} \right)$$

$$z = \left(\frac{m^2 g}{b^2} + \frac{m v_{z0}}{b} \right) \left(1 - e^{-\frac{b}{m} t} \right) - \frac{mg}{b} t$$

$$x = \frac{V_{x0}m}{b}(1 - e^{-\frac{b}{m}t}) \quad y = \frac{m}{b}(V_{y0} - w)(1 - e^{-\frac{b}{m}t}) + wt$$

$$\frac{bx}{mV_{x0}} = 1 - e^{-\frac{b}{m}t}$$

$$\frac{by}{m(V_{y0} - w)} = 1 - e^{-\frac{b}{m}t} + wt$$

$$\frac{bx}{mV_{x0}} - 1 = -e^{-\frac{b}{m}t}$$

$$1 - \frac{bx}{mV_{x0}} = e^{-\frac{b}{m}t}$$

$$\ln\left(1 - \frac{bx}{mV_{x0}}\right) = -\frac{b}{m}t$$

$$-\frac{m}{b} \ln\left(\frac{mV_{x0} - bx}{mV_{x0}}\right) = t$$

$$t = \frac{m}{b} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)$$

$$z = \left(\frac{m^2 a}{b^2} + \frac{mV_{z0}}{b}\right)(1 - e^{-\frac{b}{m}t}) - \frac{ma}{b}t$$

$$= \left(\frac{m^2 a}{b^2} + \frac{mV_{z0}}{b}\right)\left(1 - e^{-\frac{b}{m}\left(\frac{m}{b} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)\right)}\right) - \frac{ma}{b}\left(\frac{m}{b} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)\right)$$

$$= \left(\frac{m^2 a}{b^2} + \frac{mV_{z0}}{b}\right)\left(1 - \frac{1}{\frac{mV_{x0}}{mV_{x0} - bx}}\right) - \frac{m^2 a}{b^2} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)$$

$$= \left(\frac{m^2 a}{b^2} + \frac{mV_{z0}}{b}\right)\left(1 - \frac{mV_{x0} - bx}{mV_{x0}}\right) - \frac{m^2 a}{b^2} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)$$

$$= \left(\frac{m^2 a}{b^2} + \frac{mV_{z0}}{b}\right)\left(\frac{mV_{x0} - mV_{x0} + bx}{mV_{x0}}\right) - \frac{m^2 a}{b^2} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)$$

$$= \left(\frac{m^2 a}{b^2} + \frac{mV_{z0}}{b}\right)\left(\frac{bx}{mV_{x0}}\right) - \frac{m^2 a}{b^2} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)$$

$$= \left(\frac{ma}{bV_{x0}} + \frac{V_{z0}}{V_{x0}}\right)x - \frac{m^2 a}{b^2} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx}\right)$$

$$= \left(\frac{ma}{bV_{x0}} + \frac{V_{z0}}{V_{x0}}\right)x + \frac{m^2 a}{b^2} \ln\left(\frac{mV_{x0} - bx}{mV_{x0}}\right)$$

$$z = \left(\frac{ma}{bV_{x0}} + \frac{V_{z0}}{V_{x0}}\right)x + \frac{m^2 a}{b^2} \ln\left(1 - \frac{bx}{mV_{x0}}\right)$$

$$\frac{bx}{mV_{x0}} \ll 1$$

$$\ln(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \dots$$

$$z = \left(\frac{mg}{bV_{x0}} + \frac{V_{z0}}{V_{x0}} \right) x + \frac{m^2 a}{b^2} \left[\frac{-bx}{mV_{x0}} - \frac{b^2}{2m^2 V_{x0}^2} x^2 - \frac{b^3}{3m^3 V_{x0}^3} x^3 - \dots \right]$$

$$= \frac{mg}{bV_{x0}} x + \frac{V_{z0}}{V_{x0}} x - \frac{mg}{bV_{x0}} x - \frac{g}{2V_{x0}^2} x^2 - \frac{bg}{3mV_{x0}^3} x^3 -$$

$$= \frac{V_{z0}}{V_{x0}} x - \frac{g}{2V_{x0}^2} x^2 - \frac{bg}{3mV_{x0}^3} x^3$$

$$= x \left(\frac{V_{z0}}{V_{x0}} - \frac{g}{2V_{x0}^2} x - \frac{bg}{3mV_{x0}^3} x^2 \right)$$

Setting $z=0$ gives x_m

$$0 = \frac{V_{z0}}{V_{x0}} - \frac{g}{2V_{x0}^2} x - \frac{bg}{3mV_{x0}^3} x^2$$

$$\frac{g}{2V_{x0}^2} x_m = \frac{V_{z0}}{V_{x0}} - \frac{bg}{3mV_{x0}^3} x_m^2$$

$$x_m = \frac{2V_{z0}V_{x0}}{g} - \frac{2}{3} \frac{b}{mV_{x0}} x_m^2$$

First approximation

$$x_m \doteq \frac{2V_{z0}V_{x0}}{g}$$

Substitute this approximation into the previous equation to find first order terms of b .

$$x_m \doteq \frac{2V_{z0}V_{x0}}{g} - \frac{2}{3} \frac{b}{mV_{x0}} \left(\frac{2V_{z0}V_{x0}}{g} \right)^2$$

$$x_m \doteq \frac{2V_{z0}V_{x0}}{g} - \frac{8}{3} \frac{bV_{z0}^2V_{x0}}{mg^2}$$

$$\boxed{x_{1m} = \frac{2V_{z0}V_{x0}}{g} - \frac{8}{3} \frac{bV_{z0}^2V_{x0}}{mg^2}}$$

$$t_m = \frac{m}{b} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx_m}\right)$$

$$y_m = \frac{m}{b} (V_{y0} - w)(1 - e^{-\frac{b}{m}t}) + wt_m$$

$$= \frac{m}{b} (V_{y0} - w) \left(1 - \frac{1}{\frac{mV_{x0}}{mV_{x0} - bx_m}}\right) + w \frac{m}{b} \ln\left(\frac{mV_{x0}}{mV_{x0} - bx_m}\right)$$

$$= \frac{m}{b} (V_{y0} - w) \left(1 - \frac{mV_{x0} - bx_m}{mV_{x0}}\right) - w \frac{m}{b} \ln\left(\frac{mV_{x0} - bx_m}{mV_{x0}}\right)$$

$$= \frac{m}{b} (V_{y0} - w) \left(\frac{mV_{x0} - mV_{x0} + bx_m}{mV_{x0}}\right) - w \frac{m}{b} \ln\left(1 - \frac{bx_m}{mV_{x0}}\right)$$

$$= \frac{m}{b} (V_{y0} - w) \left(\frac{bx_m}{mV_{x0}}\right) - w \frac{m}{b} \ln\left(1 - \frac{bx_m}{mV_{x0}}\right)$$

$$y_m = \frac{V_{y0} - w}{V_{x0}} x_m - w \frac{m}{b} \ln\left(1 - \frac{bx_m}{mV_{x0}}\right) \quad \frac{bx}{mV_{x0}} \ll 1$$

$$-w \frac{m}{b} \ln\left(1 - \frac{bx_m}{mV_{x0}}\right) = -w \frac{m}{b} \left(-\frac{bx_m}{mV_{x0}} - \frac{b^2}{2m^2V_{x0}^2} x_m^2 - \frac{b^3}{3m^3V_{x0}^3} x_m^3 - \dots \right)$$

$$= -w \left(\frac{-x_m}{V_{x0}} - \frac{b}{2mV_{x0}^2} x_m^2 - \text{higher orders of } b \right)$$

$$= -w \left(\left(\frac{2V_{x0}}{g} + \frac{8}{3} \frac{bV_{x0}^2}{mg^2} \right) - \frac{b}{2mV_{x0}^2} \left[\frac{2V_{x0}V_{x0}}{g} - \frac{8}{3} \frac{bV_{x0}^2V_{x0}}{mg^2} \right]^2 \right)$$

$$= -w \left(\frac{2V_{x0}}{g} + \frac{8}{3} \frac{bV_{x0}^2}{mg^2} - \frac{b}{2mV_{x0}^2} \left(\frac{4V_{x0}^2V_{x0}}{g^2} + b \text{ and higher terms} \right) \right)$$

$$= -w \left(\frac{2V_{x0}}{g} + \frac{8}{3} \frac{bV_{x0}^2}{mg^2} - \frac{2bV_{x0}^2}{mg^2} \right)$$

$$y_m = \frac{V_{y0} - w}{V_{x0}} \left(\frac{2V_{x0}V_{x0}}{g} - \frac{8}{3} \frac{bV_{x0}^2V_{x0}}{mg^2} \right) - w \left(\frac{2V_{x0}}{g} + \frac{8}{3} \frac{bV_{x0}^2}{mg^2} - \frac{2bV_{x0}^2}{mg^2} \right)$$

$$= (V_{y0} - w) \left(\frac{2V_{x0}}{g} - \frac{8}{3} \frac{bV_{x0}^2}{mg^2} \right) + w \left(\frac{2V_{x0}}{g} - \frac{8}{3} \frac{bV_{x0}^2}{mg^2} + \frac{2bV_{x0}^2}{mg^2} \right)$$

$$= \frac{2V_{x0}V_{y0}}{g} - \frac{8}{3} \frac{bV_{x0}^2V_{y0}}{mg^2} - \frac{2V_{x0}w}{g} + \frac{8}{3} \frac{bV_{x0}^2w}{mg^2} + \frac{2V_{x0}w}{g} - \frac{8}{3} \frac{bV_{x0}^2w}{mg^2} + \frac{2bV_{x0}^2w}{mg^2}$$

$$y_m = \frac{2V_{x0}V_{y0}}{g} - \frac{8}{3} \frac{bV_{x0}^2V_{y0}}{mg^2} + \frac{2bV_{x0}^2w}{mg^2}$$

$$y_{gm} = \frac{2V_{x0}V_{y0}}{g} - \frac{8}{3} \frac{bV_{x0}^2V_{y0}}{mg^2} + \frac{2bV_{x0}^2w}{mg^2}$$

Neglecting b and $\vec{v}_w$

$$x = V_{x0}t$$

$$y = V_{y0}t$$

$$z = V_{z0}t - \frac{1}{2}gt^2$$

$$z_{\max} = \frac{V_{z0}^2}{2g} \rightarrow -\frac{1}{2}gt_m^2 + V_{z0}t_m - \frac{V_{z0}^2}{2g} = 0$$

$$t_m^2 - \frac{2V_{z0}}{g}t_m + \frac{V_{z0}^2}{g^2} = 0$$

$$\left(t_m - \frac{V_{z0}}{g}\right)^2 = 0$$

$$t_m = \frac{V_{z0}}{g}$$

$$t_r = 2t_m$$

$$t_r = \frac{2V_{z0}}{g}$$

$$x_m = \frac{2V_{z0}V_{x0}}{g} \quad y_m = \frac{2V_{z0}V_{y0}}{g}$$

with air resistance alone

$$x_{1m_b} = \frac{2V_{z0}V_{x0}}{g} - \frac{8}{3} \frac{bV_{z0}^2V_{x0}}{mg^2}$$

$$\frac{x_{1m_b} - x_m}{x_m} = \frac{-\frac{8}{3} \frac{bV_{z0}^2V_{x0}}{mg^2}}{\frac{2V_{z0}V_{x0}}{g}} = -\frac{8}{3} \frac{bV_{z0}^2V_{x0}}{mg^2} \cdot \frac{g}{2V_{z0}V_{x0}}$$

$$\boxed{\frac{x_{1m_b} - x_m}{x_m} = -\frac{4bV_{z0}}{3mg}}$$

$$y_{1m_b} = \frac{2V_{z0}V_{y0}}{g} - \frac{8}{3} \frac{bV_{z0}^2V_{y0}}{mg^2}, w=0$$

$$\boxed{\frac{y_{1m_b} - y_m}{y_m} = -\frac{4bV_{z0}}{3mg}}$$

$$w \neq 0 \text{ additional miss} = \frac{2bV_{z0}^2w}{mg^2}$$

3-33

$$a) z = -\frac{1}{2}gt^2 + V_{20}t$$

$$= t\left(-\frac{1}{2}gt + V_{20}\right)$$

$$0 = t\left(-\frac{1}{2}gt + V_{20}\right)$$

$$t=0 \text{ or}$$

$$t = \frac{2V_{20}}{g}$$

$$= \frac{2V_0 \sin \theta}{g}$$

$$x = V_{x0}t$$

$$= (V_0 \cos \theta) \left(\frac{2V_0 \sin \theta}{g} \right)$$

$$= \frac{V_0^2 2 \sin \theta \cos \theta}{g}$$

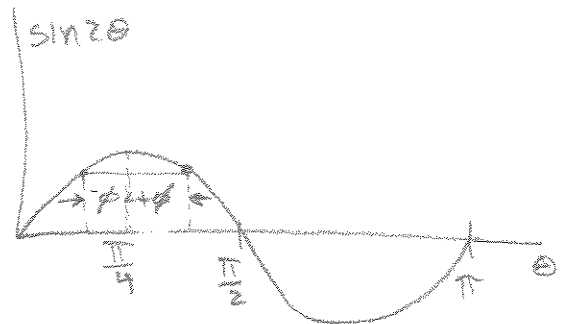
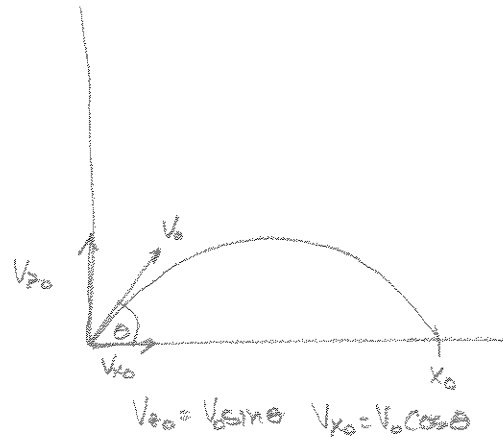
$$x = \frac{V_0^2 \sin 2\theta}{g}$$

$$x = x_m \text{ at } \theta_m = \frac{\pi}{4}$$

$$\boxed{\theta = \sin^{-1}\left(\frac{x_m}{V_0^2}\right)/2}$$

$$\frac{x_m}{V_0^2} = 2\cos^2\phi - 1, \quad x < x_m \quad \theta = \frac{\pi}{4} \pm \phi$$

$$\boxed{\pm \left(\frac{x_m}{2V_0^2} + \frac{1}{2} \right)^{1/2} = \cos \phi, \quad \cos \phi = \cos(-\phi)}$$



$$\sin 2\theta = \sin(2(\theta_m \pm \phi))$$

$$= \sin\left(\frac{\pi}{2} \pm 2\phi\right)$$

$$= \sin \frac{\pi}{2} \cos 2\phi \pm \sin 2\phi \cos \frac{\pi}{2}$$

$$= \cos 2\phi$$

$$= 2\cos^2\phi - 1$$

b) First order correction

$$X \doteq \frac{2V_{x0}V_{z0}}{g} - \frac{8}{3} \frac{bV_{z0}^2 V_{x0}}{mg^2}$$

$$\Delta X = -\frac{8}{3} \frac{bV_{z0}^2 V_{x0}}{mg^2}$$

with $b=0$

$$X = \frac{2V_0^2 \sin\theta \cos\theta}{g}$$

$$\frac{dX}{d\theta} = \frac{2V_0^2}{g} (-\sin^2\theta + \cos^2\theta)$$

$$\Delta X = \frac{2V_0^2}{g} (\cos^2\theta - \sin^2\theta) \Delta\theta$$

To offset ΔX , $-\Delta X$ must be found

$$\frac{8}{3} \frac{b}{mg^2} V_0^2 \sin^2\theta V_0 \cos\theta = \frac{2V_0^2}{g} (\cos^2\theta - \sin^2\theta) \Delta\theta$$

$$\frac{4}{3} \frac{bV_0}{mg} \cos\theta = \frac{(\cos^2\theta - \sin^2\theta) \Delta\theta}{\sin^2\theta}$$

$$= (\cot^2\theta - 1) \Delta\theta$$

$$\Delta\theta = \frac{4bV_0 \cos\theta}{3mg(\cot^2\theta - 1)}$$

3-35

$$a) F_x = 6abz^3y - 20bx^3y^2, F_y = 6abxz^3 - 10bx^4y, F_z = 18abxz^2y$$

$$\vec{\nabla} \times \vec{F} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 6abz^3y - 20bx^3y^2 & 6abxz^3 - 10bx^4y & 18abxz^2y \end{vmatrix}$$

$$= \hat{x}(18abxz^2 - (18abz^2)) + \hat{y}(18abz^2y - 18abz^2y) + \hat{z}(6abz^3 - 40bx^3y - (6abz^3 - 40bx^3y))$$

$$= 0 \rightarrow \text{conservative force}$$

$$V = - \int_{r_0}^r \vec{F} \cdot d\vec{r}$$

$$d\vec{r} = dx \hat{x} + dy \hat{y} + dz \hat{z}$$

$$= - \int_{x=0, y=0, z=0}^{x=x_0, y=y_0, z=z_0} (6abz^3y - 20bx^3y^2) dx - \int_{x=x_0, y=0, z=0}^{x=x_0, y=y_0, z=0} (6abxz^3 - 10bx^4y) dy - \int_{x=x_0, y=y_0, z=0}^{x=x_0, y=y_0, z=z_0} 18abxz^2y dz$$

$$= 0 - (-5x_0^4y_0^2) - 6abx_0y_0z_0^3$$

$$V = 5x^4y^2 - 6abxyz^3$$

$$b) F_x = 18abyz^3 - 20bx^3y^2, F_y = 18abxz^3 - 10bx^4y, F_z = 6abxyz^2$$

$$\vec{\nabla} \times \vec{F} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 18abyz^3 - 20bx^3y^2 & 18abxz^3 - 10bx^4y & 6abxyz^2 \end{vmatrix}$$

$$= \hat{x}(6abxz^2 - 56abxz^2) +$$

$$\neq 0 \rightarrow \text{not conservative}$$

$$c) \quad \vec{F} = F_x(x) \hat{x} + F_y(y) \hat{y} + F_z(z) \hat{z}$$

Since $\vec{F}$ only has components in the unit vector directions

$$\vec{\nabla} \times \vec{F} = 0$$

$$V = - \int_{x_0}^x F_x(x) dx - \int_{y_0}^y F_y(y) dy - \int_{z_0}^z F_z(z) dz$$

$$a) F_x = axe^{-R}, F_y = bye^{-R}, F_z = cze^{-R}, R = ax^2 + by^2 + cz^2$$

$$V = - \int_{r_0}^r \vec{F} \cdot d\vec{r} \quad d\vec{r} = dx\hat{x} + dy\hat{y} + dz\hat{z}$$

$$= - \int_{x=0, y=0, z=0}^{x=x_0, y=0, z=0} axe^{-ax^2} dx - \int_{x=x_0, y=0, z=0}^{x=x_0, y=y_0, z=0} bye^{-ax_0^2 - by^2} dy - \int_{x=x_0, y=y_0, z=0}^{x=x_0, y=y_0, z=z_0} cze^{-ax_0^2 - by_0^2 - cz^2} dz$$

$$u = -ax^2 \quad du = -2ax dx \quad -\frac{du}{2} = ax dx$$

$$u = -ax_0^2 - by^2 \quad du = -2by dy \quad -\frac{du}{2} = by dy$$

$$u = -ax_0^2 - by_0^2 - cz^2 \quad du = -2c dz \quad -\frac{du}{2} = cz dz$$

$$V = \frac{e^{-ax^2}}{2} \Big|_0^{x_0} + \frac{e^{-ax_0^2 - by^2}}{2} \Big|_0^{y_0} + \frac{e^{-ax_0^2 - by_0^2 - cz^2}}{2} \Big|_0^{z_0}$$

$$= \frac{1}{2} \left[e^{-ax_0} - 1 + e^{-ax_0^2 - by_0^2} - e^{-ax_0^2 - by_0^2 - cz_0^2} - e^{-ax_0^2 - by_0^2} \right]$$

$$= \frac{1}{2} \left[e^{-ax^2 - by^2 - cz^2} - 1 \right]$$

$$= \frac{1}{2} e^{-R} - \frac{1}{2}, \quad V=0 \text{ at } x=y=z=0, \text{ so the constant can be dropped since}$$

$$\boxed{V = \frac{1}{2} e^{-R}}$$

$$\vec{F} = -\vec{\nabla} V$$

$$b) \vec{F} = \vec{A} f(\vec{A} \cdot \vec{r}) \text{ where } \vec{A} \text{ is a constant vector, } f(s) \text{ where } s = \vec{A} \cdot \vec{r}$$

$$V = - \int_{r_0}^r \vec{F} \cdot d\vec{r}$$

$$= - \int_0^s f(s) \vec{A} \cdot d\vec{r} \quad s = \vec{A} \cdot \vec{r}, \quad ds = \vec{A} \cdot d\vec{r}$$

$$\boxed{V = - \int_0^s f(s) ds}$$

$$c) \vec{F} = (\vec{r} \times \vec{A}) f(\vec{A} \cdot \vec{r})$$

$$\vec{r} = x\hat{x} + y\hat{y} + z\hat{z}$$

$$\vec{A} = A_x\hat{x} + A_y\hat{y} + A_z\hat{z}$$

$$(\vec{r} \times \vec{A}) = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ x & y & z \\ A_x & A_y & A_z \end{vmatrix}$$

$$= (yA_z - zA_y)\hat{x} + (zA_x - xA_z)\hat{y} + (xA_y - yA_x)\hat{z}$$

$$\vec{A} \cdot \vec{r} = xA_x + yA_y + zA_z$$

$$F_x = (yA_z - zA_y) f(xA_x + yA_y + zA_z)$$

$$F_y = (zA_x - xA_z) f(xA_x + yA_y + zA_z)$$

$$F_z = (xA_y - yA_x) f(xA_x + yA_y + zA_z)$$

$$V = - \int \vec{F} \cdot d\vec{r} \quad d\vec{r} = dx\hat{x} + dy\hat{y} + dz\hat{z}$$

$$= - \int_{x=x_0, y=0, z=0}^{x=x_0, y=y_0, z=0} (yA_z - zA_y) f(\vec{A} \cdot \vec{r}) dx - \int_{x=x_0, y=0, z=0}^{x=x_0, y=y_0, z=0} (zA_x - xA_z) f(\vec{A} \cdot \vec{r}) dy - \int_{x=x_0, y=0, z=0}^{x=x_0, y=y_0, z=0} (xA_y - yA_x) f(\vec{A} \cdot \vec{r}) dz$$

$$= 0 + x_0 A_z \left[\int_0^{y_0} (x_0 A_x + y A_y) dy - (x_0 A_y - y_0 A_x) \int_0^z (x_0 A_x + y_0 A_y + z A_z) dz \right]$$

$$V = x A_z \int_0^{y_0} f(x A_x + y A_y) dy - (x A_y - y A_x) \int_0^z f(x A_x + y A_y + z A_z) dz$$

3-39

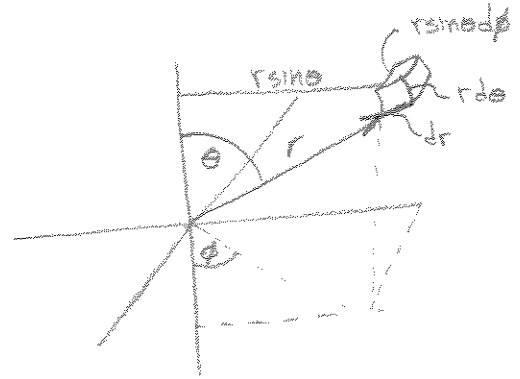
$$\vec{F} = \hat{r} F(r)$$

$$\vec{F} = F(r) \hat{r} + 0 \hat{\theta} + 0 \hat{\phi}$$

$$\int_{r_1}^{r_2} \vec{F} \cdot d\vec{r} = \int_{r_1}^{r_2} F_r dr$$

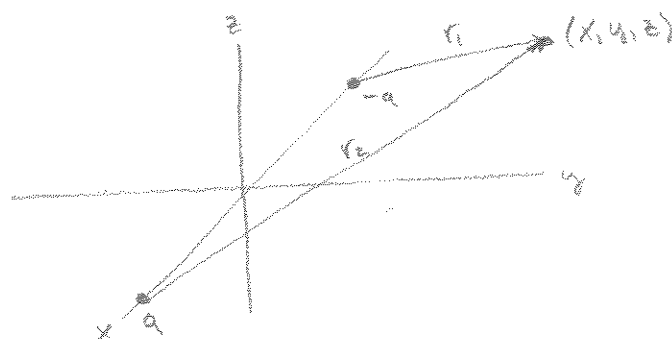
$$= V(r_2) - V(r_1) \quad \left\{ \begin{array}{l} \text{Fundamental} \\ \text{Theorem of} \\ \text{Calculus} \end{array} \right\}$$

$$d\vec{r} = dr \hat{r} + r d\theta \hat{\theta} + r \sin\theta d\phi \hat{\phi}$$



3-41

$$V = -\frac{e^2}{r_1} - \frac{e^2}{r_2}$$



$$\vec{r}_1 = (x+a)\hat{x} + y\hat{y} + z\hat{z} \quad \vec{r}_2 = (x-a)\hat{x} + y\hat{y} + z\hat{z}$$

$$\vec{F} = -\vec{\nabla} V$$

$$= -\frac{\partial V}{\partial x}\hat{x} - \frac{\partial V}{\partial y}\hat{y} - \frac{\partial V}{\partial z}\hat{z}$$

$$r_1 = ((x+a)^2 + y^2 + z^2)^{1/2}$$

$$r_2 = ((x-a)^2 + y^2 + z^2)^{1/2}$$

$$F_x = -\frac{\partial V}{\partial x}$$

$$= -\frac{\partial}{\partial x} \left(-\frac{e^2}{r_1} - \frac{e^2}{r_2} \right)$$

$$= e^2 \frac{\partial}{\partial x} \left(\frac{1}{r_1} + \frac{1}{r_2} \right)$$

$$= e^2 \frac{\partial}{\partial x} \left(\frac{1}{((x+a)^2 + y^2 + z^2)^{1/2}} + \frac{1}{((x-a)^2 + y^2 + z^2)^{1/2}} \right)$$

$$= e^2 \frac{\partial}{\partial x} \left(((x+a)^2 + y^2 + z^2)^{-1/2} + ((x-a)^2 + y^2 + z^2)^{-1/2} \right)$$

$$= e^2 \left[-\frac{1}{2} ((x+a)^2 + y^2 + z^2)^{-3/2} 2(x+a) - \frac{1}{2} ((x-a)^2 + y^2 + z^2)^{-3/2} 2(x-a) \right]$$

$$= e^2 \left[-(x+a)r_1^{-3} - (x-a)r_2^{-3} \right]$$

$$= e^2 \left[-xr_1^{-3} - ar_1^{-3} - xr_2^{-3} + ar_2^{-3} \right]$$

$$\boxed{F_x = e^2 \left[-a(r_1^{-3} - r_2^{-3}) - x(r_1^{-3} + r_2^{-3}) \right]}$$

$$\begin{aligned}
 F_y &= -\frac{\partial V}{\partial y} \\
 &= e^2 \frac{\partial}{\partial y} \left(((x+a)^2 + y^2 + z^2)^{-1/2} + ((x-a)^2 + y^2 + z^2)^{-1/2} \right) \\
 &= e^2 \left[-\frac{1}{2} r_1^{-3} 2y - \frac{1}{2} r_2^{-3} 2y \right] \\
 &= -ye^2 [r_1^{-3} + r_2^{-3}]
 \end{aligned}$$

$$\begin{aligned}
 F_z &= -\frac{\partial V}{\partial z} \\
 &= e^2 \frac{\partial}{\partial z} \left(((x+a)^2 + y^2 + z^2)^{-1/2} + ((x-a)^2 + y^2 + z^2)^{-1/2} \right) \\
 &= -ze^2 [r_1^{-3} + r_2^{-3}]
 \end{aligned}$$

3-43 $V(r) = \frac{1}{2}kr^2$

$$V'(r) = V(r) + \frac{L^2}{2mr^2}$$

$$= \frac{1}{2}kr^2 + \frac{L^2}{2mr^2}$$

$$\frac{dV'}{dr} = kr - \frac{L^2}{m} \frac{1}{r^3}$$

$$0 = \frac{kr^4 - \frac{L^2}{m}}{r^3}$$

$$kr_0^4 = \frac{L^2}{m}$$

$$r_0^4 = \frac{L^2}{km}$$

$$r_0^2 = \pm \frac{L}{(km)^{1/2}}$$

$$r_0 = \pm \frac{L^{1/2}}{(km)^{1/4}}$$

$$V'\left(\frac{L^{1/2}}{(km)^{1/4}}\right) = \frac{1}{2}L\left(\frac{k}{m}\right)^{1/2} + \frac{1}{2}L\left(\frac{k}{m}\right)^{1/2}$$

$$= L\left(\frac{k}{m}\right)^{1/2}$$

$$V'\left(\frac{L^{1/2}}{(km)^{1/4}}\right) = L\left(\frac{k}{m}\right)^{1/2}$$

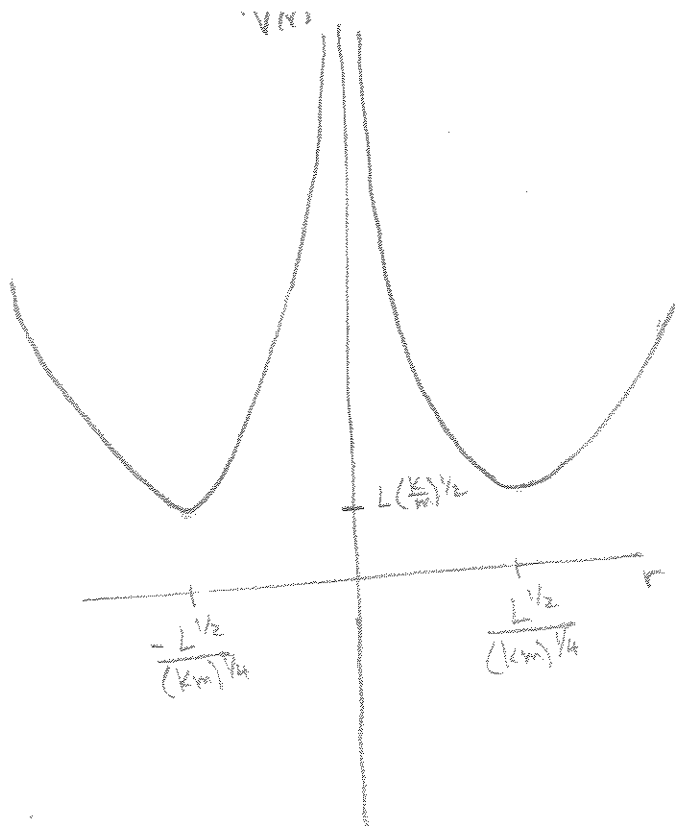
For $E = L\left(\frac{k}{m}\right)^{1/2}$, $r_0^2 = \frac{L}{(km)^{1/2}}$

$$\dot{\theta} = \frac{L}{mr_0^2}$$

$$= \frac{L}{m} \frac{1}{\frac{L}{(km)^{1/2}}}$$

$$= \frac{(km)^{1/2}}{m}$$

$$\dot{\theta} = \left(\frac{k}{m}\right)^{1/2}$$



$$\omega^2 = \frac{1}{m} \left(\frac{d^2V'}{dr^2} \right)_{r_0}, E \geq L\left(\frac{k}{m}\right)^{1/2}$$

$$\frac{d^2V'}{dr^2} = \frac{d}{dr} \left(kr - \frac{L^2}{m} \frac{1}{r^3} \right)$$

$$= k + \frac{3L^2}{m} \frac{1}{r^4}$$

$$\left(\frac{d^2V'}{dr^2} \right)_{r_0} = k + \frac{3L^2}{m} \frac{1}{\frac{L^2}{km}}$$

$$= k + 3k$$

$$\omega^2 = \frac{4k}{m}$$

$$\omega_r = 2\sqrt{\frac{k}{m}}$$

Nature of solutions:

For small E orbit is nearly circular.

For large E , $\dot{r} > \dot{r}_0$ giving an ellipse.

The orbits for $E \geq L\left(\frac{k}{m}\right)^{1/2}$ are bounded with two turning points.

3-45

$$V(r) = \frac{1}{2} Kr^2$$

$$\int_{r_0}^r \frac{dr}{\left[E - V(r) - \frac{L^2}{2mr^2}\right]^{1/2}} = \sqrt{\frac{2}{m}} t$$

$$E - \frac{1}{2} Kr^2 - \frac{L^2}{2mr^2} = \frac{2Emr^2 - Kmr^4 - L^2}{2mr^2}$$

$$= \frac{-Kmr^4 + 2Emr^2 - L^2}{2mr^2}$$

$$-Kmr^4 + 2Emr^2 - L^2 =$$

$$-Km\left(r^4 - \frac{2Er^2}{K} + \frac{L^2}{Km}\right) =$$

$$-Km\left[r^4 - \frac{2Er^2}{K} + \frac{E^2}{K^2} + \frac{L^2}{Km} - \frac{E^2}{K^2}\right] =$$

$$-Km\left[\left(r^2 - \frac{E}{K}\right)^2 - \left(\frac{E^2}{K^2} - \frac{L^2}{Km}\right)\right] =$$

$$Km\left[\frac{E^2}{K^2} - \frac{L^2}{Km} - \left(r^2 - \frac{E}{K}\right)^2\right]$$

$$\int_{r_0}^r \frac{dr}{\left[E - \frac{1}{2} Kr^2 - \frac{L^2}{2mr^2}\right]^{1/2}} = \sqrt{2m} \int_{r_0}^r \frac{r dr}{(-Kmr^4 + 2Emr^2 - L^2)^{1/2}} =$$

$$\sqrt{2m} \int_{r_0}^r \frac{r dr}{\left[Km\left(\frac{E^2}{K^2} - \frac{L^2}{Km} - \left(r^2 - \frac{E}{K}\right)^2\right)\right]^{1/2}} =$$

$$\sqrt{\frac{2}{K}} \int_{r_0}^r \frac{r dr}{\left[\frac{E^2}{K^2} - \frac{L^2}{Km} - \left(r^2 - \frac{E}{K}\right)^2\right]^{1/2}} =$$

$$\text{Let } r^2 - \frac{E}{K} = \frac{\sqrt{E^2 - L^2/Km}}{K} \sin \theta$$

$$2r dr = \frac{\sqrt{E^2 - L^2/Km}}{K} \cos \theta d\theta$$

$$\frac{1}{2} \sqrt{\frac{2}{K}} \int_{\theta_0}^{\theta} \frac{\frac{\sqrt{E^2 - L^2/Km}}{K} \cos \theta d\theta}{\frac{\sqrt{E^2 - L^2/Km}}{K} (1 - \sin^2 \theta)^{1/2}}$$

$$\sqrt{\frac{1}{2K}} \int_{\theta_0}^{\theta} d\theta = \sqrt{\frac{1}{2K}} (\theta - \theta_0)$$

$$\sqrt{\frac{1}{2K}} (\theta - \theta_0) = \sqrt{\frac{2}{m}} t$$

$$\frac{1}{2} (\theta - \theta_0) = \sqrt{\frac{K}{m}} t$$

$$\theta = 2\omega t + \theta_0$$

$$r^2 = \frac{E}{K} - \frac{(E^2 - L^2/Km)^{1/2}}{K} \sin \theta$$

$$Kr^2 = E - (E^2 - L^2\omega^2)^{1/2} \sin(2\omega t + \theta_0), \quad \omega = \sqrt{\frac{K}{m}}$$

3-47

$$V(r) = \frac{K e^{-\alpha r}}{r} \quad K < 0$$

$$\begin{aligned} a) \quad \vec{F} &= -\vec{\nabla} V \\ &= -\frac{dV}{dr} \hat{r} \\ &= -\frac{d}{dr} \left(\frac{K e^{-\alpha r}}{r} \right) \hat{r} \\ &= -\frac{(r(-\alpha K e^{-\alpha r}) - K e^{-\alpha r})}{r^2} \hat{r} \\ &= \frac{r \alpha K e^{-\alpha r} + K e^{-\alpha r}}{r^2} \hat{r} \end{aligned}$$

$$\boxed{\vec{F} = \frac{(1 + \alpha r) K e^{-\alpha r}}{r^2} \hat{r}}$$

The inverse square law force, $\vec{F}_{\text{inv}} = \frac{K}{r^2} \hat{r}$, and the above force are related by

$$\vec{F} = \vec{F}_{\text{inv}} (1 + \alpha r) e^{-\alpha r}$$

So $\vec{F}$ decreases by a factor of $(1 + \alpha r) e^{-\alpha r}$ compared to $\vec{F}_{\text{inv}}$ as r increases.

b)

$$V(r) = \frac{K e^{-\alpha r}}{r}$$

$$\frac{dV(r)}{dr} = -\frac{(1 + \alpha r) K e^{-\alpha r}}{r^2}$$

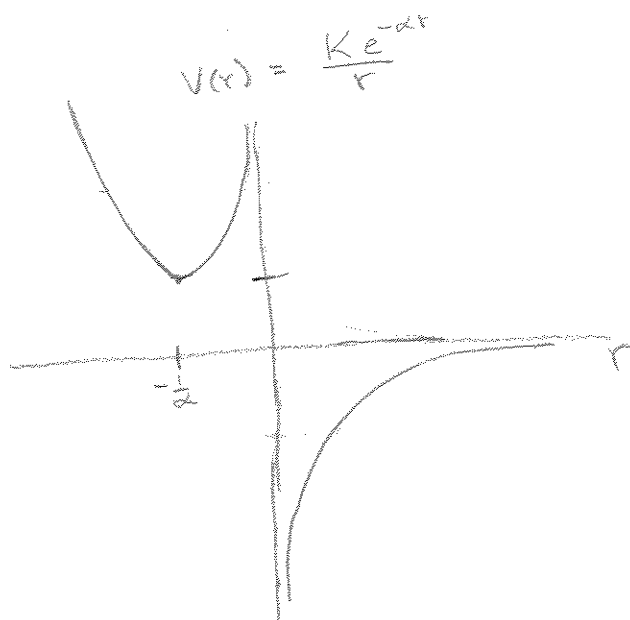
$$0 = (1 + \alpha r) K e^{-\alpha r}$$

$$0 = (1 + \alpha r)$$

$$r_0 = -\frac{1}{\alpha}$$

$$V(r_0) = \frac{K e^{-\frac{1}{\alpha}}}{-\frac{1}{\alpha}}$$

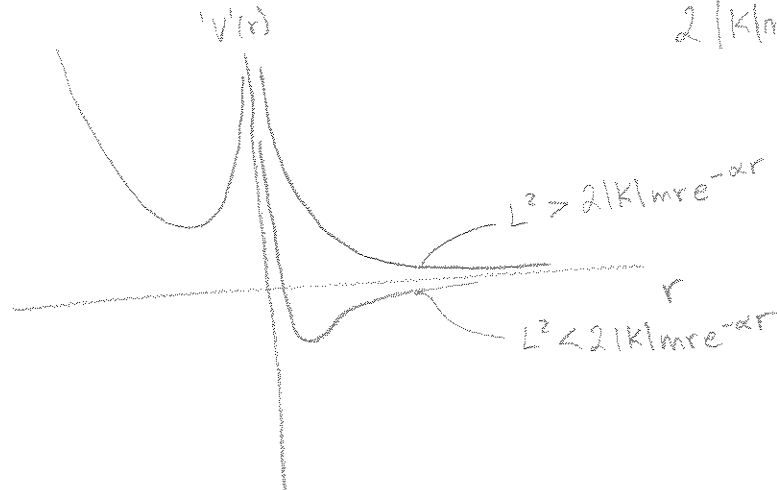
$$= \alpha K e^{-\frac{1}{\alpha}}, K < 0$$



$$V(r) = \frac{Ke^{-\alpha r}}{r} + \frac{L^2}{2mr^2}$$

$$0 > \frac{Ke^{-\alpha r}}{r} + \frac{L^2}{2mr^2}$$

$$2|K|me^{-\alpha r} > L^2$$



$E > 0$, one turning pt., open orbit $r \rightarrow \infty$

$E < 0$, two turning pts., closed orbit

$$d) \frac{dV}{dr} = \frac{-(1+\alpha r)Ke^{-\alpha r}}{r^2} - \frac{L^2}{mr^3}$$

For $r=a$, $\frac{dV}{dr}=0$ to give a circular orbit

$$0 = \frac{-(1+\alpha a)Ke^{-\alpha a}}{a^2} - \frac{L^2}{ma^3}$$

$$\boxed{L^2 = -(1+\alpha a)Ke^{-\alpha a}ma}$$

$$E = \frac{Ke^{-\alpha r}}{r} + \frac{L^2}{2mr^2} \text{ at } r=a$$

$$E = \frac{Ke^{-\alpha a}}{a} + \frac{-maK(1+\alpha a)e^{-\alpha a}}{2ma^2}$$

$$= \frac{Ke^{-\alpha a}}{a} - \frac{K(1+\alpha a)e^{-\alpha a}}{2a}$$

$$= \frac{2Ke^{-\alpha a} - Ke^{-\alpha a} - K\alpha ae^{-\alpha a}}{2a}$$

$$= \frac{Ke^{-\alpha a} - K\alpha ae^{-\alpha a}}{2a}$$

$$\boxed{E = \frac{Ke^{-\alpha a}(1-\alpha a)}{2a}}$$

$$e) i) S = \frac{L^2}{2m} \quad S = \pi a^2$$

$$r = \frac{2mS}{L}$$

$$= \frac{2\pi a^2 m}{(-(1+\alpha)e^{-\alpha a} k m a)^{1/2}}$$

$$r_c = 2\pi [-K(1+\alpha)e^{-\alpha a}/ma^3]^{-1/2}$$

ii)

$$\omega^2 = \frac{1}{m} \left(\frac{d^2 V}{dr^2} \right)_{r=a}$$

$$\frac{d^2 V}{dr^2} = \frac{d}{dr} \left(\frac{-(1+\alpha r) K e^{-\alpha r}}{r^2} - \frac{L^2}{mr^3} \right)$$

$$= \frac{d}{dr} \left(\frac{-K e^{-\alpha r}}{r^2} - \frac{K \alpha r e^{-\alpha r}}{r^2} - \frac{L^2}{mr^3} \right)$$

$$= \frac{r^2 \alpha K e^{-\alpha r} + 2r K e^{-\alpha r}}{r^4} - \frac{K \alpha r^2 (-\alpha e^{-\alpha r} + e^{-\alpha r}) - K \alpha r e^{-\alpha r} 2r}{r^4} + \frac{3L^2}{mr^4}$$

$$= \frac{K \alpha r^2 e^{-\alpha r} + 2K r e^{-\alpha r}}{r^4} - \frac{K \alpha r^2 (-\alpha e^{-\alpha r} + e^{-\alpha r})}{r^4} + \frac{2K \alpha r^2 e^{-\alpha r}}{r^4} + \frac{3L^2}{mr^4}$$

$$= \frac{K \alpha r^2 e^{-\alpha r} + 2K r e^{-\alpha r} + K \alpha^2 r^3 e^{-\alpha r} - K \alpha r^2 e^{-\alpha r} - 2K \alpha r^2 e^{-\alpha r}}{r^4} + \frac{3L^2}{mr^4}$$

$$= \frac{2K r e^{-\alpha r} + 2K \alpha r^2 e^{-\alpha r} + K \alpha^2 r^3 e^{-\alpha r}}{r^4} + \frac{3L^2}{mr^4}$$

$$\omega^2 = \frac{1}{m} \left[\frac{2K \alpha e^{-\alpha a} + 2K \alpha^2 a e^{-\alpha a} + K \alpha^3 a^3 e^{-\alpha a}}{a^4} + \frac{3(-(1+\alpha)e^{-\alpha a} k m a)}{m a^4} \right]$$

$$= \frac{2K \alpha e^{-\alpha a} + 2K \alpha^2 a e^{-\alpha a} + K \alpha^3 a^3 e^{-\alpha a} - 3K \alpha e^{-\alpha a} - 3K \alpha^2 a e^{-\alpha a}}{m a^4}$$

$$= \frac{-K \alpha e^{-\alpha a} - K \alpha^2 a e^{-\alpha a} + K \alpha^3 a^3 e^{-\alpha a}}{m a^4}$$

$$\omega^2 = \frac{-Ka(1+\alpha a - \alpha^2 a^2) e^{-\alpha a}}{ma^4}$$

$$= \frac{-K(1+\alpha a - \alpha^2 a^2) e^{-\alpha a}}{ma^3}$$

$$\frac{2\pi}{T} = \omega = \left(\frac{-K(1+\alpha a - \alpha^2 a^2) e^{-\alpha a}}{ma^3} \right)^{1/2}$$

$$T_r = 2\pi \left(\frac{-K(1+\alpha a - \alpha^2 a^2) e^{-\alpha a}}{ma^3} \right)^{-1/2}$$

f) For closed orbits

$$\omega_c = \omega_r \rightarrow T_c = T_r$$

When a is small, in order for T_c to nearly equal T_r

$$(1+\alpha a) \cong (1+\alpha a - \alpha^2 a^2)$$

So,

$$\alpha^2 a^2 < 1 + \alpha a$$

$$(\alpha a)^2 - \alpha a - 1 < 0$$

$$(\alpha a)^2 - \alpha a + \frac{1}{4} < 1 + \frac{1}{4}$$

$$(\alpha a - \frac{1}{2})^2 < \frac{5}{4}$$

$$\alpha a - \frac{1}{2} < \frac{\sqrt{5}}{2}$$

$$\alpha a < \frac{1+\sqrt{5}}{2} \text{ for stable orbits}$$

3-49

$$F' = -mkr$$

$$K = -\frac{4}{3}\pi\rho G$$

$$F = \frac{K_1}{r^2}$$

$$K_1 = -GMm$$

$$V(r) = -\int \frac{K_1}{r^2} dr$$

$$= \frac{K_1}{r}$$

$$V(r) = -\int -\frac{4}{3}\pi\rho Gmr$$

$$= \frac{2}{3}\pi\rho Gmr^2$$

$$= \frac{K}{2}r^2$$

$$V'(r) = \frac{K_1}{r} + \frac{K}{2}r^2 + \frac{L^2}{mr^2} \quad K_1 < 0, K < 0$$

$$\frac{dV'}{dr} = \frac{K_1}{r^2} + Kr - \frac{L^2}{mr^3}$$

$$= \frac{GMm}{r^2} + \frac{4}{3}\pi\rho Gmr - \frac{L^2}{mr^3}$$

For a circular orbit of r_0

$$\frac{L^2}{mr_0^3} = \frac{GMm}{r_0^2} + \frac{4}{3}\pi\rho Gmr_0$$

$$L^2 = GMmr_0^2 + \frac{4}{3}\pi\rho Gmr_0^4$$

$$L = (GMmr_0^2 + \frac{4}{3}\pi\rho Gmr_0^4)^{1/2}$$

$$\dot{\theta} = \frac{L}{mr_0^2}$$

$$\omega_c = \left(\frac{3GMr_0 + 4\pi\rho Gr_0^3}{3r_0^4} \right)^{1/2}$$

$$\omega_r^2 = \frac{1}{m} \left(\frac{d^2V'}{dr^2} \right)_{r_0}$$

$$\frac{d^2V'}{dr^2} = \frac{d}{dr} \left(\frac{GMm}{r^2} + \frac{4}{3}\pi\rho Gmr - \frac{L^2}{mr^3} \right)$$

$$= -\frac{2GMm}{r^3} + \frac{4}{3}\pi\rho Gm + \frac{3L^2}{mr^4}$$

$$\left(\frac{d^2V'}{dr^2} \right)_{r_0} = -\frac{2GMm}{r_0^3} + \frac{4}{3}\pi\rho Gm + \frac{3L^2}{mr_0^4}$$

$$\begin{aligned}
 \omega_r^2 &= -\frac{2GM}{r_0^3} + \frac{4}{3}\pi\ell G + \frac{3}{m^2 r_0^4} \left(GMm^2 r_0 + \frac{4}{3}\pi\ell G m^2 r_0^4 \right) \\
 &= -\frac{2GM}{r_0^3} + \frac{4}{3}\pi\ell G + \frac{3GM}{r_0^3} + 4\pi\ell G \\
 &= \frac{GM}{r_0^3} + \frac{16\pi\ell G}{3} \\
 &= \frac{GM r_0 + \frac{16}{3}\pi\ell G r_0^4}{r_0^4} \\
 \omega_r &= \left(\frac{3GM r_0 + 16\pi\ell G r_0^4}{3 r_0^4} \right)^{1/2}
 \end{aligned}$$

For F' much less than F , expand ω_c and ω_r

$$\omega_c = \left(\frac{GM}{r_0^3} + \frac{4}{3}\pi\ell G \right)^{1/2} \quad (a+b)^n = a^{1/2} + \frac{1}{2} a^{-1/2} b + \text{higher orders of } b$$

$$a = \frac{GM}{r_0^3}, \quad b = \frac{4}{3}\pi\ell G$$

$$\omega_c \approx \left(\frac{GM}{r_0^3} \right)^{1/2} + \frac{2}{3}\pi\ell G \left(\frac{r_0^3}{GM} \right)^{1/2}$$

$$\omega_r = \left(\frac{GM}{r_0^3} + \frac{16}{3}\pi\ell G \right)^{1/2}$$

$$a = \frac{GM}{r_0^3}, \quad b = \frac{16}{3}\pi\ell G$$

$$\omega_r \approx \left(\frac{GM}{r_0^3} \right)^{1/2} + \frac{8}{3}\pi\ell G \left(\frac{r_0^3}{GM} \right)^{1/2}$$

$$\omega_p = \omega_r - \omega_c = \left(\frac{8}{3} - \frac{2}{3} \right) \pi\ell G \left(\frac{G r_0^3}{M} \right)^{1/2}$$

$$\boxed{\omega_p = 2\pi\ell G \left(\frac{G r_0^3}{M} \right)^{1/2}}$$

b) Since $\omega_r > \omega_c$, r will reach a maximum before $\theta = 180^\circ$. Therefore, the axis of precession will move in the opposite direction of the orbit.

3-51

$$a) F(r) = -\frac{K}{r^2} + \frac{K'}{r^3}, \quad K > 0, K' > 0 \text{ or } K' < 0$$

$$V(r) = -\int \frac{K}{r^2} dr - \int \frac{K'}{r^3} dr, \quad K < 0$$

$$V(r) = -\frac{K}{r} + \frac{K'}{2r^2} + \frac{L^2}{2mr^2} = -\frac{K}{r} + \frac{mK' + L^2}{2mr^2}$$

$$b) \quad mr^2 \dot{\theta} = L$$

$$\dot{\theta} = \frac{L}{mr^2}$$

$$r = \frac{1}{u} \quad u = \frac{1}{r}$$

$$\dot{r} = -\frac{1}{u^2} \frac{du}{dt}$$

$$= -\frac{1}{u^2} \frac{du}{d\theta} \frac{d\theta}{dt}$$

$$= -\frac{1}{u^2} \frac{du}{d\theta} \frac{L}{m} u^2$$

$$\dot{r} = -\frac{L}{m} \frac{du}{d\theta}$$

$$\ddot{r} = -\frac{L}{m} \frac{d^2 u}{d\theta^2} \frac{d\theta}{dt}$$

$$= -\frac{L}{m} \frac{d^2 u}{d\theta^2} \frac{L}{m} u^2$$

$$= -\frac{L^2}{m^2} u^2 \frac{d^2 u}{d\theta^2}$$

$$m\ddot{r} = F(r) + \frac{L^2}{mr^3}$$

$$-\frac{L^2}{m} u^2 \frac{d^2 u}{d\theta^2} = F(r) + \frac{L^2}{mr^3}$$

$$\frac{d^2 u}{d\theta^2} = -\frac{m}{L^2 u^2} F\left(\frac{1}{u}\right) - u$$

$$F\left(\frac{1}{u}\right) = -\frac{K}{\left(\frac{1}{u}\right)^2} + \frac{K'}{\left(\frac{1}{u}\right)^3}$$

$$= Ku^2 + K'u^3$$

$$\frac{d^2 u}{d\theta^2} = -\frac{m}{L^2 u^2} [Ku^2 + K'u^3] - u$$

$$= -\frac{mK}{L^2} - \frac{mK'u}{L^2} - u$$

$$\frac{d^2 u}{d\theta^2} + u\left(1 + \frac{mK'}{L^2}\right) = -\frac{mK}{L^2}$$

$$\frac{d^2 u}{d\theta^2} + u\left(\frac{L^2 + mK'}{L^2}\right) = -\frac{mK}{L^2}$$

Homogeneous solution

$$\frac{d^2 u}{d\theta^2} + u\left(\frac{L^2 + mK'}{L^2}\right) = 0 \quad u = e^{\gamma\theta}$$

$$\gamma^2 + \left(\frac{L^2 + mK'}{L^2}\right) = 0$$

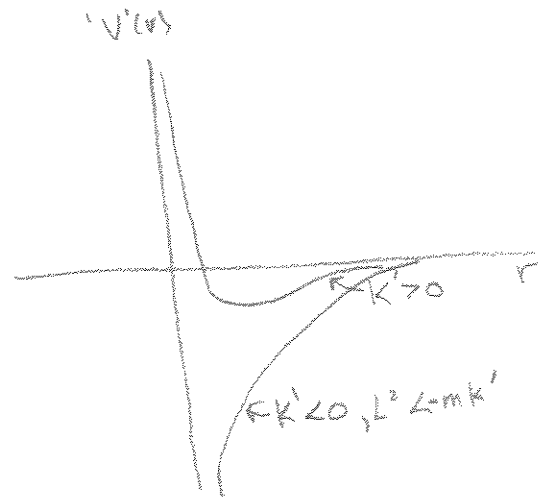
$$\gamma^2 = -\left(\frac{L^2 + mK'}{L^2}\right)$$

$$\gamma = \pm i \left(\frac{L^2 + mK'}{L^2}\right)^{1/2}$$

$$u_h = A \cos\left(\frac{(L^2 + mK')^{1/2}}{L} \theta - \theta_0\right)$$

$$u_p = -\frac{mK}{L^2}$$

$$u = \frac{1}{r} = -\frac{mK}{L^2} + A \cos\left(\frac{(L^2 + mK')^{1/2}}{L} \theta - \theta_0\right), \quad L^2 > -mK' \text{ for elliptical orbits}$$



$K' < 0$: hyperbolic or parabolic orbit

$K' > 0$: closed orbit: circular or elliptical about minimum $V(r)$ when $E < 0$. unbounded when $E \geq 0$

For $L^2 > mk'$, $\cos\left(\frac{(L^2 + mk')^{1/2}}{L} \theta - \theta_0\right)$ is real
Turning points are

$$\frac{1}{r_1} = -\frac{mk}{L^2} + A, \quad \frac{1}{r_2} = -\frac{mk}{L^2} - A$$

This is equivalent to 3.238 therefore,

$$A^2 = \frac{m^2 K^2}{L^4} + \frac{2mE}{L^2}, \quad E < 0$$

$$B = -\frac{mk}{L^2}, \quad K < 0$$

$$\frac{1}{r} = B + A \cos(\alpha \theta - \theta_0), \quad \alpha = \frac{(L^2 + mk')^{1/2}}{L}$$

$$\text{So, } r = \frac{a(1 - \epsilon^2)}{1 + \epsilon \cos \alpha \theta}, \quad \epsilon = \frac{A}{|B|}, \quad a = \left| \frac{B}{A^2 - B^2} \right| = \left| \frac{K}{2E} \right|$$

$$c) \quad \omega = \frac{2\pi}{\tau}$$

$$\tau = \frac{2\pi}{\omega}$$

$$\tau_{\text{nr.}} = \frac{2\pi}{\alpha} = 2\pi, \quad \alpha = 1$$

$$\tau = \frac{2\pi}{\alpha}$$

$$\tau_p = \tau - \tau_{\text{nr.}}$$

$$= \frac{2\pi}{\alpha} - 2\pi$$

$$= 2\pi\left(\frac{1}{\alpha} - 1\right)$$

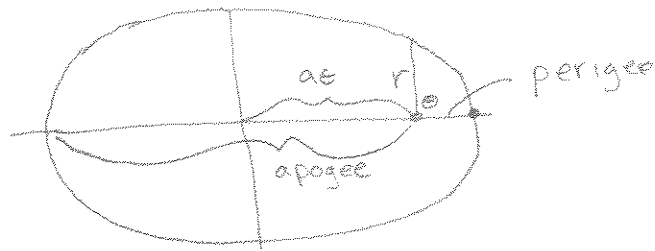
$$\tau_p = 2\pi(1 - \alpha)/\alpha, \quad \alpha = \frac{(L^2 + mk')^{1/2}}{L}$$

When $\alpha < 1$, $(1 - \alpha)/\alpha$ is positive and precession is in direction of $\hat{\theta}$. When $\alpha > 1$, $(1 - \alpha)/\alpha$ is negative and precesses in opposite direction.

3-53

$$d_1 = \text{Perigee} = 360 \text{ km} + R_e = 360 \text{ km} + 6378 \text{ km} = 6738 \text{ km}$$

$$d_2 = \text{Apogee} = 2,549 \text{ km} + \underset{\substack{\uparrow \\ \text{(equatorial)}}}{R_e} = 2549 \text{ km} + 6378 \text{ km} = 8927 \text{ km}$$



$$2a = \text{apogee} + \text{perigee}$$

$$= d_2 + d_1$$

$$a = \frac{d_2 + d_1}{2}$$

$$ae = a - d_1$$

$$e = \frac{a - d_1}{a} = 1 - \frac{d_1}{a} = 1 - \frac{d_1}{\frac{d_2 + d_1}{2}} = 1 - \frac{2d_1}{d_2 + d_1}$$

$$= \frac{d_2 + d_1 - 2d_1}{d_1 + d_2}$$

$$= \frac{d_2 - d_1}{d_2 + d_1}$$

At $\theta = 90^\circ$

$$r = \frac{a(1 - e^2)}{1 + e \cos 90^\circ}$$

$$= \frac{a(1 - e^2)}{1}$$

$$= \frac{d_2 + d_1}{2} \left(1 - \left(\frac{d_2 - d_1}{d_2 + d_1} \right)^2 \right)$$

$$= \frac{8927 + 6738}{2} \left(1 - \left(\frac{8927 - 6738}{8927 + 6738} \right)^2 \right) \text{ km}$$

$$= \frac{15665}{2} \left(1 - \left(\frac{2189}{15665} \right)^2 \right)$$

$$r = 7680 \text{ km}$$

$D = \text{Distance above earth's surface} = r - R_e$

$$= 7680 \text{ km} - 6378 \text{ km}$$

$$D = 1302 \text{ km}$$

3-55

$$V' = -\frac{\eta m M G R^2}{5r^3} (1 - 3\cos^2\theta)$$

$$V'(r, \frac{\pi}{2}) = -\frac{K_1}{r^3}, \quad K_1 = \frac{\eta m M G R^2}{5}$$

$$V'(r) = -\frac{K}{r} + \frac{L^2}{2mr^2} - \frac{K_1}{r^3}, \quad K = GMm$$

$$0 = \frac{dV'}{dr} = \frac{K}{r^2} - \frac{L^2}{mr^3} + \frac{3K_1}{r^4}$$

$$\frac{L^2}{mr^3} = \frac{K}{r^2} + \frac{3K_1}{r^4}$$

$$L^2 = mKr + \frac{3mK_1}{r}$$

$$L = (mKr + \frac{3mK_1}{r})^{1/2}$$

$$\dot{\theta} = \frac{L}{mr^2}$$

$$= \frac{(mKr + \frac{3mK_1}{r})^{1/2}}{mr^2}$$

$$\dot{\theta} = \left(\frac{K}{mr^3} + \frac{3K_1}{mr^5} \right)^{1/2}$$

$$\omega_r^2 = \frac{1}{m} \left(\frac{d^2 V'}{dr^2} \right)$$

$$= \frac{1}{m} \frac{d}{dr} \left(\frac{K}{r^2} - \frac{L^2}{mr^3} + \frac{3K_1}{r^4} \right)$$

$$= \frac{1}{m} \left(-\frac{2K}{r^3} + \frac{3L^2}{mr^4} - \frac{12K_1}{r^5} \right)$$

$$= -\frac{2K}{mr^3} - \frac{12K_1}{mr^5} + \frac{3}{m^2 r^4} \left(mKr + \frac{3mK_1}{r} \right)$$

$$= -\frac{2K}{mr^3} - \frac{12K_1}{mr^5} + \frac{3K}{mr^3} + \frac{9K_1}{mr^5}$$

$$= \frac{K}{mr^3} - \frac{3K_1}{mr^5}$$

$$\omega_r = \left(\frac{K}{mr^3} - \frac{3K_1}{mr^5} \right)^{1/2}$$

$$(x+y)^n = x^n + nx^{n-1}y + \dots$$

$$\dot{\theta} = \left(\frac{K}{mr^3} \right)^{1/2} + \frac{1}{2} \left(\frac{mr^3}{K} \right)^{1/2} \left(\frac{3K_1}{mr^5} \right)$$

$$\omega_r = \left(\frac{K}{mr^3} \right)^{1/2} - \frac{1}{2} \left(\frac{mr^3}{K} \right)^{1/2} \left(\frac{3K_1}{mr^5} \right)$$

$$\omega_p = \dot{\theta} - \omega_r$$

$$= \left(\frac{mr^3}{K} \right)^{1/2} \left(\frac{3K_1}{mr^5} \right)$$

$$= \left(\frac{r^3}{GM} \right)^{1/2} \left(\frac{3}{5} \frac{\eta G M R^2}{r^5} \right)$$

$$= \frac{3}{5} \eta \frac{R^2}{r^2} \left(\frac{GM r^3}{r^6} \right)^{1/2}$$

$$\boxed{\omega_p = \frac{3}{5} \eta \left(\frac{R}{r} \right)^2 \left(\frac{GM}{r^3} \right)^{1/2}}$$

3-57

$$V_{rel} = V(r) - \frac{[E - V(r)]^2}{2mc^2}$$

$$V(r) = \frac{K}{r}$$

$$E = \frac{1}{2} m \dot{r}^2 + \frac{L^2}{2mr^2} + V(r)$$

$$V'_{rel} = V(r) + \frac{L^2}{2mr^2}$$

$$V'_{rel} = V - \frac{[E - V]^2}{2mc^2} + \frac{L^2}{2mr^2}$$

$$\begin{aligned} \frac{dV'_{rel}}{dr} &= \frac{dV}{dr} - \frac{[E - V]}{mc^2} \left(\frac{dE}{dr} - \frac{dV}{dr} \right) - \frac{L^2}{mr^3} \\ &= \frac{dV}{dr} - \frac{[E - V]}{mc^2} \left(-\frac{dV}{dr} \right) - \frac{L^2}{mr^3}, E = \text{constant} \end{aligned}$$

$$= \frac{dV}{dr} \left(1 + \frac{[E - V]}{mc^2} \right) - \frac{L^2}{mr^3}$$

$$= \frac{-K}{r^2} \left(1 + \frac{L^2}{2mr^2c^2} \right) - \frac{L^2}{mr^3} \quad (\dot{r} = 0)$$

$$= \frac{-K}{r^2} - \left(\frac{K}{2mr^2c^2} + \frac{1}{mr^3} \right) L^2$$

$$L^2 \left(\frac{K}{2mr^2c^2} + \frac{1}{mr^3} \right) = -\frac{K}{r^2}$$

$$\frac{L^2}{mr^3} \left(\frac{K}{2mrc^2} + 1 \right) = -\frac{K}{r^2}$$

$$L^2 = Kmr \left(1 - \frac{K}{2mrc^2} \right)^{-1} \quad K < 0 \text{ (attractive force)}$$

$$L = -(Kmr)^{1/2} \left(1 - \frac{K}{2mrc^2} \right)^{-1/2}$$

$$\dot{\theta} = \frac{L}{mr^2}$$

$$= \left(\frac{K}{mr^3} \right)^{1/2} \left(1 - \frac{K}{2mrc^2} \right)^{-1/2} \quad (1-x)^{-1/2} \doteq 1 + \frac{1}{2}x$$

$$\dot{\theta} \doteq \left(\frac{K}{mr^3} \right)^{1/2} \left(1 + \frac{1}{2} \frac{K}{2mrc^2} \right)$$

$$\doteq \left(\frac{K}{mr^3} \right)^{1/2} + \left(\frac{K}{mr^3} \right)^{1/2} \left(\frac{K}{4mrc^2} \right)$$

$$\dot{\theta} \doteq \left(\frac{K}{mr^3} \right)^{1/2} + \frac{K^{3/2}}{4m^{3/2}r^{5/2}c^2}$$

$$\frac{d^2 V_{rel}}{dr^2} = \frac{d}{dr} \left(\frac{K}{r^2} + \frac{KL^2}{2mr^4c^2} - \frac{L^2}{mr^3} \right), K < 0$$

$$= \frac{-2K}{r^3} - \frac{2KL^2}{m^2 r^5 c^2} + \frac{3L^2}{mr^4}$$

$$\omega_r^2 = \frac{-2K}{mr^3} - \frac{2KL^2}{m^2 r^5 c^2} + \frac{3L^2}{mr^4}$$

$$= \frac{-2K}{mr^3} - \frac{2K}{m^3 r^5 c^2} \left(Kmr \left(1 - \frac{K}{2mrc^2} \right)^{-1} \right) + \frac{3}{m^3 r^4} \left(Kmr \left(1 - \frac{K}{2mrc^2} \right)^{-1} \right)$$

$$= \frac{-2K}{mr^3} - \frac{2K^2}{m^2 r^5 c^2} \left(1 - \frac{K}{2mrc^2} \right)^{-1} + \frac{3K}{mr^3} \left(1 - \frac{K}{2mrc^2} \right)^{-1}$$

$$= \frac{-2K}{mr^3} + \left[\frac{3K}{mr^3} - \frac{2K^2}{m^2 r^5 c^2} \right] \left(1 - \frac{K}{2mrc^2} \right)^{-1}$$

$$= \frac{-2K}{mr^3} \left(1 - \frac{K}{2mrc^2} \right) + \frac{3K}{mr^3} - \frac{2K^2}{m^2 r^5 c^2}$$

$$\frac{1 - \frac{K}{2mrc^2}}{1 - \frac{K}{2mrc^2}}$$

$$= \frac{K}{mr^3} + \frac{2K^2}{2m^2 r^5 c^2} - \frac{2K^2}{m^2 r^5 c^2}$$

$$\frac{1 - \frac{K}{2mrc^2}}{1 - \frac{K}{2mrc^2}}$$

$$= \left(\frac{K}{mr^3} - \frac{K^2}{m^2 r^5 c^2} \right) \left(1 - \frac{K}{2mrc^2} \right)^{-1}$$

$$\omega_r = \left(\frac{K}{mr^3} - \frac{K^2}{m^2 r^5 c^2} \right)^{1/2} \left(1 - \frac{K}{2mrc^2} \right)^{-1/2}$$

$$= \left(\frac{K}{mr^3} \left(1 - \frac{K}{mrc^2} \right) \right)^{1/2} \left(1 - \frac{K}{2mrc^2} \right)^{-1/2}$$

$$= \left(\frac{K}{mr^3} \right)^{1/2} \left(1 - \frac{K}{mrc^2} \right)^{1/2} \left(1 - \frac{K}{2mrc^2} \right)^{-1/2} \quad (1-x)^{-1/2} = 1 + \frac{1}{2}x$$

$$\approx \left(\frac{K}{mr^3} \right)^{1/2} \left(1 - \frac{K}{2mrc^2} \right) \left(1 + \frac{K}{4mrc^2} \right) \quad (1-x)^{1/2} = 1 - \frac{1}{2}x$$

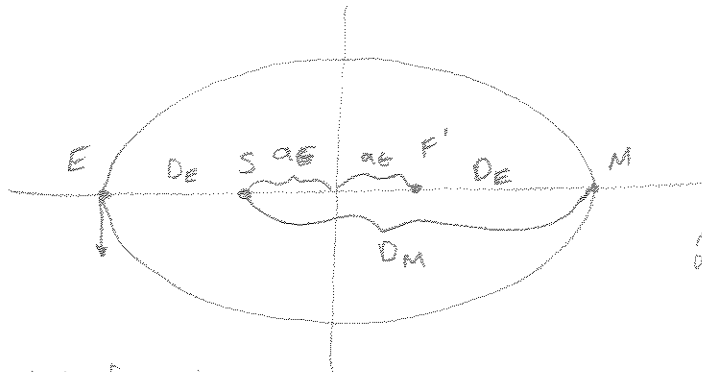
$$\approx \left(\frac{K}{mr^3} \right)^{1/2} \left(1 - \frac{K}{4mrc^2} - \frac{K^2}{8(mrc^2)^2} \right)$$

$$\approx \left(\frac{K}{mr^3} \right)^{1/2} \left(1 - \frac{K}{4mrc^2} \right)$$

$$\omega_r \approx \left(\frac{K}{mr^3} \right)^{1/2} - \frac{K^{3/2}}{4m^{3/2} r^5 c^2}$$

$$\omega_p = \dot{\theta} - \omega_r = \frac{1}{2} K^{1/2} m^{-3/2} r^{-5/2} c^{-2}$$

3-59



For circular orbit of earth,

$$\omega_E = \frac{2\pi}{1 \text{ year}} = 2.00 \times 10^{-7} \text{ s}^{-1}$$

$$L_s = m(\omega_E + \omega_s) D_E^2$$

$$\tau_s = \frac{2m}{L_s} \pi ab$$

$$= \frac{2m}{m(\omega_E + \omega_s) D_E^2} \pi ab$$

$$= \frac{2\pi}{(\omega_E + \omega_s) D_E^2} \left(\frac{D_m + D_E}{2} \right) (D_m D_E)^{1/2}$$

$$= \frac{\pi (D_m + D_E)}{(\omega_E + \omega_s) D_E^2} (D_m D_E)^{1/2}$$

$$\tau_s^2 = \frac{4\pi^2}{MG} a^3 \text{ (Kepler's Law)}$$

$$\tau_s = \frac{2\pi}{(MG)^{1/2}} a^{3/2} = 1.37 \text{ years}$$

$$\frac{2\pi}{(MG)^{1/2}} \left(\frac{D_m + D_E}{2} \right)^{3/2} = \frac{\pi (D_m + D_E)}{(\omega_E + \omega_s) D_E^2} (D_m D_E)^{1/2}$$

$$\omega_E + \omega_s = 2.188 \times 10^{-7} / \text{s}$$

$$\omega_s = 0.188 \times 10^{-7} / \text{s}$$

$$V_s = \omega_s D_E$$

$$V_s = 2.8 \text{ km/s}$$

$$2a = D_m + D_E$$

$$a = \frac{D_m + D_E}{2}$$

$$2ae = D_m - D_E$$

$$ae = \frac{D_m - D_E}{2}$$

$$e = \frac{D_m - D_E}{2a}$$

$$e = \frac{D_m - D_E}{D_m + D_E}$$

$$b = a(1 - e^2)^{1/2}$$

$$= \frac{D_m + D_E}{2} \left(1 - \left(\frac{D_m - D_E}{D_m + D_E} \right)^2 \right)^{1/2}$$

$$= \frac{D_m + D_E}{2} \left(\frac{(D_m + D_E)^2 - (D_m - D_E)^2}{(D_m + D_E)^2} \right)^{1/2}$$

$$b = \frac{D_m + D_E}{2} \left(\frac{D_m^2 + 2D_m D_E + D_E^2 - (D_m^2 - 2D_m D_E + D_E^2)}{(D_m + D_E)^2} \right)^{1/2}$$

$$= \frac{D_m + D_E}{2} \left(\frac{4D_m D_E}{(D_m + D_E)^2} \right)^{1/2}$$

$$b = \sqrt{D_m D_E}$$

$$G = 6.67 \times 10^{-11} \text{ m}^3 \text{ kg}^{-1} \text{ s}^{-2}$$

$$M = 1.99 \times 10^{30} \text{ kg}$$

$$D_E = 1.49 \times 10^{11} \text{ m}$$

$$D_M = 2.2 \times 10^{11} \text{ m}$$

To escape from sun's gravitational pull, orbit must be a parabola.

$$\frac{1}{r} = B + A \cos \theta$$

$B = A$ for parabola

$$B = \frac{1}{a}, A = \frac{1}{a}$$

For inverse square law force

$$B = \frac{-mk}{L^2} \quad (3.259)$$

$$\frac{1}{a} = \frac{-mk}{L^2}$$

$$= \frac{-mk}{(m D_E^2 \omega)^2}$$

$$K = -GMm$$

$$= \frac{GMm^2}{m^2 \omega^2 D_E^4}$$

$$\omega^2 = \frac{GMa}{D_E^4}$$

$$\omega = \frac{(GMa)^{1/2}}{D_E^2}$$

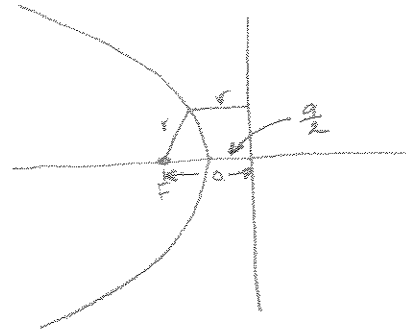
$$\omega = 2.833 \times 10^{-7} \text{ s}^{-1}$$

$$\omega_e + \omega_s = 2.833 \times 10^{-7} \text{ s}^{-1}$$

$$\omega_s = 0.833 \times 10^{-7} \text{ s}^{-1}$$

$$V_{esc} = \omega_s D_E$$

$$V_{esc} = 12.3 \text{ km/s}$$



$$\frac{a}{2} = D_E \rightarrow a = 2D_E \text{ for parabola}$$

$$G = 6.67 \times 10^{-11} \text{ m}^3 \text{ kg}^{-1} \text{ s}^{-2}$$

$$M = 1.99 \times 10^{30} \text{ kg}$$

$$D_E = 1.49 \times 10^{11} \text{ m}$$

$$\omega_e = 2.00 \times 10^{-7} \text{ s}^{-1}$$

3-61 The probe velocity v_1 is relative to Planet 1 velocity.

The relative velocity at a distance r_2 is found from the relation

$$L_1 = m r_2 v_{12} \quad (\text{conservation of angular momentum})$$

$$m r_1 v_1 = m r_2 v_{12}$$

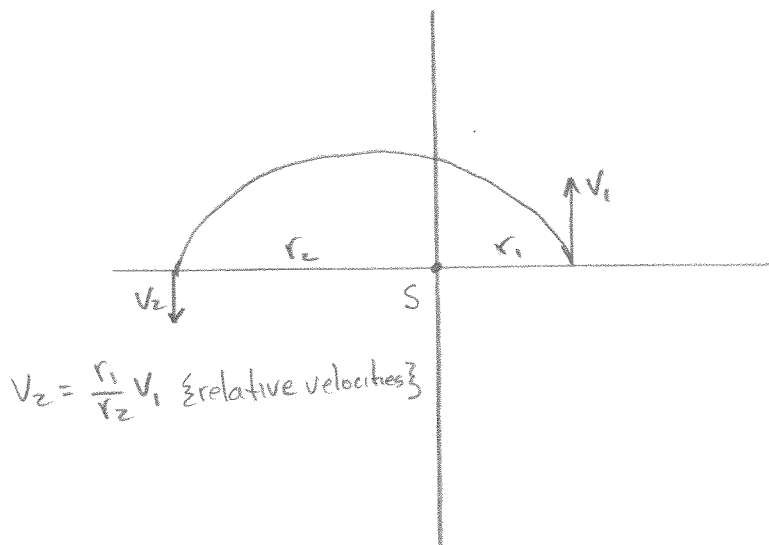
$$v_{12} = \frac{r_1}{r_2} v_1$$

where v_{12} is the component of v_2 perpendicular to the radius vector $\vec{r}$.

It's evident v_2 should be a minimum at r_2 . This occurs when

$v_2 = v_{12}$ (no radial component). This only occurs for an ellipse

with an aphelion at r_2 . $\{ \text{Assume no gravitational effects other than Sun-probe.} \}$



Therefore, the semimajor axis is

$$a = \frac{r_1 + r_2}{2}$$

Period of Planet 1

$$F_{\text{cent}} = F_g$$

$$\frac{m r_1^2 \omega_1^2}{r_1} = \frac{G m M}{r_1^2}$$

$$\omega_1^2 = \frac{G M}{r_1^3}$$

$$\omega_1 = \sqrt{\frac{G M}{r_1^3}}$$

$$T_1 = \frac{2\pi}{\omega_1}$$

$$T_1 = \frac{2\pi r_1^{3/2}}{\sqrt{GM}} \rightarrow T_2 = \frac{2\pi r_2^{3/2}}{\sqrt{GM}}$$

Planet velocities:

$$V_{P1} = \frac{2\pi r_1}{T_1}$$

$$= \frac{2\pi r_1}{\frac{2\pi r_1^{3/2}}{\sqrt{GM}}}$$

$$= \sqrt{GM} r_1^{-1/2}$$

$$V_{P1} = \sqrt{\frac{GM}{r_1}}$$

$$V_{P2} = \frac{2\pi r_2}{T_2}$$

$$= \sqrt{GM} r_2^{-1/2}$$

$$= V_{P1} r_1^{1/2} r_2^{-1/2}$$

$$V_{P2} = V_{P1} \left(\frac{r_1}{r_2} \right)^{1/2}$$

$$\left\{ \sqrt{GM} = V_{P1} r_1^{1/2} \right\}$$

Now,

$$a = \left| \frac{K}{2E} \right|$$

$$a = \frac{r_1 + r_2}{2}$$

$$E = \frac{K}{r_1} + \frac{1}{2} m v^2, \quad V = V_{P1} + V_{P2}$$

$$2E = \frac{K}{a}$$

$$\frac{2K}{r_1} + m v^2 = \frac{K}{a}$$

$$m v^2 = \frac{K}{a} - \frac{2K}{r_1}$$

$$= \frac{K r_1 - 2K a}{r_1 a}$$

$$= \frac{K (r_1 - 2a)}{r_1 a}$$

$$v^2 = \frac{K}{m r_1} \left(\frac{r_1 - 2a}{a} \right)$$

$$= -\frac{G m M}{r_1} \left(\frac{r_1 - 2a}{a} \right)$$

$$= \frac{GM}{r_1} \left(\frac{2a - r_1}{a} \right)$$

$$= \frac{GM}{r_1} \left(\frac{2(r_2 + r_1) - r_1}{\frac{r_1 + r_2}{2}} \right)$$

$$= V_{P_1}^2 \left(\frac{r_2 + r_1 - r_1}{\frac{r_1 + r_2}{2}} \right)$$

$$= V_{P_1}^2 \left(\frac{2r_2}{r_1 + r_2} \right)$$

$$V = V_{P_1} \left(\frac{2r_2}{r_1 + r_2} \right)^{1/2}$$

$$V_1 + V_{P_1} = V_{P_1} \left(\frac{2r_2}{r_1 + r_2} \right)^{1/2}$$

$$V_1 = V_{P_1} \left[\left(\frac{2r_2}{r_1 + r_2} \right)^{1/2} - 1 \right]$$

$$V_1 = \frac{2\pi r_1}{T_1} \left[\left(\frac{2r_2}{r_1 + r_2} \right)^{1/2} - 1 \right]$$

$$E = \frac{K}{r_2} + \frac{1}{2} MV^2, \quad V = V_{P_2} + V_2$$

$$V^2 = \frac{GM}{r_2} \left(\frac{2a - r_2}{a} \right) \quad \left\{ \text{using method for } V_1 \right\}$$

$$= \frac{GM}{r_2} \left(\frac{r_2 + r_1 - r_2}{\frac{r_1 + r_2}{2}} \right)$$

$$= V_{P_2}^2 \frac{2r_1}{r_1 + r_2}$$

$$V = V_{P_2} \left(\frac{2r_1}{r_1 + r_2} \right)^{1/2}$$

$$V_2 + V_{P_2} = V_{P_2} \left(\frac{2r_1}{r_1 + r_2} \right)^{1/2}$$

$$V_2 = V_{P_2} \left[\left(\frac{2r_1}{r_1 + r_2} \right)^{1/2} - 1 \right]$$

$$V_2 = \frac{2\pi r_1}{T_1} \left(\frac{r_1}{r_2} \right)^{1/2} \left[\left(\frac{2r_1}{r_1 + r_2} \right)^{1/2} - 1 \right]$$

Sun-Earth distance = 9.3×10^7 mi.

Sun-Venus distance = 6.7×10^7 mi.

Sun-Mars distance = 1.4×10^8 mi.

Earth period = 8760 hrs.

Earth-Venus trip:

$$V_1 = \frac{2\pi r_1}{T_1} \left[\left(\frac{2r_2}{r_1 + r_2} \right)^{1/2} - 1 \right]$$

$$= \frac{2\pi(9.3 \times 10^7)}{8760} \left[\left(\frac{2(6.7 \times 10^7)}{6.7 \times 10^7 + 9.3 \times 10^7} \right)^{1/2} - 1 \right]$$

$$V_1 = -7.5 \times 10^3 \frac{\text{mi}}{\text{hr}}$$

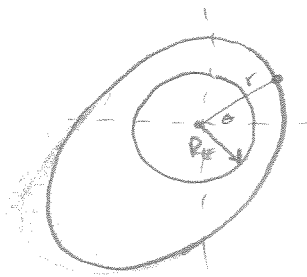
Earth-Mars trip:

$$V_1 = \frac{2\pi r_1}{T_1} \left[\left(\frac{2r_2}{r_1 + r_2} \right)^{1/2} - 1 \right]$$

$$= \frac{2\pi(9.3 \times 10^7)}{8760} \left[\left(\frac{2(1.4 \times 10^8)}{1.4 \times 10^8 + 9.3 \times 10^7} \right)^{1/2} - 1 \right]$$

$$V_1 = 6.4 \times 10^3 \frac{\text{mi}}{\text{hr}}$$

3-63



$$\dot{\theta} = \frac{L}{mr^2}$$

i) The perigee has r as a minimum. So, the perigee as a function of θ is located where $\dot{\theta} = \text{maximum}$.

ii) Kepler's Law states

$$T^2 = \frac{4\pi^2}{MG} a^3$$

where $M = M_e$. MG is to be expressed in terms of g and R_e .

$$F = \frac{GmM}{r^2}$$

$$mg = \frac{GmM}{R_e^2}$$

$$g = \frac{GM}{R_e^2}$$

$$GM = R_e^2 g$$

So,

$$T^2 = \frac{4\pi^2}{gR_e^2} a^3$$

$$a^3 = \frac{T^2 g R_e^2}{4\pi^2}$$

$$a = \left(\frac{T^2 g R_e^2}{4\pi^2} \right)^{1/3}$$

iii) The eccentricity is related to r by

$$r_{1,2} = a(1 \pm e)$$

$$r_1 = r_{\max}, r_2 = r_{\min}$$

$$r_{\max} = a(1+e), r_{\min} = a(1-e)$$

$$\frac{r_{\max}}{r_{\min}} = \frac{1+e}{1-e}$$

$$\text{Let } \alpha = \frac{r_{\max}}{r_{\min}}$$

$$\alpha = \frac{1+e}{1-e}$$

$$\alpha - \alpha e = 1 + e$$

$$\alpha - 1 = e + \alpha e$$

$$\alpha - 1 = e(1 + \alpha)$$

$$\frac{\alpha - 1}{\alpha + 1} = e$$

$$L = m r^2 \dot{\theta}$$

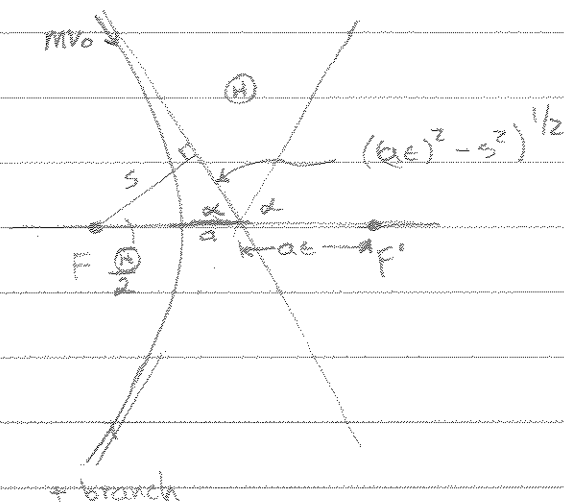
$$r_{\max}^2 \dot{\theta}_{\min} = r_{\min}^2 \dot{\theta}_{\max}$$

$$\frac{r_{\max}^2}{r_{\min}^2} = \frac{\dot{\theta}_{\max}}{\dot{\theta}_{\min}}$$

$$\frac{r_{\max}}{r_{\min}} = \left(\frac{\dot{\theta}_{\max}}{\dot{\theta}_{\min}} \right)^{1/2}$$

$$e = \frac{\alpha - 1}{\alpha + 1}, \alpha = \left(\frac{\dot{\theta}_{\max}}{\dot{\theta}_{\min}} \right)^{1/2}$$

3-65



$$r = \frac{a(e^2 - 1)}{1 + e \cos \theta}, \quad \cos \alpha = -\frac{1}{e}$$

$$r_1 = a(e-1)$$

$$v_1 = a(e-1)$$

$$v_2 = \frac{K}{2E} + \left(\left(\frac{K}{2E} \right)^2 + \frac{L^2}{2mE} \right)^{1/2}, \quad E > 0, K < 0$$

$$= -a + \left(a^2 + \frac{m^2 v_0^2 s^2}{m^2 v_0^2} \right)^{1/2} \quad E = \frac{1}{2} m v_0^2$$

$$= -a + (a^2 + s^2)^{1/2} \quad L = mv_0 s$$

$$a(\epsilon-1) = -a + (a^2 + s^2)^{1/2}$$

$$a + a(e-1) = (a^2 + s^2)^{1/2}$$

$$a(1+\epsilon-1) = (a^2+s^2)^{1/2}$$

$$a_t = (a_t + z^t)^{1/2}$$

$$c = \left(1 + \frac{z^2}{a^2}\right)^{1/2}$$

$$\tan \frac{(A)}{2} = \cot \alpha = \frac{(\kappa E)^2 - S^2}{S}^{1/2} = \frac{a}{S} = \frac{|K|}{\kappa E} \frac{1}{S} = \frac{|K|}{m b^2 S}$$

$$K = \frac{1}{1000} = 0.001$$

$$|K| = 1 - g_1 g_2 = 1 - g_1 g_2$$

$$\tan \frac{\theta}{2} = \frac{g \cos \theta}{m v_0^2} \quad \therefore S = \frac{g \cos \theta}{m v_0^2} \cot \frac{\theta}{2}$$

$$\frac{1}{2} \sec^2 \left(\frac{\pi}{4} \right) d\left(\frac{\pi}{4} \right) = \frac{-8.82}{\text{m/s}^2} ds = ds$$

$$d\sigma = 2\pi s ds$$

$$= 2\pi \left[\frac{q_1 q_2}{mv_0^2} \cot \frac{\Theta}{2} \right] \left[\frac{1}{2} \sec^2 \frac{\Theta}{2} \frac{mv_0^2}{q_1 q_2} \left(\frac{q_1 q_2}{mv_0^2} \cot \frac{\Theta}{2} \right)^2 \right]$$

$$= \pi \left[\cot \frac{\Theta}{2} \sec^2 \frac{\Theta}{2} \left(\frac{q_1 q_2}{mv_0^2} \right)^2 \cot^2 \frac{\Theta}{2} \right]$$

$$= \pi \left[\frac{\cos^3 \frac{\Theta}{2}}{\sin^3 \frac{\Theta}{2}} \frac{1}{\cos^2 \frac{\Theta}{2}} \right] \left(\frac{q_1 q_2}{mv_0^2} \right)^2$$

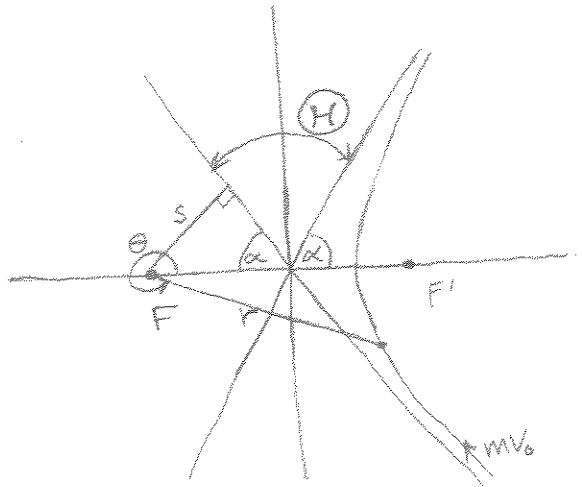
$$= \pi \left(\frac{q_1 q_2}{mv_0^2} \right)^2 \frac{\cos \frac{\Theta}{2}}{\sin^3 \frac{\Theta}{2}} \cdot \frac{\sin \frac{\Theta}{2}}{\sin \frac{\Theta}{2}}$$

$$= \pi \left(\frac{q_1 q_2}{mv_0^2} \right)^2 \frac{\frac{1}{2} \sin \Theta}{\sin^4 \frac{\Theta}{2}}$$

$$d\sigma = \left(\frac{q_1 q_2}{2mv_0^2} \right)^2 \frac{2\pi \sin \Theta}{\sin^4 \frac{\Theta}{2}}, \quad K < 0$$

$$\boxed{d\sigma_{K<0} = d\sigma_{K>0}}$$

3-67



$$L = mv_0 s \quad E = \frac{1}{2}mv_0^2$$

$$V'(r) = V(r) + \frac{L^2}{2mr^2} = \text{const}$$

$$= V(r) + \frac{m^2 v_0^2 r^2}{2m r^2}, \quad r = \frac{1}{u}$$

$$V\left(\frac{1}{a}\right) = V\left(\frac{1}{b}\right) + \frac{m^2 V_0^2 \frac{1}{a^2}}{2m\left(\frac{1}{a}\right)^2} \quad u = \frac{1}{r}$$

$$V\left(\frac{1}{a}\right) = V\left(\frac{1}{a}\right) + \frac{1}{2} m v_0^2 \sin^2 \alpha$$

$$\textcircled{H} = \pi - 2\alpha$$

$$r = \sqrt{\frac{2}{m} (E - V(r))}^{1/2}$$

$$= \sqrt{\frac{2}{m} \left(\frac{1}{2} m v_0^2 - \frac{1}{2} m v_0^2 \sin^2 \theta - V\left(\frac{1}{\sin \theta}\right) \right)^{1/2}}$$

$$V_0 \left(1 - \frac{S^2 u^2}{\frac{1}{2} m v_0^2} - V \left(\frac{1}{u} \right) \right)^{1/2}$$



$$x = \frac{a}{b} \rightarrow \frac{a}{b} = \frac{a}{b}$$

$$m \frac{dv}{dt} = m \frac{d}{dt} \left(\frac{dx}{dt} \right)$$

1000 - Vos du do

$$\frac{1}{\sqrt{5}} \frac{d}{dt} \frac{1}{\sqrt{5}}$$

$$\frac{d}{dx} \frac{1}{v_0} = \frac{1}{v_0} \left(1 - \frac{v^2}{c^2} - \frac{v \left(\frac{dv}{dx} \right)}{\frac{1}{2} m v^2} \right)^{-1/2}$$

$$-d\theta = \frac{1}{\mu_0} \left(1 - \frac{V(u-1)}{\frac{1}{2} \mu_0 V_0^2} \right)^{-1/2} du$$

$$E = \int \left(1 - \beta^2 \right)^{-\frac{1}{2}} \frac{1}{2} m v^2 dx$$

But $\Theta = 2\alpha$ when r begins at ∞ and ends at r_0 to establish 2α .

$$\textcircled{H} = \left| \pi - 2s \int_0^{u_0} \left(1 - s^2 u^2 - V(u) \right)^{-1/2} du \right| \quad \{ \textcircled{H} \text{ must be positive} \}$$

$$d_0 = \text{first positive root of denominator of integrand.}$$

3-69

$$F = \frac{K}{r^2}, \quad K > 0$$

$$V = - \int_{\infty}^r \frac{K}{r^2} dr$$

$$= \frac{K}{r}$$

$$\textcircled{H} = \left| \pi - 2s \int_0^{u_0} \left[1 - s^2 u^2 - V(u^{-1}) / \frac{1}{2} m v_0^2 \right]^{\frac{-1}{2}} du \right|$$

$$= \left| \pi - 2s \int_0^{u_0} \left[1 - s^2 u^2 - Ku / \frac{1}{2} m v_0^2 \right]^{\frac{-1}{2}} du \right|$$

Completing the square:

$$-s^2 u^2 - Ku / \frac{1}{2} m v_0^2 + 1 = -s^2 \left(u^2 + \frac{2Ku}{m v_0^2 s^2} \right) + 1$$

$$= -s^2 \left(u^2 + \frac{2Ku}{m v_0^2 s^2} + \left(\frac{K}{m v_0^2 s^2} \right)^2 \right) + 1 + \left(\frac{Ks}{m v_0^2 s^2} \right)^2$$

$$= -s^2 \left(u + \frac{K}{m v_0^2 s^2} \right)^2 + \frac{(m v_0^2 s^2)^2 + (Ks)^2}{(m v_0^2 s^2)^2}$$

$$= -s^2 (x)^2 + B$$

$$= B - s^2 x^2$$

$$-s^2 \left(u_0 + \frac{K}{m v_0^2 s^2} \right)^2 + B = 0$$

$$u_0 + \frac{K}{m v_0^2 s^2} = \pm \left(\frac{B}{s^2} \right)^{1/2}$$

$$u_0 = \frac{-K}{m v_0^2 s^2} + \frac{B^{1/2}}{s}$$

$$\textcircled{H} = \left| \pi - 2s \int_{x_1}^{x_2} \left[B - s^2 x^2 \right]^{\frac{-1}{2}} dx \right| \left\{ x = u + \frac{K}{m v_0^2 s^2} \right\}$$

$$= \left| \pi - 2s \frac{B^{1/2}}{s} \int_{\theta_1}^{\theta_2} \frac{\cos \theta d\theta}{[B - B \sin^2 \theta]^{1/2}} \right|$$

$$= \left| \pi - 2 \int_{\theta_1}^{\theta_2} d\theta \right|$$

$$= \left| \pi - 2\theta \right|_{\theta_1}^{\theta_2}$$

$$= \left| \pi - 2 \sin^{-1} \left(x \frac{s}{B^{1/2}} \right) \right|_{x_1}^{x_2}$$

$$\text{let } B \sin^2 \theta = s^2 x^2$$

$$s x = B^{1/2} \sin \theta$$

$$x = \frac{B^{1/2}}{s} \sin \theta$$

$$dx = \frac{B^{1/2}}{s} \cos \theta d\theta$$

$$= \left| \pi - 2 \sin^{-1} \left(\left[u + \frac{K}{m v_0^2 s^2} \right] \frac{s}{B^{1/2}} \right) \right|_{u_0}^{u_1}$$

$$= \left| \pi - 2 \left[\sin^{-1} \left(\frac{B^{1/2}}{s} \cdot \frac{s}{B^{1/2}} \right) - \sin^{-1} \left(\frac{Ks}{m v_0^2 s^2 B^{1/2}} \right) \right] \right|$$

$$= \left| \pi - 2 \left(\frac{\pi}{2} - \sin^{-1} \left(\frac{Ks}{m v_0^2 s^2 B^{1/2}} \right) \right) \right|$$

$$= 2 \sin^{-1} \left(\frac{Ks}{m v_0^2 s^2 B^{1/2}} \right)$$

$$\sin \left(\frac{\theta}{2} \right) = \frac{Ks}{m v_0^2 s^2 B^{1/2}} \quad B = \frac{(m v_0^2 s^2)^2 + (Ks)^2}{(m v_0^2 s^2)^2}$$

$$= \frac{Ks m v_0^2 s^2}{m v_0^2 s^2 \left((m v_0^2 s^2)^2 + (Ks)^2 \right)^{1/2}}$$

$$= \frac{Ks}{\left[(m v_0^2 s^2)^2 + (Ks)^2 \right]^{1/2}}$$

$$= \frac{K}{\left[(m v_0^2 s)^2 + K^2 \right]^{1/2}}$$

$$\sin^2 \left(\frac{\theta}{2} \right) = \frac{K^2}{(m v_0^2 s)^2 + K^2}$$

$$\frac{1}{\sin^2 \left(\frac{\theta}{2} \right)} = \frac{(m v_0^2 s)^2 + K^2}{K^2}$$

$$\frac{K^2}{\sin^2 \left(\frac{\theta}{2} \right)} - K^2 = (m v_0^2 s)^2$$

$$\frac{(K^2 \csc^2 \left(\frac{\theta}{2} \right) - K^2)^{1/2}}{m v_0^2} = s$$

$$ds = \frac{1}{2 m v_0^2} (K^2 \csc^2 \left(\frac{\theta}{2} \right) - K^2)^{-1/2} d(K^2 \csc^2 \left(\frac{\theta}{2} \right)) \frac{d(\sin \left(\frac{\theta}{2} \right))^{-2}}{2} = -2 (\sin \left(\frac{\theta}{2} \right))^{-3} \cos \left(\frac{\theta}{2} \right) \frac{d\left(\frac{\theta}{2} \right)}{2} = -\frac{\cos \left(\frac{\theta}{2} \right) d\left(\frac{\theta}{2} \right)}{\sin^3 \left(\frac{\theta}{2} \right)}$$

$$ds = \frac{1}{2mv_0^2} (K^2 \csc^2 \frac{\theta}{2} - K)^{-1/2} \left(-\frac{\cos(\frac{\theta}{2})}{\sin^3 \frac{\theta}{2}} \right) d\theta$$

$$= -\frac{K^2 \cos \frac{\theta}{2}}{2mv_0^2 (K^2 \csc^2 \frac{\theta}{2} - K)^{1/2} \sin^3 \frac{\theta}{2}} d\theta$$

$$d\sigma = 2\pi s ds$$

$$= 2\pi \left[\frac{(K^2 \csc^2 \frac{\theta}{2} - K)^{1/2}}{mv_0^2} \right] \left[\frac{K^2 \cos \frac{\theta}{2}}{2mv_0^2 (K^2 \csc^2 \frac{\theta}{2} - K)^{1/2} \sin^3 \frac{\theta}{2}} \right] d\theta$$

$$= 2\pi \frac{K^2 \cos \frac{\theta}{2}}{2(mv_0^2)^2 \sin^3 \frac{\theta}{2}} d\theta$$

$$= \frac{2\pi K^2 \cos \frac{\theta}{2} \sin \frac{\theta}{2}}{(mv_0^2)^2 \sin^3 \frac{\theta}{2} \sin \frac{\theta}{2}} d\theta$$

$$= \frac{2\pi K^2}{2(mv_0^2)^2} \frac{\frac{1}{2} \sin \theta}{\sin^4 \frac{\theta}{2}} d\theta$$

$$\boxed{d\sigma = \left(\frac{K}{2mv_0^2} \right)^2 \frac{2\pi \sin \theta}{\sin^4 \frac{\theta}{2}} d\theta}$$

$$\frac{1}{\sin^4 \frac{\theta}{2}}$$

3-71

$$F(r) = \frac{K}{r^3}, K > 0$$

$$\frac{d^2u}{d\theta^2} = -u - \frac{m}{L^2 u^2} F\left(\frac{1}{u}\right)$$

$$= -u - \frac{m}{L^2 u^2} K u^3$$

$$= -u - \frac{mK}{L^2} u$$

$$\frac{d^2u}{d\theta^2} + u\left(1 + \frac{mK}{L^2}\right) = 0, \quad u = e^{\gamma\theta}$$

$$\gamma^2 + 1 + \frac{mK}{L^2} = 0$$

$$\gamma^2 = -\left(1 + \frac{mK}{L^2}\right)$$

$$\gamma = \pm i \left(1 + \frac{mK}{L^2}\right)^{1/2}$$

$$u = A \cos \left[\left(1 + \frac{mK}{L^2}\right)^{1/2} (\theta - \theta_0) \right]$$

$$V(r) = \frac{K}{2r^2} + \frac{L^2}{2mr^2} = E$$

$$\frac{1}{r^2} \left(\frac{L^2 + Km}{2m} \right) = E$$

$$\frac{1}{r^2} = \frac{2mE}{L^2 + Km} \quad \{ \text{turning point} \}$$

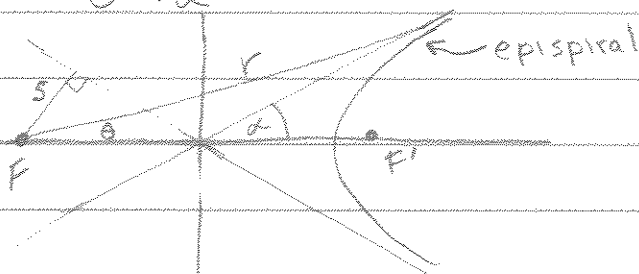
$$\boxed{\frac{1}{r} = \left(\frac{2mE}{L^2 + Km} \right)^{1/2} \cos \left[\left(1 + \frac{mK}{L^2}\right)^{1/2} (\theta - \theta_0) \right]}$$

Since $\left(1 + \frac{mK}{L^2}\right)^{1/2} > 1$, $\theta - \theta_0$ range must

be small so that $\frac{1}{r} > 0$. In particular,

$$0 \leq \left(1 + \frac{mK}{L^2}\right)^{1/2} (\theta - \theta_0) \leq \frac{\pi}{2} \quad \text{and} \quad \frac{3\pi}{2} \leq \left(1 + \frac{mK}{L^2}\right)^{1/2} (\theta - \theta_0) \leq 2\pi$$

As $r \rightarrow \infty$ $\theta \rightarrow \alpha$



When $r \rightarrow \infty$, $(1 + \frac{mk}{L^2})^{1/2} (\Theta) \rightarrow \frac{\pi}{2}$ $\{ \Theta_0 = 0 \}$

$$\Theta = \frac{\pi}{2} (1 + \frac{mk}{L^2})^{-1/2}$$

But $\Theta \rightarrow \alpha$ as $r \rightarrow \infty$

$$\alpha = \frac{\pi}{2} (1 + \frac{mk}{L^2})^{-1/2}$$

$$\Theta = \pi - 2\alpha$$

$$= \pi - \pi (1 + \frac{mk}{L^2})^{-1/2}$$

$$L = mv_0 s$$

$$= \pi - \pi \left(\frac{L^2}{L^2 + mk} \right)^{1/2}$$

$$= \pi - \pi \frac{mv_0 s}{(m^2 v_0^2 s^2 + mk)^{1/2}} = \pi - \pi \frac{s}{(s^2 + \frac{k}{mv_0^2})^{1/2}}$$

The parameter s can also be expressed in terms of the scattering angle, Θ , by using the expression $\{ \text{This is an alternative approach} \}$

$$\Theta = \pi - 2s \int_0^{u_0} \left[1 - s^2 u^2 - V(u) / \frac{1}{2} m v_0^2 \right]^{-1/2} du$$

where u_0 is the first positive root of denominator of the integrand.

$$V(r) = - \int_{\infty}^r F(r) dr, \quad F(r) = \frac{k}{r^2}$$

$$= \frac{k}{2r^2}$$

$$V(u) = \frac{k}{2} u^2$$

$$1 - s^2 u_0^2 - \frac{k}{2} u_0^2 / \frac{1}{2} m v_0^2 = 0$$

$$u_0^2 (s^2 + \frac{k}{m v_0^2}) = 1$$

$$u_0 = (s^2 + \frac{k}{m v_0^2})^{-1/2}$$

$$\textcircled{A} = \left| \pi - 2s \int_0^{u_0} \left[1 - u^2 \left(s^2 + \frac{k}{mv_0^2} \right) \right]^{-1/2} du \right|$$

$$\text{let } u^2 \left(s^2 + \frac{k}{mv_0^2} \right) = \sin^2 \theta$$

$$u = \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \sin \theta$$

$$du = \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \cos \theta d\theta$$

$$= \left| \pi - 2s \int_{\theta=0}^{\theta=\theta_0} \frac{\left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \cos \theta d\theta}{\left[1 - \sin^2 \theta \right]^{1/2}} \right|$$

$$= \left| \pi - 2s \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \int_0^{\theta_0} d\theta \right|$$

$$= \left| \pi - 2s \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \sin^{-1} \left(u \left(s^2 + \frac{k}{mv_0^2} \right)^{1/2} \right) \right|_{u_0 = \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2}}$$

$$= \left| \pi - 2s \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \sin^{-1}(1) \right|$$

$$= \left| \pi - 2s \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \frac{\pi}{2} \right|$$

$$= \left| \pi - \pi s \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2} \right| \quad \{ \text{agrees with first approach} \}$$

$$\textcircled{A} - \pi = -\pi s \left(s^2 + \frac{k}{mv_0^2} \right)^{-1/2}$$

$$\frac{\pi - \textcircled{A}}{\pi} = \frac{s}{\left(s^2 + \frac{k}{mv_0^2} \right)^{1/2}}$$

$$\frac{(\pi - \textcircled{A})^2}{\pi^2} = \frac{s^2}{s^2 + \frac{k}{mv_0^2}}$$

$$\frac{(\pi - \textcircled{A})^2}{\pi^2} = \frac{1}{1 + \frac{k}{mv_0^2 s^2}}$$

$$\frac{\pi^2}{(\pi - \textcircled{A})^2} = 1 + \frac{k}{mv_0^2 s^2}$$

$$\frac{\pi^2}{(\pi - \theta)^2} - 1 = \frac{K}{m v_0^2 s^2}$$

$$\frac{\pi^2 - (\pi - \theta)^2}{(\pi - \theta)^2} = \frac{K}{m v_0^2 s^2}$$

$$s^2 = \frac{K}{m v_0^2} \frac{(\pi - \theta)^2}{\pi^2 - (\pi - \theta)^2}$$

$$= \frac{K}{m v_0^2} \frac{(\pi - \theta)^2}{\pi^2 - [\pi^2 - 2\pi\theta + \theta^2]}$$

$$= \frac{K}{m v_0^2} \frac{(\pi - \theta)^2}{\theta(2\pi - \theta)}$$

$$s = \left(\frac{K}{m v_0^2} \frac{(\pi - \theta)^2}{\theta(2\pi - \theta)} \right)^{1/2}$$

Now,

$$\theta = \pi - \pi \left(1 + \frac{mk}{L^2} \right)^{-1/2} \quad \text{where } L = m v_0 s$$

$$d\theta = \frac{\pi}{2} \left(1 + \frac{mk}{L^2} \right)^{-3/2} \left(\frac{-2mk}{L^3} \right) dL \quad dL = m v_0 ds$$

$$= -\frac{\pi mk}{L^3} \left(\frac{L^2 + mk}{L^2} \right)^{-3/2} m v_0 ds$$

$$= -\frac{\pi mk}{L^5} \left(\frac{L^2}{L^2 + mk} \right)^{3/2} m v_0 ds$$

$$= -\frac{\pi mk}{L^3} \frac{L^3}{(L^2 + mk)^{3/2}} m v_0 ds$$

$$= -\frac{\pi mk}{(L^2 + mk)^{3/2}} m v_0 ds$$

$$ds = \frac{(L^2 + mk)^{3/2}}{\pi m^2 v_0 K} d\theta$$

$$L^2 = m^2 v_0^2 s^2$$

$$= m^2 v_0^2 \left(\frac{K}{m v_0^2} \frac{(\pi - \theta)^2}{\theta(2\pi - \theta)} \right)$$

$$= \frac{mK (\pi - \theta)^2}{\theta(2\pi - \theta)}$$

$$ds = \frac{\left(\frac{mk(\pi - \theta)^2}{\theta(2\pi - \theta)} + mk \right)^{3/2}}{\pi m^2 v_0 K} d\theta$$

$$= \frac{(mk)^{3/2} \left[\frac{(\pi - \theta)^2}{\theta(2\pi - \theta)} + 1 \right]^{3/2}}{\pi m^2 v_0 K} d\theta$$

$$= \frac{(mk)^{3/2}}{\pi m^2 v_0 K} \left[\frac{(\pi - \theta)^2 + \theta(2\pi - \theta)}{\theta(2\pi - \theta)} \right]^{3/2} d\theta$$

$$= \frac{(mk)^{3/2}}{\pi m^2 v_0 K} \left[\frac{\pi^2 - 2\pi\theta + \theta^2 + 2\pi\theta - \theta^2}{\theta(2\pi - \theta)} \right]^{3/2} d\theta$$

$$ds = \frac{(mk)^{3/2}}{\pi m^2 v_0 K} \left[\frac{\pi^2}{\theta(2\pi - \theta)} \right]^{3/2} d\theta$$

Now,

$$d\sigma = 2\pi s ds$$

$$= 2\pi \left[\frac{K}{m^2 v_0^2} \frac{(\pi - \theta)^2}{\theta(2\pi - \theta)} \right]^{1/2} \frac{(mk)^{3/2}}{\pi m^2 v_0 K} \left[\frac{\pi^2}{\theta(2\pi - \theta)} \right]^{3/2} d\theta$$

$$= 2\pi^3 \left(\frac{K}{m^2 v_0^2} \right)^{1/2} \frac{(mk)^{3/2}}{m^2 v_0 K} \frac{(\pi - \theta)}{\theta^2 (2\pi - \theta)^2} d\theta$$

$$\boxed{d\sigma = 2\pi^3 \frac{K}{m^2 v_0^2} \frac{(\pi - \theta)}{\theta^2 (2\pi - \theta)^2} d\theta}$$

3-73

$$\vec{B} = B_0 \hat{z}$$

$$\vec{E} = E_0 \hat{x} \sin\left(\frac{qB_0}{mc} t\right)$$

$$\vec{F} = q\vec{E} + \frac{q}{c} \vec{v} \times \vec{B}$$

$$F_x = qE_0 \sin\left(\frac{qB_0}{mc} t\right) + \frac{q}{c} v_y B_0$$

$$F_y = -\frac{q}{c} v_x B_0$$

$$F_z = 0 \rightarrow \boxed{z=0}$$

$$m\ddot{y} = qE_0 \sin\left(\frac{qB_0}{mc} t\right) + \frac{qB_0}{c} \dot{x}$$

$$\ddot{x} = \frac{q}{m} E_0 \sin\left(\frac{qB_0}{mc} t\right) + \frac{qB_0}{mc} \dot{y}$$

$$m\ddot{y} = -\frac{qB_0}{c} \dot{x}$$

$$\vec{r}(0) = 0$$

$$\dot{y} = -\frac{qB_0}{mc} \dot{x}$$

$$\vec{v}(0) = 0, t(0) = 0$$

$$\int_0^{\dot{y}} d\dot{y} = \int_0^{\dot{x}} -\frac{qB_0}{mc} d\dot{x}$$

$$\dot{y} = -\frac{qB_0}{mc} \dot{x}$$

$$\ddot{x} = \frac{q}{m} E_0 \sin\left(\frac{qB_0}{mc} t\right) - \left(\frac{qB_0}{mc}\right)^2 x$$

$$\ddot{x} + \left(\frac{qB_0}{mc}\right)^2 x = \frac{q}{m} E_0 \sin\left(\frac{qB_0}{mc} t\right)$$

Homogeneous solution

$$\ddot{x} + \left(\frac{qB_0}{mc}\right)^2 x = 0 \quad x = e^{\lambda t}$$

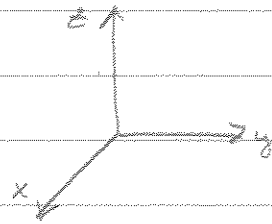
$$\lambda^2 + \left(\frac{qB_0}{mc}\right)^2 = 0$$

$$\lambda^2 = -\left(\frac{qB_0}{mc}\right)^2$$

$$\lambda = \pm i \frac{qB_0}{mc}$$

$$x = A \cos\left(\frac{qB_0}{mc} t\right) + B \sin\left(\frac{qB_0}{mc} t\right)$$

$$x_h = A \cos(\omega t) + B \sin(\omega t), \quad \omega = \frac{qB_0}{mc}$$



Particular solution

$$x_p = A \cos(\omega t) + B \sin(\omega t)$$

$$\dot{x} = -A\omega \sin \omega t + A \cos \omega t + B\omega \cos \omega t + B \sin \omega t$$

$$\ddot{x} = -A\omega^2 \cos \omega t - A\omega \sin \omega t - A\omega \sin \omega t - B\omega^2 \sin \omega t + B\omega \cos \omega t + B\omega \cos \omega t$$

$$= (-A\omega^2 + 2B\omega) \cos \omega t - (B\omega^2 + 2A\omega) \sin \omega t$$

Substituting $\ddot{x}$ and x into the differential equation gives

$$(-A\omega^2 + 2B\omega) \cos \omega t - (B\omega^2 + 2A\omega) \sin \omega t + \omega^2 [A \cos \omega t + B \sin \omega t] = \frac{q}{m} E_0 \sin \omega t$$

Equating coefficients,

$$-A\omega^2 + 2B\omega + A\omega^2 = 0 \rightarrow B = 0$$

$$-B\omega^2 - 2A\omega + B\omega^2 = \frac{q}{m} E_0$$

$$A = -\frac{qE_0}{2m\omega}$$

$$x_p = -\frac{qE_0}{2m\omega} t \cos(\omega t)$$

General solution is

$$x = x_h + x_p$$

$$x = A \cos \omega t + B \sin \omega t - \frac{qE_0}{2m\omega} t \cos \omega t$$

$$0 = x(0) = A$$

$$x = B \sin \omega t - \frac{qE_0}{2m\omega} t \cos \omega t$$

$$\dot{x} = B\omega \cos \omega t + \frac{qE_0}{2m} t \sin \omega t - \frac{qE_0}{2m\omega} \cos \omega t$$

$$0 = \dot{x}(0) = B\omega - \frac{qE_0}{2m\omega}$$

$$B = \frac{qE_0}{2m\omega^2}$$

$$x = \frac{qE_0}{2m\omega^2} \sin \omega t - \frac{qE_0}{2m\omega} t \cos \omega t$$

$$x = \frac{qE_0}{2m\omega^2} (\sin \omega t - \omega t \cos \omega t)$$

$$\dot{y} = -\omega x$$

$$\int_0^t dy = -\omega \int_0^t x dt$$

$$y = -\omega \int_0^t \left[\frac{qE_0}{2m\omega^2} \sin \omega t - \frac{qE_0}{2m\omega} t \cos \omega t \right] dt$$

$$= -\frac{qE_0}{2m\omega} \int_0^t [\sin \omega t - \omega t \cos \omega t] dt$$

$$= -\frac{qE_0}{2m\omega} \left[\int_0^t \sin \omega t dt - \omega \int_0^t t \cos \omega t dt \right]$$

$$\text{let } u = t \quad du = dt$$

$$= -\frac{qE_0}{2m\omega} \left[-\frac{1}{\omega} \cos \omega t \Big|_0^t - \omega \left(\frac{t}{\omega} \sin \omega t \Big|_0^t - \int_0^t \frac{1}{\omega} \sin \omega t dt \right) \right]$$

$$= -\frac{qE_0}{2m\omega} \left[-\frac{1}{\omega} \cos \omega t \Big|_0^t - t \sin \omega t \Big|_0^t - \frac{1}{\omega} \cos \omega t \Big|_0^t \right]$$

$$= -\frac{qE_0}{2m\omega} \left[-\frac{1}{\omega} \cos \omega t + \frac{1}{\omega} - t \sin \omega t - \frac{1}{\omega} \cos \omega t + \frac{1}{\omega} \right]$$

$$= -\frac{qE_0}{2m\omega} \left[-\frac{2}{\omega} \cos \omega t + \frac{2}{\omega} - t \sin \omega t \right]$$

$$y = \frac{qE_0}{2m\omega^2} \left[2 \cos \omega t - 2 + \omega t \sin \omega t \right]$$

$$\omega = \frac{qB_0}{mc}$$

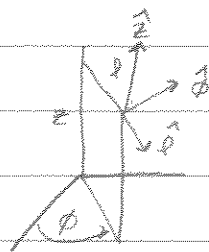
$$x = \frac{E_0 mc^2}{2 B_0^2 q} \left[\sin \left(\frac{qB_0}{mc} t \right) - \frac{qB_0}{mc} t \cos \left(\frac{qB_0}{mc} t \right) \right]$$

$$y = \frac{E_0 mc^2}{2 B_0^2 q} \left[2 \cos \left(\frac{qB_0}{mc} t \right) - 2 + \frac{qB_0}{mc} t \sin \left(\frac{qB_0}{mc} t \right) \right]$$

3-75

$$\vec{B} = B\hat{z}$$

$$E = \frac{q}{r}\hat{r}$$



$$\frac{d\hat{r}}{d\phi} = \hat{\phi} \quad \frac{d\hat{\phi}}{d\phi} = -\hat{r}$$

a)
$$\vec{F} = q\vec{E} + \frac{q}{c}\vec{v} \times \vec{B}$$

$$\frac{q}{c}\vec{v} \times \vec{B} = \frac{q}{c} \begin{vmatrix} \hat{r} & \hat{\phi} & \hat{z} \\ \dot{r} & r\dot{\phi} & \dot{z} \\ 0 & 0 & B \end{vmatrix}$$

$$v_{\phi} = r\dot{\phi}$$

$$= \frac{q}{c} r\dot{\phi} B \hat{r} - \frac{q}{c} \dot{z} B \hat{\phi}$$

$$\vec{F} = q \frac{q}{r} \hat{r} + \frac{qB}{c} r\dot{\phi} \hat{r} - \frac{qB}{c} \dot{z} \hat{\phi}$$

For cylindrical coordinates

$$\vec{a} = (\ddot{r} - r\dot{\phi}^2)\hat{r} + (r\ddot{\phi} + 2\dot{r}\dot{\phi})\hat{\phi} + \ddot{z}\hat{z}$$

$$\vec{F} = m\vec{a} = q \frac{q}{r} \hat{r} + \frac{qB}{c} r\dot{\phi} \hat{r} - \frac{qB}{c} \dot{z} \hat{\phi}$$

$$(\ddot{r} - r\dot{\phi}^2)\hat{r} = \frac{q^2}{mr} \hat{r} + \frac{qB}{mc} r\dot{\phi} \hat{r}, \quad (r\ddot{\phi} + 2\dot{r}\dot{\phi})\hat{\phi} = -\frac{qB}{mc} \dot{z} \hat{\phi}$$

$$\ddot{z} = 0$$

$$\dot{z} = \dot{z}_0$$

$$z = z_0 + \dot{z}_0 t$$

$$r^2\ddot{\phi} + 2r\dot{r}\dot{\phi} = -\frac{qB}{mc} \dot{z}$$

$$m(r^2\ddot{\phi} + 2r\dot{r}\dot{\phi}) = -\frac{qB}{c} \dot{z}$$

$$\frac{d}{dt}(mr^2\dot{\phi}) = -\frac{qB}{c} \dot{z}$$

$$\frac{dL}{dt} = -\frac{qB}{c} \dot{z}$$

$$dL = -\frac{qB}{c} \dot{z} dt$$

$$L = -\frac{qB}{2c} z^2$$

b) L_B is the angular momentum due to the B field. Another component of L , due to the central force $q\vec{E}$ acting on a ϕ component is $L_{\phi} = m\dot{\phi}r^2$. Therefore, the total angular momentum is a constant.

$$L_{\dot{\phi}} + L_B = K$$

$$\boxed{m\dot{\phi}^2 + \frac{qB}{2c}\ell^2 = K}$$

$$c) \quad T + qU = E \quad U = - \int_{\ell_s}^{\ell} \vec{E} \cdot d\vec{r}$$

$$\frac{1}{2}m\dot{\phi}^2 + \frac{1}{2}mV_{\text{tan}}^2 + qU = E$$

$$V_{\text{tan}} = \ell\dot{\phi}$$

$$\frac{1}{2}m\dot{\phi}^2 + \frac{1}{2}m\ell^2\dot{\phi}^2 + qU = E$$

$$\dot{\phi} = \frac{K - \frac{qB}{2c}\ell^2}{m\ell^2}$$

$$\frac{1}{2}m\dot{\phi}^2 + \frac{1}{2}m\ell^2\left(\frac{2Kc - qB\ell^2}{2mc\ell^2}\right)^2 + qU = E = \frac{K}{m\ell^2} - \frac{qB}{2mc} = \frac{2Kc - qB\ell^2}{2mc\ell^2}$$

$$\frac{1}{2}m\dot{\phi}^2 + \frac{(2Kc - qB\ell^2)^2}{8mc^2\ell^2} + qU = E$$

$$\frac{1}{2}m\dot{\phi}^2 = E - qU - \frac{(2Kc - qB\ell^2)^2}{8mc^2\ell^2}$$

$$\frac{d\ell}{dt} = \dot{\phi} = \sqrt{\frac{2}{m}} \left(E - qU - \frac{(2Kc - qB\ell^2)^2}{8mc^2\ell^2} \right)^{1/2}$$

$$\int_{\ell_0}^{\ell} \frac{d\ell}{\left(E - qU - \frac{(2Kc - qB\ell^2)^2}{8mc^2\ell^2} \right)^{1/2}} = \sqrt{\frac{2}{m}} t$$

$$U = - \int_{\ell_s}^{\ell} \frac{a}{\ell} d\ell$$

$$= -a \ln \ell \Big|_{\ell_s}^{\ell}$$

$$= -a \ln \frac{\ell}{\ell_s}$$

$$= a \ln \frac{\ell_s}{\ell}, \quad 0 < \ell \leq \ell_s$$

$$'V(\ell) = qU + \frac{(2Kc - qB\ell^2)^2}{8mc^2\ell^2}$$

$$= qa \ln \frac{\ell_s}{\ell} + \frac{(2Kc - qB\ell^2)^2}{8mc^2\ell^2}$$

$$= qa \ln \frac{\ell_s}{\ell} + \frac{4K^2c^2 - 4Kc qB\ell^2 + q^2B^2\ell^4}{8mc^2\ell^2}$$

$$'V(\ell) = qa \ln \frac{\ell_s}{\ell} + \frac{K^2}{2m\ell^2} - \frac{KqB}{2mc} + \frac{q^2B^2\ell^2}{8mc^2}$$

$$V'(r) = qU + \frac{K^2}{2m} \frac{1}{r^2} - \frac{KqB}{2mc} + \frac{q^2 B^2}{8mc^2} r^2$$

$$\frac{dV'}{dr} = -qE - \frac{K^2}{m} \frac{1}{r^3} + \frac{q^2 B^2}{4mc^2} r$$

$$0 = -qE - \frac{K^2}{m} \frac{1}{r^3} + \frac{q^2 B^2}{4mc^2} r$$

$$= -qEr^3 - \frac{K^2}{m} + \frac{q^2 B^2}{4mc^2} r^4$$

$$= -qEr^3 - \frac{K^2}{m} + \frac{q^2 B^2}{4mc^2} r^4$$

$$r^4 - \frac{4mc^2}{q^2 B^2} qEr^3 - \frac{4mc^2}{q^2 B^2} \frac{K^2}{m} = 0$$

$$r^4 - \frac{4mc^2 a}{B^2 q} r^3 - \frac{4K^2 c^2}{q^2 B^2} = 0$$

$$r^4 - \frac{4mc^2 a}{B^2 q} r^3 + \left(\frac{2mc^2 a}{B^2 q} \right)^2 = \left(\frac{2Kc}{qB} \right)^2 + \left(\frac{2mc^2 a}{B^2 q} \right)^2$$

$$\left(r^2 - \frac{2mc^2 a}{B^2 q} \right)^2 = \frac{4K^2 c^2}{q^2 B^2} + \frac{4m^2 c^4 a^2}{B^4 q^2}$$

$$= \frac{4K^2 B^2 c^2 + 4m^2 c^4 a^2}{B^4 q^2}$$

$$r_0^2 = \frac{2mc^2 a}{B^2 q} \pm \frac{2c}{B^2 q} (K^2 B^2 + m^2 c^2 a^2)^{1/2}$$

d) For circular motion $\dot{z}_0 = 0, \dot{r}_0 = 0$

$$(\dot{r} - r\dot{\phi}^2) = \frac{qA}{m\dot{r}} + \frac{qB}{mc} r\dot{\phi}$$

$$-r\dot{\phi}^2 = \frac{qA}{m\dot{r}} + \frac{qB}{mc} r\dot{\phi}$$

$$\dot{\phi}^2 + \frac{qB}{mc} \dot{\phi} + \frac{qA}{m\dot{r}^2} = 0$$

$$\left(\dot{\phi}_0 + \frac{qB}{2mc} \right)^2 = \left(\frac{qB}{2mc} \right)^2 - \frac{qA}{m\dot{r}_0^2} \quad \{ r = r_0 \} \quad \{ \dot{\phi} = \dot{\phi}_0 \}$$

$$\dot{\phi}_0 = -\frac{qB}{2mc} \pm \left(\left(\frac{qB}{2mc} \right)^2 - \frac{qA}{m\dot{r}_0^2} \right)^{1/2}$$

$$e) \quad \omega_f^2 = \frac{1}{m} \left(\frac{d^2 \psi}{d\rho^2} \right) \rho_0$$

$$= \frac{1}{m} \frac{d}{d\rho} \left[-\frac{qA}{\rho} - \frac{K^2}{m} \frac{1}{\rho^3} + \frac{q^2 B^2}{4mc^2} \rho \right] \rho_0$$

$$= \frac{1}{m} \left[\frac{qA}{\rho^2} + \frac{3K^2}{m\rho^4} + \frac{q^2 B^2}{4mc^2} \right] \rho_0$$

$$= \left(\frac{qA}{m\rho_0^2} + \frac{3K^2}{m^2\rho_0^4} + \left(\frac{qB}{2mc} \right)^2 \right) \rho_0 \quad K = \frac{2mc\rho_0^2 \dot{\phi} + qB\rho_0^2}{2c}$$

$$= \left(\frac{qA}{m\rho_0^2} + \frac{3 \left[\frac{2mc\rho_0^2 \dot{\phi} + qB\rho_0^2}{2c} \right]^2}{4m^2 c^2} + \left(\frac{qB}{2mc} \right)^2 \right) \rho_0 \quad K^2 = \rho_0^4 \left[\frac{2mc\dot{\phi} + qB}{4c} \right]^2$$

$$= \left(\frac{qA}{m\rho_0^2} + 3 \left(\frac{2mc\dot{\phi} + qB}{2mc} \right)^2 + \left(\frac{qB}{2mc} \right)^2 \right) \rho_0$$

$$= \left(\frac{qA}{m\rho_0^2} + 3 \frac{(4m^2 c^2 \dot{\phi}^2 + 4mcqB\dot{\phi} + q^2 B^2)}{(2mc)^2} + \left(\frac{qB}{2mc} \right)^2 \right) \rho_0$$

$$= \left(\frac{qA}{m\rho_0^2} + \frac{3m^2 c^2 \left(-\frac{qA}{m\rho_0^2} - \frac{qB\dot{\phi}}{mc} \right) + 3mcqB\dot{\phi} + 4 \left(\frac{qB}{2mc} \right)^2}{m^2 c^2} \right) \rho_0$$

$$= \left(\frac{qA}{m\rho_0^2} - \frac{3qA}{m\rho_0^2} - \frac{3qB\dot{\phi}}{mc} + \frac{3qB\dot{\phi}}{mc} + 4 \left(\frac{qB}{2mc} \right)^2 \right) \rho_0$$

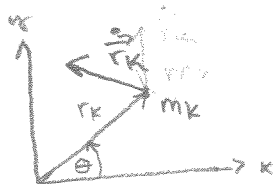
$$= 4 \left(\frac{qB}{2mc} \right)^2 - \frac{2qA}{m\rho_0^2}$$

$$\boxed{\omega_f = \pm 2 \left[\left(\frac{qB}{2mc} \right)^2 - \frac{qA}{2m\rho_0^2} \right]^{1/2}}$$

4-1

$$\vec{L}_{K0} = m_K \vec{r}_K \times \dot{\vec{r}}_K$$

$$\dot{\vec{r}}_K = \dot{r} \hat{r} + r \dot{\theta} \hat{\theta}$$



$$\begin{aligned} \vec{L}_{K0} &= m_K \vec{r}_K \times (\dot{r} \hat{r} + r \dot{\theta} \hat{\theta}) \\ &= m_K r \hat{r} \times (\dot{r} \hat{r} + r \dot{\theta} \hat{\theta}) \\ &= m_K [r \hat{r} \times \dot{r} \hat{r} + r \hat{r} \times r \dot{\theta} \hat{\theta}] \end{aligned}$$

$$\vec{L}_{K0} = m_K r \hat{r} \times r \dot{\theta} \hat{\theta} = m r^2 \dot{\theta} \hat{z}$$

$$\begin{aligned} \frac{d\vec{L}_{K0}}{dt} &= \frac{d}{dt} (m_K \vec{r}_K \times \dot{\vec{r}}_K) \\ &= \vec{r}_K \times \frac{d}{dt} (m \dot{\vec{r}}) + \frac{d\vec{r}_K}{dt} \times m \dot{\vec{r}} \\ &= \vec{r}_K \times m \ddot{\vec{r}} + \dot{\vec{r}} \times m \dot{\vec{r}} \\ &= \vec{r}_K \times m \ddot{\vec{r}} \\ &= \vec{r}_K \times \vec{F} \quad \{ \vec{F} = m \ddot{\vec{r}} \} \end{aligned}$$

If the external applied force is zero then

$$\frac{d\vec{L}_{K0}}{dt} = 0$$

$$\vec{L}_{K0} = \text{constant}$$

$$\vec{L}_{K0} = m r^2 \dot{\theta} \hat{z} = \text{constant}$$

4-29

A spaceship of mass m , initial velocity $\vec{v}_0$ approaches the moon and passes by. The distance of closest approach is R (measured from the moon's center). The velocity $\vec{v}_0$ is perpendicular to the orbit velocity $\vec{v}$ of the moon. Show that if the spaceship passes behind the moon, it will gain kinetic energy and calculate the increase of kinetic energy as it leaves the vicinity of the moon. Assume $M \gg m$, where M is the moon's mass.

This is a 2-body problem which can be separated into two one body systems. The one system is the center of mass and the other is the motion of one mass relative to the other. A derivation of this approach is instructive.

The equations of motion in a reference frame with an arbitrary origin are

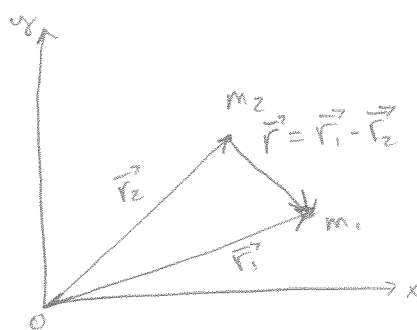
$$m_1 \ddot{\vec{r}}_1 = -\frac{dV}{dr_1} \hat{r}_1$$

$$m_2 \ddot{\vec{r}}_2 = -\frac{dV}{dr_2} \hat{r}_2$$

$$V = \frac{-Gm_1 m_2}{|\vec{r}_1 - \vec{r}_2|}$$

$$\text{Let } \vec{r} = \vec{r}_1 - \vec{r}_2$$

$$V = \frac{-Gm_1 m_2}{r}$$



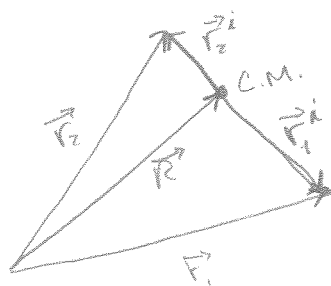
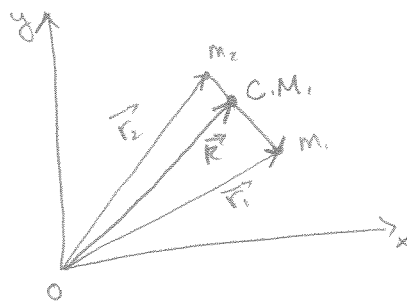
Now, the center of mass (C.M.) is on the line between m_1 and m_2 . Its location is found from

$$\vec{R} = \frac{m_1 \vec{r}_1 + m_2 \vec{r}_2}{m_1 + m_2}$$

The total momentum of m_1 and m_2 is equivalent to $(m_1 + m_2) \dot{\vec{R}}$

$$\text{Let } \vec{r}_1' = \vec{r}_1 - \vec{R}$$

$$\vec{r}_2' = \vec{r}_2 - \vec{R}$$



$$\vec{v}_1' = \vec{v}_1 - \vec{v}_{cm}$$

$$\vec{v}_2' = \vec{v}_2 - \vec{v}_{cm}$$

$$\vec{v}_1 = \vec{v}_1' + \vec{v}_{cm}$$

$$\vec{v}_2 = \vec{v}_2' + \vec{v}_{cm}$$

where $\vec{v}_1$ and $\vec{v}_2$ are in the laboratory frame, and $\vec{v}_1'$ and $\vec{v}_2'$ are in the center of mass frame. The relation between the center of mass coordinates and the relative coordinate $\vec{r}$ is found by:

$$\vec{R} = \frac{m_1 \vec{r}_1 + m_2 \vec{r}_2}{m_1 + m_2}, \quad \vec{r} = \vec{r}_1 - \vec{r}_2$$

$$(m_1 + m_2) \vec{R} = m_1 \vec{r}_1 + m_2 (\vec{r}_1 - \vec{r})$$

$$= (m_1 + m_2) \vec{r}_1 - m_2 \vec{r}$$

$$\vec{r}_1 = \vec{R} + \frac{m_2}{m_1 + m_2} \vec{r}$$

$$(m_1 + m_2) \vec{R} = m_1 (\vec{r} + \vec{r}_2) + m_2 \vec{r}_2$$

$$= (m_1 + m_2) \vec{r}_2 + m_1 \vec{r}$$

$$\vec{r}_2 = \vec{R} - \frac{m_1}{m_1 + m_2} \vec{r}$$

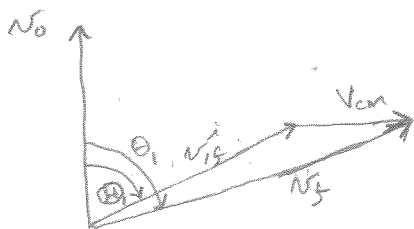
Therefore,

$$\vec{r}_1' = \frac{m_2}{m_1 + m_2} \vec{r}$$

$$\vec{r}_2' = -\frac{m_1}{m_1 + m_2} \vec{r}$$

$$\vec{v}_1' = \frac{m_2}{m_1 + m_2} \vec{v} = \frac{\mu}{m_1} \vec{v}, \quad \vec{v}_2' = -\frac{m_1}{m_1 + m_2} \vec{v} = -\frac{\mu}{m_2} \vec{v}, \quad \mu = \frac{m_1 m_2}{m_1 + m_2}$$

where $\vec{v}$ is the relative velocity between the two masses.



Θ_1 = scatter angle in C.M. frame

θ_1 = scatter angle in lab frame

$$\vec{v}_{cm} = \frac{M \vec{v}_1 + m \vec{v}_2}{M + m}$$

$$= \frac{M \vec{v}_1 + m \vec{v}_2}{M} \quad \{M \gg m\}$$

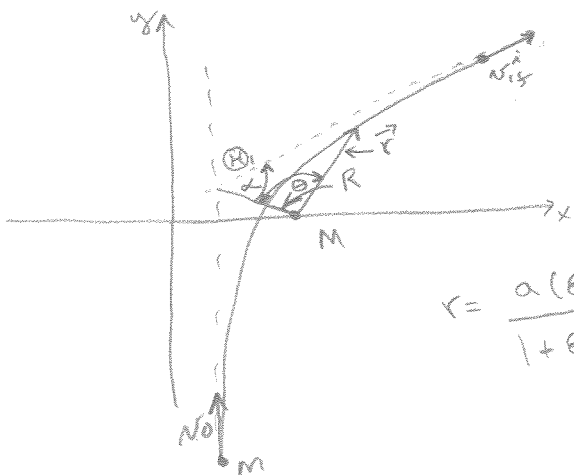
$$= \vec{v}_1 + \frac{m}{M} \vec{v}_2$$

$$= \vec{v}_1$$

$$r = \frac{a(E^2 - 1)}{1 + E \cos \theta}, \quad \text{at } r = \infty \quad 1 + E \cos \theta = 0 \quad \{ \theta = \alpha \}$$

$$\cos \alpha = \frac{-1}{E}$$

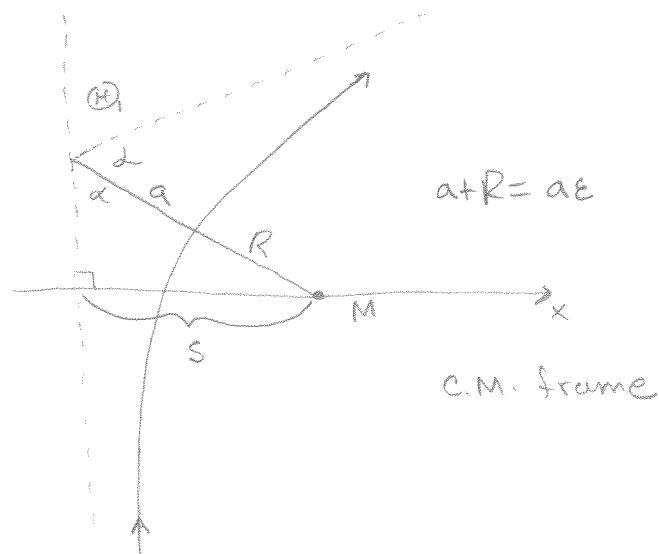
$$\cos \alpha = \frac{1}{E} \quad \{ + \text{branch} \}$$



The scattering angle, Θ , is related to α by:

$$\Theta = \pi - 2\alpha$$

Therefore, α must be determined in terms of the given parameters.



For an ellipse or hyperbola, the semi-major axis, a , is

$$a = \left| \frac{K}{2E} \right| = \frac{GmM}{2E}$$

where E is the energy in the C.M. frame and constant $\rightarrow E = \frac{1}{2}\mu v_0^2$

The minimum radius for the hyperbola is

$$r_{\min} = a(\epsilon - 1)$$

$$R = r_{\min}$$

$$R = \frac{K}{2E}(\epsilon - 1)$$

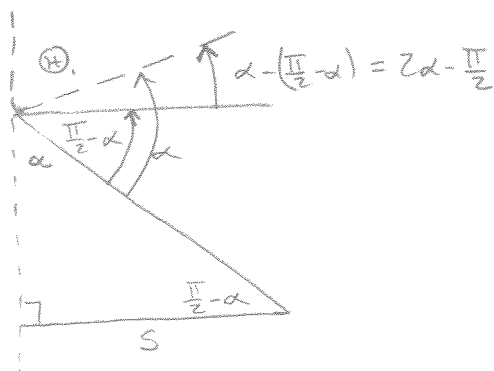
$$\cos \alpha = \frac{1}{\epsilon}$$

$$R = \frac{K}{\mu v_0^2} \left(\frac{1}{\cos \alpha} - 1 \right)$$

$$\frac{R\mu v_0^2}{K} + 1 = \frac{1}{\cos \alpha}$$

$$\frac{R\mu v_0^2 + K}{K} = \frac{1}{\cos \alpha}$$

$$\cos \alpha = \frac{K}{R\mu v_0^2 + K}$$



$$\cos \alpha = \frac{K}{Rm v_0^2 + K} \quad K = GmM, \quad u = \frac{mM}{m+M} \quad (4)$$

$$= \frac{GmM}{R \frac{mM}{m+M} v_0^2 + GmM}$$

$$\doteq \frac{GmM}{Rm v_0^2 + GmM} \quad \{M \gg m\}$$

$$\doteq \frac{GM}{R v_0^2 + GM}$$

$$\doteq \frac{\frac{GM}{R}}{v_0^2 + \frac{GM}{R}}$$

$$\cos \alpha \doteq \frac{C}{v_0^2 + C} \quad \{C = \frac{GM}{R}\}$$

$$\sin^2 \alpha = 1 - \frac{C^2}{(v_0^2 + C)^2}$$

$$= \frac{(v_0^2 + C)^2 - C^2}{(v_0^2 + C)^2}$$

$$= \frac{v_0^4 + 2v_0^2 C}{(v_0^2 + C)^2}$$

$$\sin \alpha = \frac{(v_0^4 + 2v_0^2 C)^{1/2}}{(v_0^2 + C)} = \frac{v_0 (v_0^2 + 2C)^{1/2}}{(v_0^2 + C)}$$

The components of $\vec{v}_f$ are in the lab frame

$$\vec{v}_f^i = v_f^i \cos(2\alpha - \frac{\pi}{2}) \hat{x} + v_f^i \sin(2\alpha - \frac{\pi}{2}) \hat{y}$$

$$= v_f^i (\sin 2\alpha \hat{x} - \cos 2\alpha \hat{y})$$

$$= v_f^i (2 \sin \alpha \cos \alpha \hat{x} - (2 \cos^2 \alpha - 1) \hat{y})$$

$$= \frac{u}{m} v (2 \sin \alpha \cos \alpha \hat{x} - (2 \cos^2 \alpha - 1) \hat{y})$$

$$= \frac{M}{m+M} v (2 \sin \alpha \cos \alpha \hat{x} - (2 \cos^2 \alpha - 1) \hat{y})$$

$$v_f^i \doteq v (2 \sin \alpha \cos \alpha \hat{x} - (2 \cos^2 \alpha - 1) \hat{y}) \quad \{M \gg m\}$$

At $\theta = \alpha$ (along the asymptote), $v = v_0$.

$$\sin(A-B) = \sin A \cos B - \cos A \sin B$$

$$\cos(A-B) = \cos A \cos B + \sin A \sin B$$

$$\sin 2\alpha = 2 \sin \alpha \cos \alpha$$

$$\cos 2\alpha = 2 \cos^2 \alpha - 1$$

$$\vec{V}_f = \vec{V}_f^i + \vec{V}_{cm} \quad \{ \text{laboratory frame} \}$$

$$= (V_0 2 \sin \alpha \cos \alpha + V) \hat{x} - V_0 (2 \cos^2 \alpha - 1) \hat{y}$$

$$V_f^2 = \vec{V}_f \cdot \vec{V}_f$$

$$= (2V_0 \sin \alpha \cos \alpha + V)^2 + (V_0 (2 \cos^2 \alpha - 1))^2$$

$$= 4V_0^2 \sin^2 \alpha \cos^2 \alpha + 4V V_0 \sin \alpha \cos \alpha + V_0^2 (4 \cos^4 \alpha - 4 \cos^2 \alpha + 1) + V^2$$

$$= 4V_0^2 \sin^2 \alpha \cos^2 \alpha + 4V V_0 \sin \alpha \cos \alpha + 4V_0^2 \cos^4 \alpha - 4V_0^2 \cos^2 \alpha + V_0^2 + V^2$$

$$= 4V V_0 \sin \alpha \cos \alpha + 4V_0^2 \sin^2 \alpha \cos^2 \alpha + 4V_0^2 \cos^4 \alpha - 4V_0^2 \cos^2 \alpha + V_0^2 + V^2$$

$$= 4V V_0 \sin \alpha \cos \alpha + 4V_0^2 \cos^2 \alpha (\sin^2 \alpha + \cos^2 \alpha - 1) + V_0^2 + V^2$$

$$V_f^2 = 4V V_0 \sin \alpha \cos \alpha + V_0^2 + V^2$$

The final kinetic energy of m is

$$E_f = \frac{1}{2} m (4V V_0 \sin \alpha \cos \alpha + V_0^2 + V^2)$$

The initial kinetic energy of m is

$$E_0 = \frac{1}{2} m V_0^2$$

The change in kinetic energy is

$$\Delta E = E_f - E_0$$

$$\Delta E = \frac{1}{2} m (4V V_0 \sin \alpha \cos \alpha + V^2)$$

$$\sin \alpha \cos \alpha = \frac{V_0 (V_0^2 + 2C)^{1/2}}{V_0^2 + C} \cdot \frac{C}{V_0^2 + C}$$

$$\Delta E = \frac{1}{2} m \left(\frac{4V V_0^2 C (V_0^2 + 2C)^{1/2}}{(V_0^2 + C)^2} + V^2 \right)$$

$$\Delta E = \frac{1}{2} m \left[\frac{4 \frac{GM}{R} V V_0^2 (V_0^2 + \frac{2GM}{R})^{1/2}}{(V_0^2 + \frac{GM}{R})^2} + V^2 \right]$$

4-31

Show that if the incident particle is much heavier than the target particle ($m_1 \gg m_2$), the Rutherford scattering cross section in laboratory coordinates is approximately

$$d\sigma = \left(\frac{q_1 q_2}{2m_2 v_0^2} \right)^2 \frac{4\gamma^2}{[1 - (1 - \gamma^2 \Theta_1^2)^{1/2}]^2 (1 - \gamma^2 \Theta_1^2)^{1/2}} 2\pi \sin \Theta_1 d\Theta_1$$

if $\gamma \Theta_1 < 1$, where $\gamma = \frac{m_1}{m_2}$. Otherwise, $d\sigma = 0$

the relation between Θ_1 and the relative (c.m.) frame Θ is

$$\tan \Theta_1 = \frac{\sin \Theta}{\cos \Theta + \frac{m_1}{m_2}} = \frac{\sin \Theta}{\cos \Theta + \gamma}$$

The scattering formula is

$$d\sigma = \left(\frac{q_1 q_2}{2m_2 v_0^2} \right)^2 \frac{2\pi \sin \Theta}{\sin^4(\frac{\Theta}{2})} d\Theta$$

If $\gamma \Theta_1 < 1$ and $\gamma \gg 1$ $\{m_1 \gg m_2\}$ then $\Theta_1 < 1$

$$\tan \Theta_1 \doteq \Theta_1$$

$$\Theta_1 \doteq \frac{\sin \Theta}{\cos \Theta + \gamma}$$

$$\Theta_1 \doteq \frac{\sin \Theta}{\gamma} \quad \{ \gamma \gg \cos \Theta \}$$

$$\gamma \Theta_1 \doteq \sin \Theta$$

Now,

$$\begin{aligned} \sin^4\left(\frac{\Theta}{2}\right) &= \left(\frac{1 - \cos \Theta}{2}\right)^2, & \cos \Theta &= (1 - \sin^2 \Theta)^{1/2} \\ &= \frac{[1 - (1 - \gamma^2 \Theta_1^2)^{1/2}]^2}{4} & &= (1 - \gamma^2 \Theta_1^2)^{1/2} \end{aligned}$$

Also,

$$\Theta_1 \doteq \frac{\sin \Theta}{\gamma} \rightarrow \sin \Theta_1 = \frac{\sin \Theta}{\gamma} \rightarrow \gamma \sin \Theta_1 = \sin \Theta$$

Taking the derivative of $\gamma\theta_1 = \sin\theta$ gives

$$\gamma d\theta_1 = \cos\theta d\theta$$

$$d\theta = \frac{\gamma d\theta_1}{\cos\theta}$$

$$d\theta = \frac{\gamma d\theta_1}{(1-\gamma^2\theta_1^2)^{1/2}}$$

Finally, substituting into the scattering formula:

$$d\sigma = \left(\frac{q_1 q_2}{2m v_0^2}\right)^2 \frac{2\pi \gamma \sin\theta_1}{\left[\frac{1-(1-\gamma^2\theta_1^2)^{1/2}}{4}\right]^2} \frac{\gamma d\theta_1}{(1-\gamma^2\theta_1^2)^{1/2}}$$

$$d\sigma = \left(\frac{q_1 q_2}{2m v_0^2}\right)^2 \frac{4\gamma^2}{[1-(1-\gamma^2\theta_1^2)^{1/2}]^2 (1-\gamma^2\theta_1^2)^{1/2}} 2\pi \sin\theta_1 d\theta_1$$

When $\gamma\theta_1 \geq 1$, $d\sigma$ becomes imaginary $\{\gamma\theta_1 > 1\}$ or undefined $\{\gamma\theta_1 = 1\}$. So,

$d\sigma = 0$ otherwise. Physically, this implies θ_1 is large but a massive incident particle will always have θ_1 small, so only γ can increase and the scattering angle θ tends to zero.

4-33 Assume that $m_2 \gg m_1$, and that $\Theta = \Theta_1 + \delta$, in Eq. (4.117). Find a formula for δ in terms of Θ_1 . Show that the first order correction to the Rutherford scattering cross section [Eq. (3.276)], due to the finite mass of m_2 , vanishes.

Eq. (4.117)

$$\tan \Theta_1 = \frac{\sin \Theta}{\cos \Theta + \frac{m_1}{m_2}}$$

$$\tan \Theta_1 = \frac{\sin(\Theta_1 + \delta)}{\cos(\Theta_1 + \delta) + \gamma} \quad \gamma = \frac{m_1}{m_2}$$

$$\{\cos(\Theta_1 + \delta) + \gamma\} \tan \Theta_1 = \sin(\Theta_1 + \delta)$$

$$\sin(A+B) = \sin A \cos B + \cos B \sin A$$

$$\cos(A+B) = \cos A \cos B - \sin A \sin B$$

$$\{\cos \Theta_1 \cos \delta - \sin \Theta_1 \sin \delta + \gamma\} \tan \Theta_1 = \sin \Theta_1 \cos \delta + \cos \Theta_1 \sin \delta$$

$$\sin \Theta_1 \cos \delta - \frac{\sin^2 \Theta_1 \sin \delta}{\cos \Theta_1} + \gamma \frac{\sin \Theta_1}{\cos \Theta_1} = \sin \Theta_1 \cos \delta + \cos \Theta_1 \sin \delta$$

When $m_2 \gg m_1$, $\Theta_1 \approx \Theta$. Therefore, $\delta \ll 1$.

$$\cos \alpha = 1 - \frac{\alpha^2}{2} + \dots$$

$$\sin \alpha = \alpha - \frac{\alpha^3}{3!} + \dots$$

$$\sin \Theta_1 \left(1 - \frac{\delta^2}{2}\right) - \frac{\sin^2 \Theta_1}{\left(1 - \frac{\delta^2}{2}\right)} \delta + \gamma \frac{\sin \Theta_1}{\cos \Theta_1} = \sin \Theta_1 \left(1 - \frac{\delta^2}{2}\right) + \cos \Theta_1 \delta$$

$$-\frac{\sin^2 \Theta_1}{1 - \frac{\delta^2}{2}} \delta + \gamma \frac{\sin \Theta_1}{\cos \Theta_1} = \cos \Theta_1 \delta$$

$$\frac{-\sin^2 \Theta_1 \cos \Theta_1 \delta + \gamma \sin \Theta_1 \left(1 - \frac{\delta^2}{2}\right)}{\left(1 - \frac{\delta^2}{2}\right) \cos \Theta_1} = \cos \Theta_1 \delta$$

$$-\sin^2 \Theta_1 \cos \Theta_1 \delta + \gamma \sin \Theta_1 - \gamma \sin \Theta_1 \frac{\delta^2}{2} = \cos^2 \Theta_1 \delta \left(1 - \frac{\delta^2}{2}\right)$$

$$= \cos^2 \Theta_1 \delta - \cos^2 \Theta_1 \frac{\delta^3}{2}$$

$$-\gamma \sin \Theta_1 \frac{\delta^2}{2} + \cos^2 \Theta_1 \frac{\delta^3}{2} - \sin^2 \Theta_1 \cos \Theta_1 \delta - \cos^2 \Theta_1 \delta + \gamma \sin \Theta_1 = 0$$

$$\frac{\cos^2 \Theta_1 - \gamma \sin \Theta_1}{2} \delta^2 - (\sin^2 \Theta_1 \cos \Theta_1 + \cos^2 \Theta_1) \delta + \gamma \sin \Theta_1 = 0$$

$$\delta = \frac{\sin^2 \Theta_1 \cos \Theta_1 + \cos^2 \Theta_1 \pm \left[(\sin^2 \Theta_1 \cos \Theta_1 + \cos^2 \Theta_1)^2 - 4 \left(\frac{\cos^2 \Theta_1 - \gamma \sin \Theta_1}{2} \right) \gamma \sin \Theta_1 \right]^{1/2}}{\cos^2 \Theta_1 - \gamma \sin \Theta_1}$$

For a finite mass of m_z , $\gamma \rightarrow 0$. Then

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$$f \doteq \frac{\sin^2\theta_1 \cos\theta_1 + \cos^3\theta_1 \pm [(\sin^2\theta_1 \cos\theta_1 + \cos^3\theta_1)^2 - 0]^{1/2}}{\cos^2\theta_1}$$

$$f \doteq \frac{\sin^2\theta_1 \cos\theta_1 + \cos^3\theta_1 \pm \sin^2\theta_1 \cos\theta_1 + \cos^3\theta_1}{\cos^2\theta_1}$$

Taking the difference gives

$$f \doteq 0$$

the sum has no physical significance since f must be small.

4-35 A pair of masses m_1, m_2 connected by a spring of force constant k , slide without friction along the x -axis. Show that the center of mass moves with uniform velocity and the masses oscillate with frequency $\left[k \frac{(m_1 + m_2)}{m_1 m_2} \right]^{1/2}$.

This is a two body problem.

$$M \ddot{\vec{R}} = \vec{F}_{ext} \quad \{ \text{center of mass} \}$$

$$\mu \ddot{\vec{r}} = \vec{F}_{int} \quad \{ \text{relative motion} \}$$

Since the external net forces are zero $\{ \text{horizontal frictionless motion} \}$

$$M \ddot{\vec{R}} = \vec{0}$$

$$\ddot{\vec{R}} = 0$$

$$\dot{\vec{R}} = \text{constant} \quad \{ \text{c.m. moving at uniform velocity} \}$$

The relative motion equation is a one body motion of reduced mass μ .

$$\mu \ddot{x} = -kx \quad \mu = \frac{m_1 m_2}{m_1 + m_2}$$

$$\mu \ddot{x} + kx = 0$$

$$\ddot{x} + \frac{k}{\mu} x = 0 \quad x = A e^{\gamma t}$$

$$\gamma^2 + \frac{k}{\mu} = 0$$

$$\gamma^2 = -\frac{k}{\mu}$$

$$\gamma = \pm i \left(\frac{k}{\mu} \right)^{1/2}$$

$$x = A e^{\pm i \left(\frac{k}{\mu} \right)^{1/2} t}$$

$$= A \cos \left(\left(\frac{k}{\mu} \right)^{1/2} t + \theta_1 \right)$$

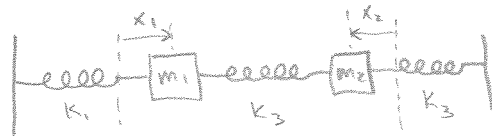
$$\omega = \left(\frac{k}{\mu} \right)^{1/2}$$

$$\omega = \left[k \frac{m_1 + m_2}{m_1 m_2} \right]^{1/2}$$

4-37 For the normal mode of vibration given by Eq. 4.162 and 4.163, find the force exerted on m_1 through the coupling spring, and show that the motion of x_1 satisfies the equation for a simple harmonic oscillator subject to a driving force.

$$x_1 = A_1 \cos(\omega t + \theta_1) \quad \{ \text{Eq. 4.162} \}$$

$$x_2 = \frac{\Delta \omega^2}{2K^2} \sqrt{\frac{m_1}{m_2}} A_1 \cos(\omega t + \theta_1) \quad \{ \text{Eq. 4.163} \}$$



The oscillation of m_1 and m_2 are out of phase. The force on m_1 through the coupling spring is

$$F = -K_3(x_2 + x_1)$$

$$F = -K_3 \left(A_1 \cos(\omega t + \theta_1) \left[1 + \frac{\Delta \omega^2}{2K^2} \sqrt{\frac{m_1}{m_2}} \right] \right)$$

The equation of motion of m_1 is

$$m_1 \ddot{x}_1 = F - Kx_1$$

$$m_1 \ddot{x}_1 + Kx_1 = F$$

This is the equation for a simple harmonic oscillator subject to a driving force.

4-39. Find the two normal modes of vibration for a pair of identical damped coupled harmonic oscillators {Egs. 4.180 and 4.181}. That is, $m_1 = m_2$, $b_1 = b_2$, $K_1 = K_2$.

The equations of motion are:

$$m\ddot{x}_1 = -Kx_1 - K_3(x_1 + x_2) - b\dot{x}_1 \quad m_1 = m_2 = m$$

$$m\ddot{x}_2 = -Kx_2 - K_3(x_1 + x_2) - b\dot{x}_2$$

$$m\ddot{x}_1 + b\dot{x}_1 + K'x_1 + K_3x_2 = 0 \quad K' = K + K_3$$

$$m\ddot{x}_2 + b\dot{x}_2 + K'x_2 + K_3x_1 = 0$$

Let

$$x_1 = C_1 e^{pt}$$

$$x_2 = C_2 e^{pt}$$

$$\ddot{x}_1 = p^2 C_1 e^{pt} \quad \dot{x}_1 = p C_1 e^{pt}$$

$$\ddot{x}_2 = p^2 C_2 e^{pt} \quad \dot{x}_2 = p C_2 e^{pt}$$

$$mC_1 p^2 + bC_1 p + K'C_1 + K_3 C_2 = 0$$

$$mC_2 p^2 + bC_2 p + K'C_2 + K_3 C_1 = 0$$

$$\frac{C_2}{C_1} = - \frac{mp^2 + bp + K'}{K_3} = - \frac{K_3}{mp^2 + bp + K'}$$

$$m^2 p^4 + mbp^3 + mK'p^2 + mbp^3 + b^2 p^2 + bK'p + mK'p^2 + bK'p + K'^2 - K_3^2 = 0$$

$$m^2 p^4 + 2mbp^3 + (2mK' + b^2)p^2 + 2bK'p + K'^2 - K_3^2 = 0$$

$$p^4 + \frac{2b}{m}p^3 + \left(\frac{2K'}{m} + \frac{b^2}{m^2}\right)p^2 + \frac{2bK'}{m^2}p + \frac{K'^2 - K_3^2}{m^2} = 0$$

The general form of the roots are:

$$p = -\gamma_1 \pm i\omega_1$$

$$p = -\gamma_2 \pm i\omega_2$$

For an uncoupled damped oscillator the solution is

$$p = -\gamma \pm i\omega, \quad \gamma = \frac{b}{2m}, \quad \omega = (\omega_0^2 - \gamma^2)^{1/2} \quad \{K_3 = 0\}$$

This solution is obtained from

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$$mp^2 + bp + k = 0$$

$$p^2 + \frac{b}{m}p + \frac{k}{m} = 0$$

$$p = -\frac{b}{2m} \pm \left[\left(\frac{b}{2m} \right)^2 - \frac{k}{m} \right]^{1/2}$$

Note also that the constant term, $\frac{k}{m}$, is a possible factor of

$$p^2 + \frac{b}{m}p + \frac{k}{m} = 0$$

Extending this to the equation

$$p^4 + \frac{zb}{m}p^3 + \left(\frac{2k}{m} + \frac{b^2}{m^2} \right)p^2 + \frac{2bk'}{m^2}p + \frac{k'^2 - k_3^2}{m^2} = 0$$

gives possible factors of

$$\frac{k'^2 - k_3^2}{m^2} = \frac{k' + k}{m} \frac{k' - k}{m}$$

Therefore, by analogy

$$p = -\gamma \pm i\omega_1 \quad \omega_1^2 = -\gamma^2 + \frac{k' + k}{m}$$

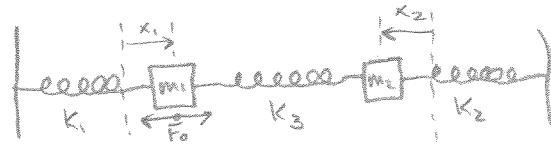
$$p = -\gamma \pm i\omega_2 \quad \omega_2^2 = -\gamma^2 + \frac{k' - k}{m}$$

The normal modes are:

$$x_1 = x_2 = Ae^{-\gamma t} \cos(\omega_1 t + \theta_1)$$

$$x_1 = -x_2 = Ae^{-\gamma t} \cos(\omega_2 t + \theta_2)$$

4-41 An applied force $F = F_0 \cos \omega t$ is applied to m_1 . Set up the equations of motion and find the steady state solution. Sketch the amplitude and phase of each oscillator as functions of ω .



$$m_1 \ddot{x}_1 = -K_1 x_1 - K_3(x_1 + x_2) + F_0 \cos \omega t$$

$$m_2 \ddot{x}_2 = -K_2 x_2 - K_3(x_1 + x_2)$$

$$m_1 \ddot{x}_1 + K'_1 x_1 + K_3 x_2 = F_0 \cos \omega t, \quad K'_1 = K_1 + K_3$$

$$m_2 \ddot{x}_2 + K'_2 x_2 + K_3 x_1 = 0, \quad K'_2 = K_2 + K_3$$

$$x_1 = C_1 e^{pt}$$

$$x_2 = C_2 e^{pt}$$

$$(m_1 p^2 + K'_1) C_1 + K_3 C_2 = 0 \quad \{ \text{homogeneous equations} \}$$

$$(m_2 p^2 + K'_2) C_2 + K_3 C_1 = 0$$

$$\frac{C_2}{C_1} = - \frac{m_1 p^2 + K'_1}{K_3} = - \frac{K_3}{m_2 p^2 + K'_2}$$

$$\frac{m_1 p^2 + K'_1}{K_3} = \frac{K_3}{m_2 p^2 + K'_2}$$

$$m_1 m_2 p^4 + (m_2 K'_1 + m_1 K'_2) p^2 + (K'_1 K'_2 - K_3^2) = 0$$

$$p^2 = \frac{-(m_2 K'_1 + m_1 K'_2) \pm \left[(m_2 K'_1 + m_1 K'_2)^2 - 4 m_1 m_2 (K'_1 K'_2 - K_3^2) \right]^{1/2}}{2 m_1 m_2}$$

$$p^2 = -\frac{1}{2} \left(\frac{K'_1}{m_1} + \frac{K'_2}{m_2} \right) \pm \left[\frac{1}{4} \left(\frac{K'_1}{m_1} + \frac{K'_2}{m_2} \right)^2 - \frac{K'_1 K'_2}{m_1 m_2} + \frac{K_3^2}{m_1 m_2} \right]^{1/2}$$

$$\text{Let } \omega_{10}^2 = \frac{K'_1}{m_1}, \quad \omega_{20}^2 = \frac{K'_2}{m_2}$$

$$p^2 = -\frac{1}{2} (\omega_{10}^2 + \omega_{20}^2) \pm \left[\frac{1}{4} (\omega_{10}^2 - \omega_{20}^2)^2 + \frac{K_3^2}{m_1 m_2} \right]^{1/2}$$

$$\text{Assume } \omega_{10}^2 \geq \omega_{20}^2$$

Then the quantity inside the square root brackets is always less than the square of the first term. Thus p^2 is always negative

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$$p^2 = -\omega_1^2 = -(\omega_{10}^2 + \frac{1}{2} \Delta\omega^2)$$

$$p^2 = -\omega_2^2 = -(\omega_{20}^2 - \frac{1}{2} \Delta\omega^2)$$

$$\Delta\omega^2 = (\omega_{10}^2 - \omega_{20}^2) \left[\left(1 + \frac{4K^2}{(\omega_{10}^2 - \omega_{20}^2)^2} \right)^{1/2} - 1 \right] \quad \{ \approx 4,150 \}$$

$$K^2 = \frac{K_3}{\sqrt{m_1 m_2}}$$

The four solutions are

$$p = \pm i\omega_1$$

$$p = \pm i\omega_2$$

When $p^2 = -\omega_1^2$

$$\frac{C_2}{C_1} = \frac{m_1(\omega_1^2 - \omega_{10}^2)}{K_3} = \frac{\Delta\omega^2}{2K^2} \sqrt{\frac{m_1}{m_2}}$$

when $p^2 = -\omega_2^2$

$$\frac{C_1}{C_2} = \frac{m_2(\omega_2^2 - \omega_{20}^2)}{K_3} = -\frac{\Delta\omega^2}{2K^2} \sqrt{\frac{m_2}{m_1}}$$

The general solution is the sum of the four solutions

$$X = X_1 + X_2$$

$$= C_1 e^{pt} + C_2 e^{pt}$$

$$X_1 = C_1 e^{i\omega_1 t} + C_1' e^{-i\omega_1 t} - \frac{\Delta\omega^2}{2K^2} \sqrt{\frac{m_2}{m_1}} C_2 e^{i\omega_2 t} - \frac{\Delta\omega^2}{2K^2} \sqrt{\frac{m_2}{m_1}} e^{-i\omega_2 t}$$

$$X_2 = \frac{\Delta\omega^2}{2K^2} \sqrt{\frac{m_1}{m_2}} C_2 e^{i\omega_1 t} + \frac{\Delta\omega^2}{2K^2} \sqrt{\frac{m_1}{m_2}} e^{-i\omega_1 t} + C_2 e^{i\omega_2 t} + C_2' e^{-i\omega_2 t}$$

For the solutions to be real set

$$C_1 = \frac{1}{2} A_1 e^{i\theta_1} \quad C_1' = \frac{1}{2} A_1 e^{-i\theta_1}$$

$$C_2 = \frac{1}{2} A_2 e^{i\theta_2} \quad C_2' = \frac{1}{2} A_2 e^{-i\theta_2}$$

Then

$$x_1 = A_1 \cos(\omega_1 t + \theta_1) - \frac{\Delta \omega^2}{2K_3} \sqrt{\frac{m_2}{m_1}} A_2 \cos(\omega_2 t + \theta_2)$$

$$x_2 = A_2 \cos(\omega_2 t + \theta_1) + \frac{\Delta \omega^2}{2K_3} \sqrt{\frac{m_1}{m_2}} A_1 \cos(\omega_2 t + \theta_1)$$

These are the homogeneous solutions.

The equations of motion in matrix form is

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} K_1 & K_3 \\ K_3 & K_2' \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F_0 \cos \omega t \\ 0 \end{bmatrix}$$

Let

$$x_1 = u_1 \cos \omega t$$

$$x_2 = u_2 \cos \omega t \quad \{m_2 \text{ will be forced by } F_0 \cos \omega t\}$$

$$\ddot{x}_1 = -u_1 \omega^2 \cos \omega t$$

$$\ddot{x}_2 = -u_2 \omega^2 \cos \omega t$$

The equations of motion are

$$-m_1 \omega^2 u_1 + K_1' u_1 + K_3 u_2 = F_0$$

$$-m_2 \omega^2 u_2 + K_2' u_2 + K_3 u_1 = 0$$

In matrix form

$$\begin{bmatrix} K_1' - m_1 \omega^2 & K_3 \\ K_3 & K_2' - m_2 \omega^2 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} F_0 \\ 0 \end{bmatrix}$$

$$\text{Let } [S] = \begin{bmatrix} K_1' - m_1 \omega^2 & K_3 \\ K_3 & K_2' - m_2 \omega^2 \end{bmatrix}$$

Then

$$\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = [S]^{-1} \begin{bmatrix} F_0 \\ 0 \end{bmatrix}$$

The inverse of $[S]$ is

$$[S]^{-1} = \frac{\text{adj}[S]}{\det[S]} \quad \{ \text{From matrix algebra} \}$$

$$\text{adj}[S] = \begin{bmatrix} k'_2 - m_2 \omega^2 & -k_3 \\ -k_3 & k'_1 - m_1 \omega^2 \end{bmatrix}$$

$$\det[S] = (k'_1 - m_1 \omega^2)(k'_2 - m_2 \omega^2) - k_3^2$$

Now,

$$\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \frac{1}{(k'_1 - m_1 \omega^2)(k'_2 - m_2 \omega^2) - k_3^2} \begin{bmatrix} k'_2 - m_2 \omega^2 & -k_3 \\ -k_3 & k'_1 - m_1 \omega^2 \end{bmatrix} \begin{bmatrix} F_0 \\ 0 \end{bmatrix}$$

$$u_1 = \frac{(k'_2 - m_2 \omega^2) F_0}{(k'_1 - m_1 \omega^2)(k'_2 - m_2 \omega^2) - k_3^2} = \frac{(m_2 \omega^2 - k'_2) F_0}{k_3^2 - (m_1 \omega^2 - k'_1)(m_2 \omega^2 - k'_2)}$$

$$u_2 = \frac{-k_3 F_0}{(k'_1 - m_1 \omega^2)(k'_2 - m_2 \omega^2) - k_3^2} = \frac{k_3 F_0}{k_3^2 - (m_1 \omega^2 - k'_1)(m_2 \omega^2 - k'_2)}$$

$$x_1 = \frac{(m_2 \omega^2 - k'_2) F_0 \cos \omega t}{k_3^2 - (m_1 \omega^2 - k'_1)(m_2 \omega^2 - k'_2)}$$

$$x_2 = \frac{k_3 F_0 \cos \omega t}{k_3^2 - (m_1 \omega^2 - k'_1)(m_2 \omega^2 - k'_2)}$$

Steady state solutions

The general solutions are

$$x_1 = A_1 \cos(\omega_1 t + \theta_1) - \frac{\Delta \omega}{2K^2} \sqrt{\frac{m_1}{m_2}} A_2 \cos(\omega_2 t + \theta_2) + \frac{(m_2 \omega^2 - k'_2) F_0 \cos \omega t}{k_3^2 - (m_1 \omega^2 - k'_1)(m_2 \omega^2 - k'_2)}$$

$$x_2 = A_2 \cos(\omega_2 t + \theta_2) + \frac{\Delta \omega}{2K^2} \sqrt{\frac{m_2}{m_1}} A_1 \cos(\omega_1 t + \theta_1) + \frac{k_3 F_0 \cos \omega t}{k_3^2 - (m_1 \omega^2 - k'_1)(m_2 \omega^2 - k'_2)}$$

Sketch of amplitude vs. ω

For m_1 :

$$X_{1s} = \frac{(m_2 \omega^2 - k'_2) F_0 \cos \omega t}{k_3^2 - (m_1 \omega^2 - k'_1)(m_2 \omega^2 - k'_2)}$$

$$k'_1 = m_1 \omega_{10}^2, k'_2 = m_2 \omega_{20}^2$$

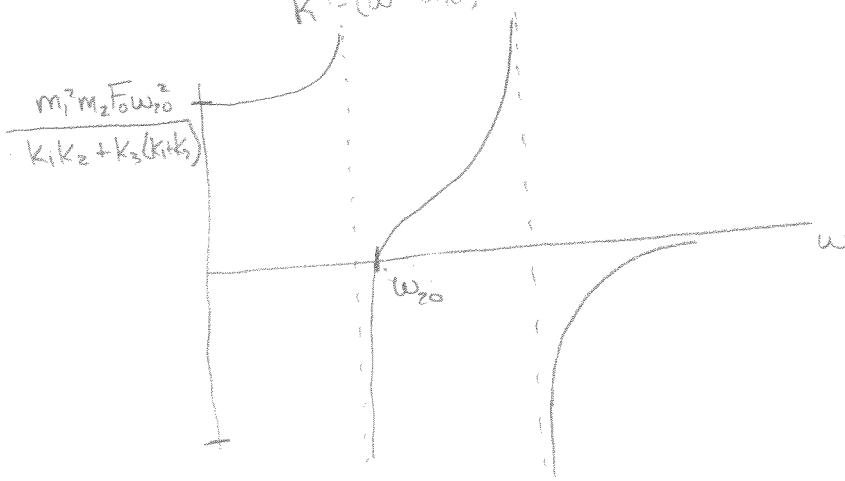
$$= \frac{(m_2 \omega^2 - m_2 \omega_{20}^2) F_0 \cos \omega t}{k_3^2 - (m_1 \omega^2 - m_1 \omega_{10}^2)(m_2 \omega^2 - m_2 \omega_{20}^2)}$$

$$= \frac{m_2 (\omega^2 - \omega_{20}^2) F_0 \cos \omega t}{k_3^2 - m_1 (\omega^2 - \omega_{10}^2) m_2 (\omega^2 - \omega_{20}^2)}$$

$$= \frac{m_2 (\omega^2 - \omega_{20}^2) F_0 \cos \omega t}{\frac{k_3^2}{m_1 m_2} - (\omega^2 - \omega_{10}^2)(\omega^2 - \omega_{20}^2)} \cdot \frac{1}{m_1 m_2}$$

$$X_{1s} = \frac{m_1 (\omega^2 - \omega_{20}^2) F_0 \cos \omega t}{K^4 - (\omega^2 - \omega_{10}^2)(\omega^2 - \omega_{20}^2)} \quad \left\{ K^2 = \frac{k_3}{\sqrt{m_1 m_2}} \right\}$$

$$A_1 = \frac{m_1 (\omega^2 - \omega_{20}^2) F_0}{K^4 - (\omega^2 - \omega_{10}^2)(\omega^2 - \omega_{20}^2)}$$



steady state amplitude vs. ω
Mass 1

when $\omega = 0$

$$A_1 = \frac{-m_1 F_0 \omega_{20}^2}{K^4 - (\omega_{10}^2)(\omega_{20}^2)}$$

$$= \frac{-m_1 F_0 \omega_{20}^2}{\frac{k_3^2}{m_1 m_2} - \left(\frac{k'_1}{m_1}\right)\left(\frac{k'_2}{m_2}\right)}$$

$$= \frac{-m_1 F_0 \omega_{20}^2}{\frac{1}{m_1 m_2} (k_3^2 - k'_1 k'_2)}$$

$$= \frac{-m_1 F_0 \omega_{20}^2}{\frac{1}{m_1 m_2} (k_3^2 - (k_1 + k_3)(k_2 + k_3))}$$

$$= \frac{-m_1 F_0 \omega_{20}^2}{\frac{1}{m_1 m_2} (k_3^2 - (k_1 k_2 + k_3(k_1 + k_2) + k_3^2))}$$

$$= \frac{-m_1 F_0 \omega_{20}^2}{\frac{1}{m_1 m_2} (-k_1 k_2 - k_3(k_1 + k_2))}$$

$$= \frac{m_1 F_0 \omega_{20}^2}{\frac{1}{m_1 m_2} (k_1 k_2 + k_3(k_1 + k_2))}$$

For m_2 :

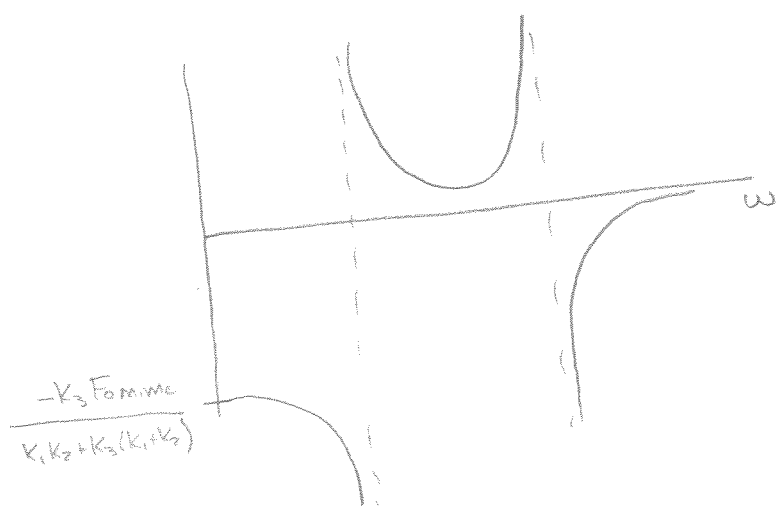
$$x_{zs} = \frac{k_3 F_0 \cos \omega t}{k_3^2 - (m_1 \omega^2 - k_1)(m_2 \omega^2 - k_2')}$$

$$x_{zs} = \frac{k_3 F_0 \cos \omega t}{K^4 - (\omega^2 - \omega_0^2)(\omega^2 - \omega_{20}^2)}$$

$$A_2 = \frac{k_3 F_0}{K^4 - (\omega^2 - \omega_0^2)(\omega^2 - \omega_{20}^2)}$$

when $\omega = 0$

$$\begin{aligned} A_2 &= \frac{k_3 F_0}{K^4 - (\omega^2 - \omega_0^2)(\omega^2 - \omega_{20}^2)} \\ &= \frac{-k_3 F_0 m_1 m_2}{k_1 k_2 + k_3(k_1 + k_2)} \end{aligned}$$



Steady state amplitude vs. ω
Mass 2

a) For a system of particles making up a rigid body

$$T = \sum_{k=1}^N \frac{1}{2} m_k v_k^2 \quad \{ \text{Eq. 4.37} \}$$

For a rigid body rotating about an axis, the moment of inertia of the rigid body made from a system of particles is

$$I_z = \sum_{k=1}^N m_k r_k^2$$

The tangential velocity is

$$v = r \dot{\theta}$$

$$v^2 = r^2 \dot{\theta}^2$$

For a system of particles

$$v_k^2 = r_k^2 \dot{\theta}^2 \quad \{ \dot{\theta} \text{ is the same for each particle of the rigid body} \}$$

Substituting v_k^2 into the kinetic energy equation gives

$$\begin{aligned} T &= \sum_{k=1}^N \frac{1}{2} m_k r_k^2 \dot{\theta}^2 \\ &= \frac{1}{2} \left(\sum_{k=1}^N m_k r_k^2 \right) \dot{\theta}^2 \end{aligned}$$

$$T = \frac{1}{2} I_z \dot{\theta}^2 \quad \{ \text{Eq. 5.16} \}$$

b) The definition of work is

$$W = \int_{x_0}^x \vec{F} \cdot d\vec{x}$$

Where $\vec{F}$ is the sum of external forces.

Torque is defined as

$$\vec{N}_z = \vec{F}_\theta r$$

$$N_z = \vec{F} \cdot \vec{r}_\perp$$

$$N_z = F_\theta r$$

Now,

$$d\vec{r}_\perp = r d\theta \hat{\theta}$$

$$d\vec{x} = d\vec{r}_\perp \\ = r d\theta \hat{\theta}$$

Substituting into the definition of work gives

$$V = - \int_{\theta_s}^{\theta} \vec{F} \cdot r d\theta \hat{\theta}$$

$$= - \int_{\theta_s}^{\theta} F_\theta r d\theta$$

$$V = - \int_{\theta_s}^{\theta} N_z d\theta \quad \{ \text{Eq. 5.14} \}$$

5-3

Starting with

$$\frac{dL}{dt} = I_z \ddot{\theta} = N_z$$

where N_z is a function of θ .

The energy theorem is

$$T_2 - T_1 = \int_{x_1}^{x_2} F dx$$

$$I_z \frac{d\dot{\theta}}{dt} = N_z$$

$$\frac{1}{2} I_z \dot{\theta}^2 - \frac{1}{2} I_z \dot{\theta}_0^2 = \int_{\theta_0}^{\theta} N_z d\theta$$

The potential energy is defined as

$$V = - \int_{x_0}^x F dx$$

$$= - \int_{\theta_0}^{\theta} N_z d\theta$$

$$- \int_{\theta_0}^{\theta} N_z d\theta = -V(\theta) + V(\theta_0)$$

Now,

$$\frac{1}{2} I_z \dot{\theta}^2 - \frac{1}{2} I_z \dot{\theta}_0^2 = -V(\theta) + V(\theta_0)$$

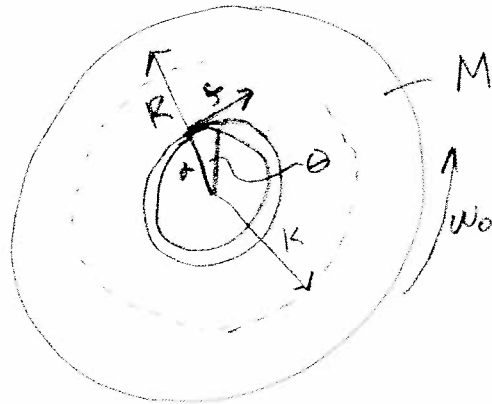
$$\frac{1}{2} I_z \dot{\theta}^2 + V(\theta) = \frac{1}{2} I_z \dot{\theta}_0^2 + V(\theta_0)$$

The quantity on the right only depends on the initial conditions and is therefore constant. So

$$T + V = \text{constant.}$$

- 5- 5. A wheel of mass M , radius of gyration k , spins smoothly on a fixed horizontal axle of radius a which passes through a hole of slightly larger radius at the hub of the wheel. The coefficient of friction between the bearing surfaces is μ . If the wheel is initially spinning with angular velocity ω_0 , find the time and the number of turns that it takes to stop.

Number of Turns (time on back side)



$$f = \mu Mg \cos \theta$$

Work-Energy Theorem:

$$\Delta K = W$$

$$\Delta K = \frac{1}{2} I \omega_0^2 - \frac{1}{2} I (0)$$

$$\Delta K = \frac{1}{2} I \omega_0^2$$

$$I = Mk^2$$

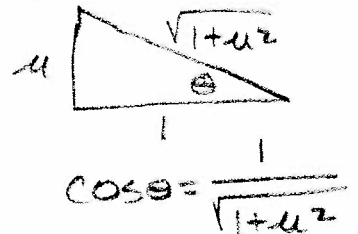
$$\Delta K = \frac{MK^2 \omega_0^2}{2}$$

$$W = T \theta \quad (T = \text{torque})$$

$$= f a \theta$$

$$= \mu a \cos \theta Mg \theta$$

$$\mu = \tan \theta \quad \{ \text{angle of repose} \}$$



$$\frac{MK^2 \omega_0^2}{2} = \mu Mga \theta \cos \theta$$

$$\frac{K^2 \omega_0^2}{2} = \mu ga \theta \frac{1}{\sqrt{1+\mu^2}}$$

$$\theta = \frac{K^2 \omega_0^2 \sqrt{1+\mu^2}}{2 \mu ga}$$

$$\boxed{\# \text{ of turns} = \frac{\theta}{2\pi} = \frac{K^2 \omega_0^2 \sqrt{1+\mu^2}}{4\pi \mu ga}}$$

$$\frac{dL}{dt} = T$$

$$dL = T dt$$

$$\int_0^{\omega_0} dL = T \int_0^{t_s} dt$$

$$L|_0^{\omega_0} = T t|_0^{t_s}$$

$$MK\omega_0^2 = \frac{\mu Mga}{\sqrt{1+\mu^2}} t_s$$

$$\boxed{\frac{K^2 \omega_0^2 \sqrt{1+\mu^2}}{\mu ga} = t_s}$$

$$T = f_a$$

$$= \mu Mga \cos \theta$$

$$= \frac{\mu Mga}{\sqrt{1+\mu^2}}$$

$$L = I \dot{\theta}$$

$$= MK^2 \dot{\theta}$$

5-7

$$I\ddot{\theta} = N + N_f$$

$$N = N_0(1 + \alpha \cos \omega_0 t)$$

$$N_f = -b\dot{\theta}$$

$$I\ddot{\theta} = N_0 + N_0\alpha \cos \omega_0 t - b\dot{\theta} \rightarrow I\ddot{\theta} + b\dot{\theta} = N_0 + N_0\alpha \cos \omega_0 t$$

$$\text{Eqn. 1 } I\ddot{\theta} = N_0 - b\dot{\theta}$$

$$I \frac{d\dot{\theta}}{dt} = N_0 - b\dot{\theta}$$

$$\frac{d\dot{\theta}}{N_0 - b\dot{\theta}} = \frac{dt}{I}$$

$$\int_0^{\dot{\theta}} \frac{d\dot{\theta}}{N_0 - b\dot{\theta}} = \int_0^t \frac{dt}{I}$$

$$u = N_0 - b\dot{\theta}$$

$$du = -b d\dot{\theta}$$

$$-\frac{du}{b} = d\dot{\theta}$$

$$-\frac{1}{b} \int \frac{du}{u} = -\frac{1}{b} \ln|u| + C$$

$$\int_0^{\dot{\theta}} \frac{d\dot{\theta}}{N_0 - b\dot{\theta}} = -\frac{1}{b} \ln|N_0 - b\dot{\theta}|_0^{\dot{\theta}}$$

$$= -\frac{1}{b} \ln \frac{N_0 - b\dot{\theta}}{N_0}$$

$$= -\frac{1}{b} \ln \left(1 - \frac{b\dot{\theta}}{N_0}\right)$$

$$-\frac{1}{b} \ln \left(1 - \frac{b\dot{\theta}}{N_0}\right) = \frac{t}{I}$$

$$\ln \left(1 - \frac{b\dot{\theta}}{N_0}\right) = -\frac{bt}{I}$$

$$1 - \frac{b\dot{\theta}}{N_0} = e^{-\frac{bt}{I}}$$

$$\dot{\theta} \frac{b}{N_0} = 1 - e^{-\frac{bt}{I}}$$

$$\dot{\theta} = \frac{N_0}{b} (1 - e^{-\frac{bt}{I}})$$

For steady state, $t \rightarrow \infty$

$$\dot{\theta}_s = \frac{N_0}{b}$$

$$\text{Eqn. 2 } I\ddot{\theta} = N_0\alpha \cos \omega_0 t - b\dot{\theta}$$

$$\ddot{\theta} + \frac{b}{I}\dot{\theta} = \frac{N_0\alpha}{I} \cos \omega_0 t$$

$$\theta_p = A \cos \omega_0 t + B \sin \omega_0 t$$

$$\dot{\theta}_p = -A\omega_0 \sin \omega_0 t + B\omega_0 \cos \omega_0 t$$

$$\ddot{\theta}_p = -A\omega_0^2 \cos \omega_0 t - B\omega_0^2 \sin \omega_0 t$$

$$-A\omega_0^2 \cos \omega_0 t - B\omega_0^2 \sin \omega_0 t + \frac{b}{I}(-A\omega_0 \sin \omega_0 t + B\omega_0 \cos \omega_0 t) = \frac{N_0\alpha}{I} \cos \omega_0 t$$

Equating like terms:

$$1) -A\omega_0^2 + B \frac{b}{I} \omega_0 = \frac{N_0\alpha}{I}$$

$$2) -B\omega_0^2 - A \frac{b}{I} \omega_0 = 0 \rightarrow B = -\frac{Ab}{I\omega_0}$$

$$-A\omega_0^2 - A \frac{b^2}{I^2} = \frac{N_0\alpha}{I}$$

$$-A(\omega_0^2 + \frac{b^2}{I^2}) = \frac{N_0\alpha}{I}$$

$$-A(\frac{I^2\omega_0^2 + b^2}{I^2}) = \frac{N_0\alpha}{I}$$

$$A = \frac{-N_0\alpha I}{I^2\omega_0^2 + b^2}$$

$$B = \frac{N_0\alpha b}{\omega_0(I^2\omega_0^2 + b^2)}$$

$$\theta_p = \frac{-N_0\alpha I}{I^2\omega_0^2 + b^2} \cos \omega_0 t + \frac{N_0\alpha b}{I\omega_0(I^2\omega_0^2 + b^2)} \sin \omega_0 t$$

The homogeneous equation $\rightarrow 0$ as $t \rightarrow \infty$,
of the form e^{-kt} .

$$\theta_{s_2} = \frac{N_0\alpha b}{\omega_0(I^2\omega_0^2 + b^2)} \sin \omega_0 t - \frac{N_0\alpha I}{I^2\omega_0^2 + b^2} \cos \omega_0 t$$

$$d\theta_{s_1} = \frac{N_0}{b} dt$$

$$\int_{\theta_0}^{\theta_{s_1}} d\theta_{s_1} = \int_0^t \frac{N_0}{b} dt$$

$$\theta_{s_1} - \theta_0 = \frac{N_0}{b} t$$

$$\boxed{\theta_{s_1} = \theta_0 + \frac{N_0}{b} t}$$

$$\theta_s = \theta_{s_1} + \theta_{s_2}$$

$$= \theta_0 + \frac{N_0}{b} t + \frac{N_0 \times b}{\omega_0 (I^2 \omega_0^2 - b^2)} \sin \omega_0 t - \frac{N_0 \times I}{I^2 \omega_0^2 - b^2} \cos \omega_0 t$$

$$\boxed{\theta_s = \theta_0 + \frac{N_0}{b} t + \frac{N_0}{I^2 \omega_0^3 - b^2 \omega_0} [b \sin \omega_0 t - I \omega_0 \cos \omega_0 t]}$$

5-9

i) Solve for ϕ

$$\phi + \frac{1}{8}a^2(z\phi - \sin z\phi) + \dots = \left(\frac{a}{2}\right)^{1/2}t \quad \{ \text{Eq. 5.33} \}$$

$$\begin{aligned} \phi &= \left(\frac{a}{2}\right)^{1/2}t - \frac{1}{8}a^2(z\phi - \sin z\phi) \\ &= \omega_0 t - \frac{a^2}{4}\phi + \frac{a^2}{8}\sin z\phi \quad \{ \omega_0 = \left(\frac{a}{2}\right)^{1/2} \} \end{aligned}$$

First approximation

$$\phi^{(1)} = \omega_0 t$$

Second approximation

$$\phi^{(2)} = \omega_0 t - \frac{a^2}{4}\phi^{(1)} + \frac{a^2}{8}\sin z\phi^{(1)}$$

$$\phi^{(2)} = \omega_0 t - \frac{a^2}{4}\omega_0 t + \frac{a^2}{8}\sin z\omega_0 t$$

$$= \omega_0 t - \frac{1}{4}\left(\frac{K}{2} - \frac{K^3}{48}\right)\omega_0 t + \frac{1}{8}\left(\frac{K}{2} - \frac{K^3}{48}\right)^2 \sin 2\omega_0 t$$

$$= \omega_0 t - \frac{1}{4}\left(\frac{K^2}{4} + \text{terms} > K^3\right)\omega_0 t + \frac{1}{8}\left(\frac{K^2}{4} + \text{terms} > K^3\right)\sin 2\omega_0 t$$

$$\doteq \omega_0 t - \frac{K^2}{16}\omega_0 t + \dots$$

$$\begin{aligned} a &= \sin \frac{K}{2} \\ &\doteq \frac{K}{2} - \frac{K^3}{8 \cdot 3!} = \frac{K}{2} - \frac{K^3}{48} \end{aligned}$$

$$\phi^{(2)} = \omega_0 t \left(1 - \frac{K^2}{16} + \dots\right) \rightarrow \omega' = \omega_0 \left(1 - \frac{K^2}{16} + \dots\right) \quad \{ \omega_0 = \left(\frac{a}{2}\right)^{1/2} \}$$

ii) Solve for θ

$$\frac{1}{a}\sin \frac{\theta}{2} = \sin \phi \quad \{ \text{Eq. 5.29} \}$$

$$\sin \frac{\theta}{2} = a \sin \phi$$

$$\frac{\theta}{2} - \frac{\theta^3}{48} \doteq a \sin \phi$$

$$\theta = 2a \sin \phi + \frac{\theta^3}{24}$$

$$\theta^{(1)} = 2a \sin \phi$$

$$\theta^{(2)} = 2a \sin \phi + \frac{(2a \sin \phi)^3}{24}$$

$$= 2a \sin \phi + \frac{a^3}{3} \sin^3 \phi$$

$$\sin^3 \phi = \frac{3 \sin \phi - \sin 3\phi}{4}$$

$$= 2a \sin \phi + \frac{a^3}{3} \left[\frac{3 \sin \phi - \sin 3\phi}{4} \right]$$

$$= 2\left(\frac{K}{2} - \frac{K^3}{48}\right) \sin \phi + \frac{\left(\frac{K}{2} - \frac{K^3}{48}\right)^3}{3} \left[\frac{3 \sin \phi - \sin 3\phi}{4} \right]$$

$$= \left(K - \frac{K^3}{24}\right) \sin \phi + \frac{K^3}{24} \left[\frac{3 \sin \phi - \sin 3\phi}{4} \right] \quad \{ \left(\frac{K}{2} - \frac{K^3}{48}\right)^3 = \frac{K^3}{8} + \text{terms} > K^3 \}$$

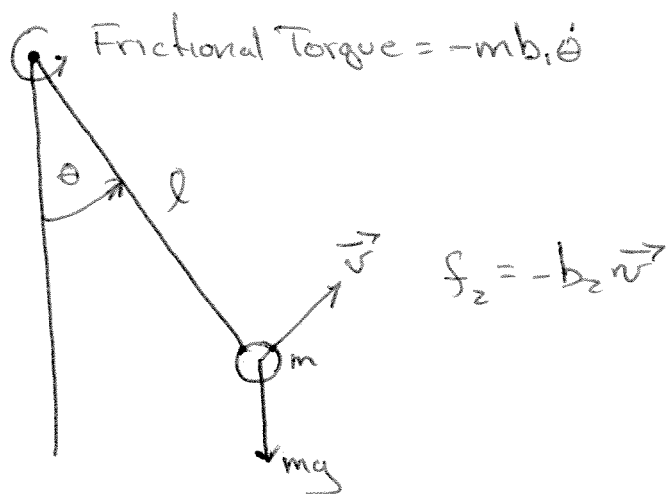
$$= \left(K - \frac{K^3}{24}\right) \sin \phi + \frac{K^3}{32} \sin \phi - \frac{K^3 \sin 3\phi}{96}$$

$$= \left(K - \frac{K^3}{96}\right) \sin \phi - \frac{K^3}{96} \sin 3\phi$$

$$\theta^{(2)} = \left(K - \frac{K^3}{96}\right) \sin \omega' t - \frac{K^3}{96} \sin 3\omega' t$$

Note: equation 5.35 in text is different.

S-10



$$I_z = ml^2$$

$$N_{zg} = -mgl \sin \theta \quad \{ \text{torque due to gravity} \}$$

$$N_{zs_1} = -mb_1 \dot{\theta}$$

$$N_{zs_2} = -b_z \vec{v} l = -b_z l \dot{\theta} l = -b_z l^2 \dot{\theta} \quad \{ v = r\dot{\theta} = l\dot{\theta} \}$$

Equation of motion:

$$\frac{d\vec{L}}{dt} = I_z \ddot{\theta} = \sum N_z$$

$$= N_{zg} + N_{zs_1} + N_{zs_2}$$

$$ml^2 \ddot{\theta} = -mgl \sin \theta - mb_1 \dot{\theta} - b_z l^2 \dot{\theta}$$

$$\ddot{\theta} = -\frac{g}{l} \sin \theta - \frac{b_1}{l^2} \dot{\theta} - \frac{b_z}{m} \dot{\theta}$$

$$= -\frac{g}{l} \theta - \left(\frac{b_1}{l^2} + \frac{b_z}{m} \right) \dot{\theta} \quad \{ \sin \theta \approx \theta \text{ for small } \theta \}$$

$$\ddot{\theta} + \left(\frac{b_1}{l^2} + \frac{b_z}{m} \right) \dot{\theta} + \frac{g}{l} \theta = 0 \quad \theta = A e^{\gamma t}$$

$$\gamma^2 + \gamma \left(\frac{b_1}{l^2} + \frac{b_z}{m} \right) + \frac{g}{l} = 0$$

$$\gamma = \frac{-\left(\frac{b_1}{l^2} + \frac{b_z}{m} \right) \pm \left[\left(\frac{b_1}{l^2} + \frac{b_z}{m} \right)^2 - \frac{4g}{l} \right]^{1/2}}{2}$$

$$\lambda = -\left(\frac{b_1}{2l^2} + \frac{b_2}{2m}\right) \pm \left[\frac{1}{4} \left(\frac{b_1}{l^2} + \frac{b_2}{m} \right)^2 - \frac{g}{l} \right]^{1/2}$$

$$\text{Assume } \frac{g}{l} > \frac{1}{4} \left(\frac{b_1}{l^2} + \frac{b_2}{m} \right)^2$$

$$\lambda = \underbrace{-\left(\frac{b_1}{2l^2} + \frac{b_2}{2m}\right)}_{\text{damping term}} \pm i \underbrace{\left[\frac{g}{l} - \frac{1}{4} \left(\frac{b_1}{l^2} + \frac{b_2}{m} \right)^2 \right]^{1/2}}_{\text{oscillation term}}$$

$$\theta = A e^{-\left(\frac{b_1}{2l^2} + \frac{b_2}{2m}\right)t} \cos(\omega t + \theta_0)$$

$$\omega = \left[\frac{g}{l} - \frac{1}{4} \left(\frac{b_1}{l^2} + \frac{b_2}{m} \right)^2 \right]^{1/2}$$

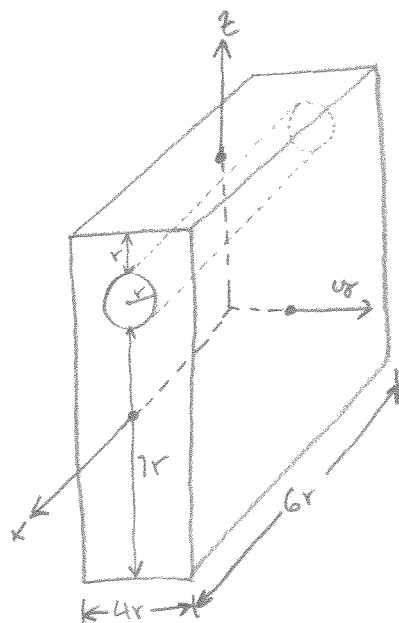
The amplitude A will be $A \cdot \frac{1}{e} = A e^{-1}$ when

$$\left(\frac{b_1}{2l^2} + \frac{b_2}{2m} \right) t = 1$$

$$\left(\frac{2mb_1 + 2l^2b_2}{4ml^2} \right) t = 1$$

$$t = \frac{4ml^2}{2mb_1 + 2l^2b_2}$$

5-17



$$r = 1 \text{ cm}$$

Find I_x , I_y , and I_z about the center of mass.

The x - y - z axes origin is located at the prism geometric center. The parallel axis theorem will be utilized to determine I_x , I_y , and I_z .

First, the moment integrals will be found.

$$dm = \rho dx dy dz$$

$$X = \rho \int_{-5r}^{5r} \int_{-2r}^{2r} \int_{-3r}^{3r} x^2 dx dy dz$$

$$= \rho (10r)(4r) \left. \frac{x^3}{3} \right|_{-3r}^{3r}$$

$$= \rho (10r)(4r) \left[\frac{27r^3}{3} + \frac{27r^3}{3} \right]$$

$$= \rho (10r)(4r)(18r^3)$$

$$X = 720 \rho r^5$$

$$Y = \rho \int_{-5r}^{5r} \int_{-2r}^{2r} \int_{-3r}^{3r} y^2 dy dx dz$$

$$= \rho (10r)(6r) \left. \frac{y^3}{3} \right|_{-2r}^{2r}$$

$$= \rho (10r)(6r) \left[\frac{8r^3}{3} + \frac{8r^3}{3} \right]$$

$$= \rho (10r)(6r) \left(\frac{16r^3}{3} \right)$$

$$Y = 320 \rho r^5$$

$$Z = \rho \int_{-2r}^{2r} \int_{-3r}^{3r} \int_{-5r}^{5r} z^2 dz dx dy$$

$$= \rho (4r)(6r) \left. \frac{z^3}{3} \right|_{-5r}^{5r}$$

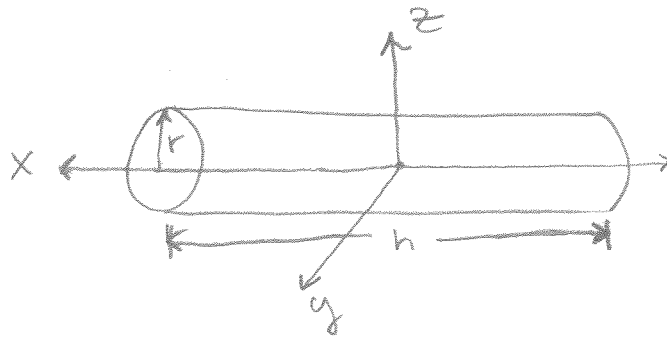
$$= \rho (4r)(6r) \left[\frac{125r^3}{3} + \frac{125r^3}{3} \right]$$

$$= \rho (4r)(6r) \left(\frac{250r^3}{3} \right)$$

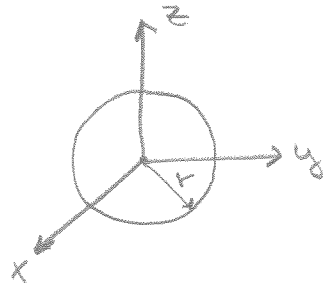
$$Z = 2000 \rho r^5$$

Now, find the moments for a cylinder

②



Begin with a lamina



$$\begin{aligned} I_{x\ell} &= \int r^2 dm \\ &= \rho \int_0^{2\pi} \int_0^r r'^3 dr' d\theta \\ &= 2\pi \rho \frac{r^4}{4} \end{aligned} \quad dm = \rho r' dr' d\theta$$

$$I_{x\ell} = \frac{\pi \rho r^4}{2}$$

$$\begin{aligned} I_{x_{sc}} &= \int_{-h/2}^{h/2} I_{x\ell} dh' \\ &= I_{x\ell} h \end{aligned}$$

$$I_{x_{sc}} = \frac{\pi \rho r^4 h}{2}$$

Using the $\perp$ axis theorem $I_{x\ell}$ and $I_{y\ell}$ can be determined.

$$I_{x\ell} = I_{z\ell} + I_{y\ell}, \quad I_{z\ell} = I_{y\ell} \text{ \{symmetry\}}$$

$$I_{x\ell} = 2 I_{z\ell}$$

$$I_{z\ell} = \frac{1}{2} I_{x\ell}$$

$$I_{zcl} = \frac{\pi \rho r^4}{4} = I_{ycl}$$

Now, using the // axis theorem, I_{zsc} can be found.

$$I = I_c + Mh^2$$

$$I_{zsc} = \int_{-\frac{h}{2}}^{\frac{h}{2}} I_{zcl} dh + \int dm h^2, \quad dm = \rho r' dr' d\theta dh$$

$$= \frac{\rho \pi r^4}{4} \int_{-\frac{h}{2}}^{\frac{h}{2}} dh + \rho \int_{-\frac{h}{2}}^{\frac{h}{2}} \int_0^{2\pi} \int_0^r r' dr' d\theta h^2 dh$$

$$= \frac{\rho \pi r^4 h}{4} + \rho \pi r^2 \left[\frac{h^3}{3} \right]_{-\frac{h}{2}}^{\frac{h}{2}}$$

$$= \frac{\rho \pi r^4 h}{4} + \frac{\rho \pi r^2}{3} \left[\frac{h^3}{8} + \frac{h^3}{8} \right]$$

$$I_{zsc} = \frac{\rho \pi r^4 h}{4} + \frac{\rho \pi r^2 h^3}{12}$$

$$I_{y'sc} = I_{z'sc}$$

$$I_{y'sc} = \frac{\rho \pi r^4 h}{4} + \frac{\rho \pi r^2 h^3}{12}$$

The center of mass is to be found.

$$\bar{x} = \bar{y} = 0 \quad \{ \text{symmetry} \}$$

$$\bar{z} = \frac{1}{M} \int z dm$$

$$= \frac{1}{M} \left[(0r)(\rho)(10r)(4r)(6r) - \underbrace{(3r)(\rho)(\pi r^2)(6r)}_{\text{negative mass}} \right]$$

$$= \frac{-\rho 18 \pi r^4}{\rho (240 r^3 - 6 \pi r^3)}$$

$$= \frac{-18 \pi r}{240 - 6 \pi}$$

$$\bar{z} = -0.256 r$$

(4)

The moments for the solid prism are to be found.

$$I_{x_{sp}} = \int r^2 dm \quad r^2 = y^2 + z^2 \quad dm = \rho dx dy dz$$

$$= \rho \iiint (y^2 + z^2) dx dy dz$$

$$= Y + Z$$

$$= 320 \rho r^5 + 2000 \rho r^5$$

$$I_{x_{sp}} = 2320 \rho r^5$$

The // axis theorem is used to find the moment at the center of mass.

$$I_{x_{cm_{sp}}} = I_{x_{sp}} + M(\bar{z})^2$$

$$= 2320 \rho r^5 + 240 \rho r^3 (-.26)^2$$

$$= 2320 \rho r^5 + 16.22 \rho r^5$$

$$I_{x_{cm_{sp}}} = 2336.22 \rho r^5$$

$$I_{x_{cm_{sc}}} = I_{x_{sc}} + \rho \pi r^2 (6r) (3r + .26r)^2$$

$$= \frac{\rho \pi r^4 (6r)}{2} + \rho 6 \pi r^3 (10.63 r^2)$$

$$= 43 \pi r^5 [1 + 2(10.63)]$$

$$= 43 \pi r^5 [22.26]$$

$$I_{x_{cm_{sc}}} = 209.80$$

$$I_x = I_{x_{cm_{sp}}} - I_{x_{cm_{sc}}}$$

$$= (2336.22 - 209.80) \rho r^5$$

$$I_x = 2126 \rho \text{cm}^5 \quad \{r = 1 \text{cm}\}$$

(5)

$$I_{y_{sp}} = \int r^2 dm \quad r^2 = x^2 + z^2, \quad dm = \rho dx dy dz$$

$$= \rho \iiint (x^2 + z^2) dm$$

$$= X + Z$$

$$= 720 \rho r^5 + 2000 \rho r^5$$

$$I_{y_{sp}} = 2720 \rho r^5$$

Using the // axis theorem

$$I_{y_{cm_{sp}}} = I_{y_{sp}} + M(\bar{z})^2$$

$$= 2720 \rho r^5 + 240 r^3 (.26r)^2$$

$$= 2720 \rho r^5 + 16.22 \rho r^5$$

$$I_{y_{cm_{sp}}} = 2736.22 \rho r^5$$

$$I_{y_{cm_{sc}}} = I_{y_{sc}} + M(3r + .26r)^2$$

$$= \frac{\rho \pi r^2 h}{4} + \frac{\rho \pi r^2 h^3}{12} + \rho \pi r^2 h (3.26r)^2$$

$$= \rho \pi r^2 \left(\frac{6r^3}{4} + \frac{(6r)^3}{12} + 6r (3.26r)^2 \right)$$

$$= \rho \pi r^5 \left(\frac{3}{2} + 18 + 63.77 \right)$$

$$I_{y_{cm_{sc}}} = 261.60 \rho r^5$$

$$I_y = I_{y_{cm_{sp}}} - I_{y_{cm_{sc}}}$$

$$= (2736.22 - 261.60) \rho r^5$$

$$\boxed{I_y = 2474 \rho \text{ cm}^5}$$

(6)

$$I_{zsp} = \int r^2 dm \quad r^2 = x^2 + y^2, \quad dm = \rho dx dy dz$$

$$= \rho \iiint (x^2 + y^2) dm$$

$$= X + Y$$

$$= 720 \rho r^5 + 320 \rho r^5$$

$$I_{zsp} = 1040 \rho r^5$$

Using the // axis theorem

$$I_{zcmsp} = I_{zsp} + M(\bar{z})^2$$

$$= 1040 \rho r^5 + 16.22 \rho r^5$$

$$I_{zcmsp} = 1056.22 \rho r^5$$

The cylinder c.m. is along the z-axis

$$I_z = I_{zcmsp} - I_{zsc}$$

$$= 1056.22 \rho r^5 - \rho \pi r^2 \left(\frac{r^2 h}{4} + \frac{h^3}{12} \right)$$

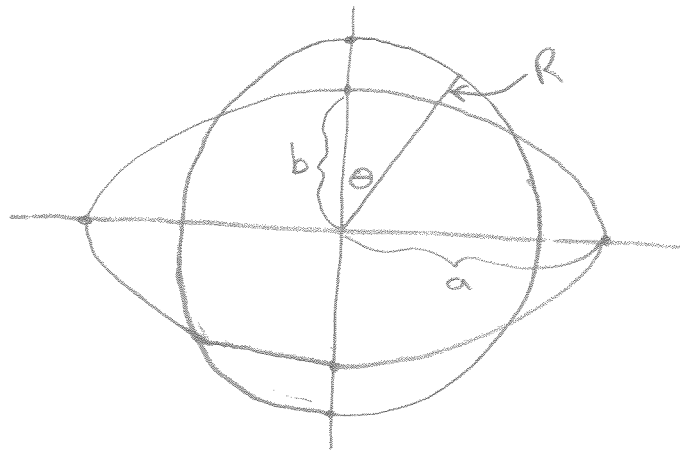
$$= 1056.22 \rho r^5 - \rho \pi r^5 \left(\frac{6}{4} + 18 \right)$$

$$= 1056.22 \rho r^5 - 61.26 \rho r^5$$

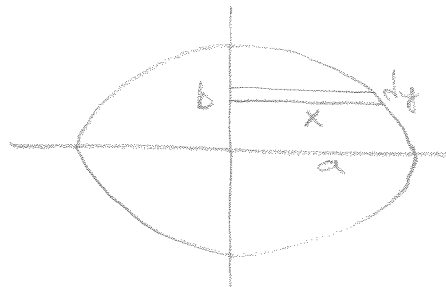
$$\boxed{I_z = 995 \rho cm^5}$$

6-17

a)



Volume of ellipse



$$dV = \pi x^2 dy$$

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$$

$$x^2 = a^2 \left(1 - \frac{y^2}{b^2}\right)$$

$$V = 2\pi a^2 \int_0^b \left(1 - \frac{y^2}{b^2}\right) dy$$

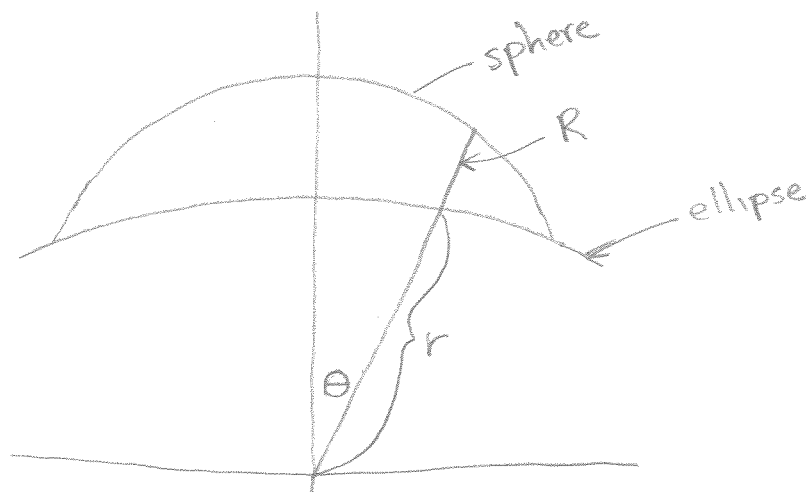
$$= 2\pi a^2 \left(b - \frac{b}{3}\right)$$

$$= \frac{4}{3}\pi a^2 b \quad b = a(1-n)$$

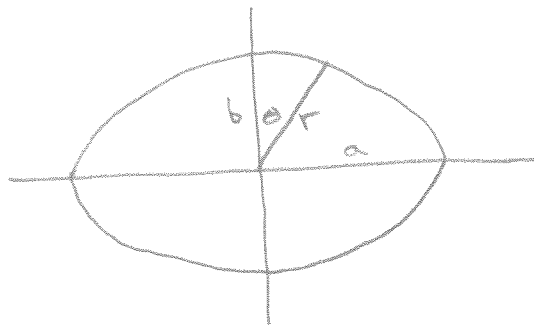
$$V = \frac{4}{3}\pi a^3(1-n)$$

$$\therefore R^3 = a^3(1-n) \quad \{\text{equivalent spherical volume of radius } R\}$$

$$R = a(1-n)^{1/3}$$



Find expression for r to first order m .



$$\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1 \quad \begin{aligned} y &= r \cos \theta \\ x &= r \sin \theta \end{aligned} \quad b = a(1-m)$$

$$b^2 x^2 + a^2 y^2 = a^2 b^2$$

$$a^2(1-m)^2 r^2 \sin^2 \theta + a^2 r^2 \cos^2 \theta = a^4(1-m)^2$$

$$r^2 \left[\sin^2 \theta + \frac{\cos^2 \theta}{(1-m)^2} \right] = a^2$$

$$r^2 [(1 - \cos^2 \theta) + (1-m)^{-2} \cos^2 \theta] = a^2$$

$$r^2 [1 - \cos^2 \theta + (1+2m) \cos^2 \theta] = a^2 \quad \{\text{first order } m\}$$

$$r^2 [1 - \cos^2 \theta + \cos^2 \theta + 2m \cos^2 \theta] = a^2$$

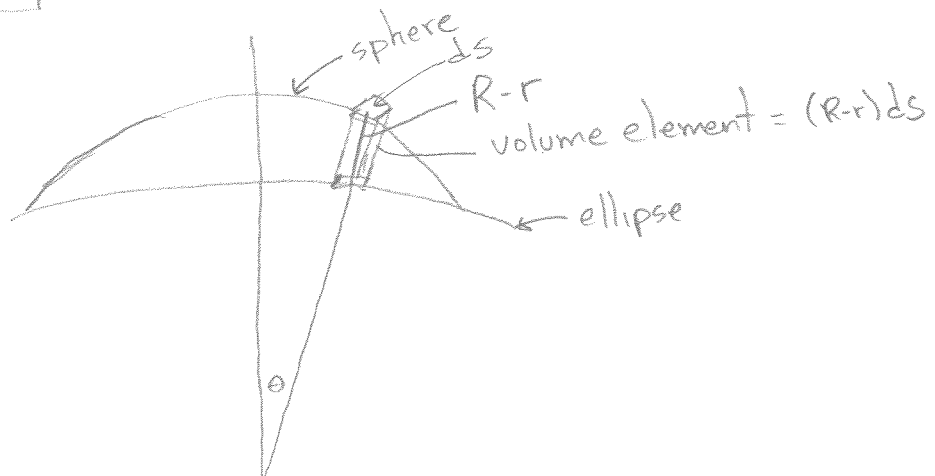
$$r^2 [1 + 2m \cos^2 \theta] = a^2$$

$$r^2 = \frac{a^2}{1 + 2m \cos^2 \theta}$$

$$r = \frac{a}{(1 + 2m \cos^2 \theta)^{1/2}}$$

$$r = a(1 + 2m \cos^2 \theta)^{-1/2}$$

$$\boxed{r = a(1 - m \cos^2 \theta)}$$



$$R-r = a(1-n)^{1/3} - a(1-n\cos^2\theta)$$

$$\approx a(1-\frac{1}{3}n) - a + an\cos^2\theta$$

$$= a - \frac{1}{3}an - a + an\cos^2\theta$$

$$= -\frac{1}{3}an + an\cos^2\theta$$

$$dm = \rho dV$$

$$= \rho(R-r)dS$$

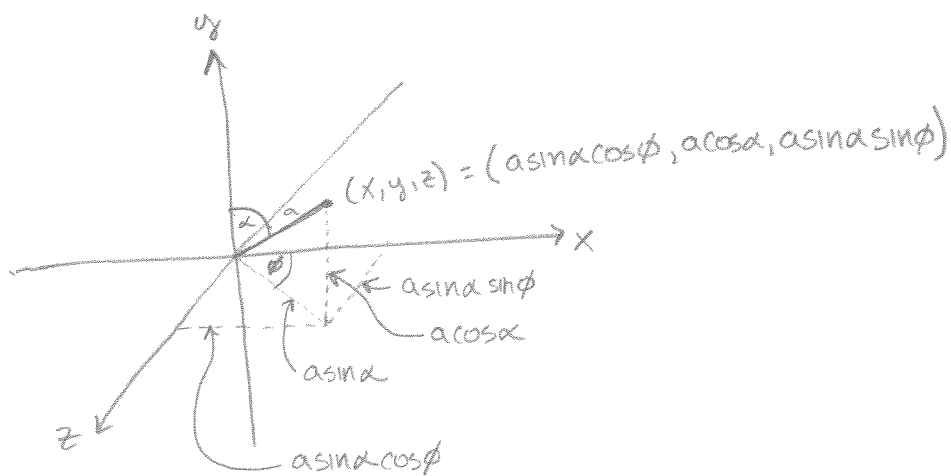
$$\frac{dm}{dS} = \rho(-\frac{1}{3}an + an\cos^2\theta)$$

$$\sigma = \frac{1}{3}\rho a n (3\cos^2\theta - 1)$$

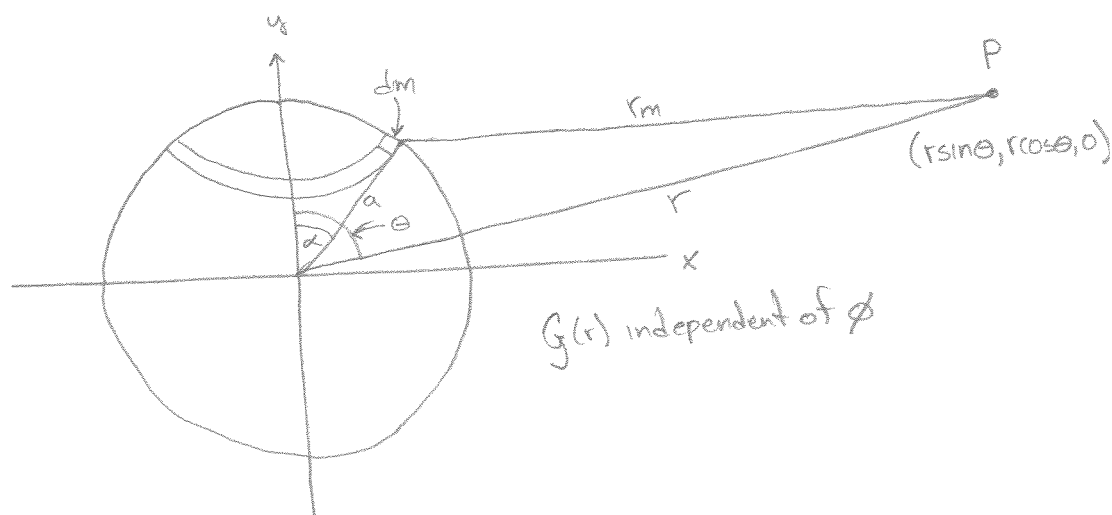
$\therefore$ the surface density to create the ellipsoid is $-\sigma$

$$\boxed{\sigma = \frac{1}{3}\rho a n (1 - 3\cos^2\theta)}$$

b)



$$da = (a \sin \alpha d\phi)(a d\alpha)$$



$$\vec{r}_a = a \sin \alpha \cos \phi \hat{i} + a \cos \alpha \hat{j} + a \sin \alpha \sin \phi \hat{k}$$

$$\vec{r} = r \sin \theta \hat{i} + r \cos \theta \hat{j}$$

$$|\vec{r}_m| = |\vec{r}_a - \vec{r}|$$

$$= [(a \sin \alpha \cos \phi - r \sin \theta)^2 + (a \cos \alpha - r \cos \theta)^2 + a^2 \sin^2 \alpha \sin^2 \phi]^{1/2}$$

$$= [a^2 \sin^2 \alpha \cos^2 \phi + r^2 \sin^2 \theta - 2ar \sin \alpha \cos \phi \sin \theta + a^2 \cos^2 \alpha + r^2 \cos^2 \theta - 2ar \cos \alpha \cos \theta + a^2 \sin^2 \alpha \sin^2 \phi]^{1/2}$$

$$= [r^2 (\sin^2 \theta + \cos^2 \theta) + a^2 \sin^2 \alpha (\cos^2 \phi + \sin^2 \phi) + a^2 \cos^2 \alpha - 2ar (\sin \alpha \cos \phi \sin \theta + \cos \alpha \cos \theta)]^{1/2}$$

$$= [r^2 + a^2 - 2ar (\sin \alpha \cos \phi \sin \theta + \cos \alpha \cos \theta)]^{1/2}$$

$$= [r^2 + a^2 - 2ar f(\alpha, \phi, \theta)]^{1/2}$$

$$(1+b)^n = 1 + nb + \frac{n(n-1)}{2!}b^2 + \frac{n(n-1)(n-2)}{3!}b^3 + \dots$$

$$\frac{1}{|\vec{r}_m|} = \frac{1}{r} \left[1 + \frac{a^2}{r^2} - \frac{2a}{r} f(\alpha, \phi, \theta) \right]^{-1/2}$$

$$b = \frac{a^2}{r^2} - \frac{2a}{r} f(\alpha, \phi, \theta), \quad n = -1/2$$

$$\frac{1}{|\vec{r}_m|} = \frac{1}{r} \left[1 - \frac{1}{2} \left(\frac{a^2}{r^2} - \frac{2a}{r} f(\alpha, \phi, \theta) \right) + \frac{(-1/2)(-3/2)}{2} \left(\frac{a^2}{r^2} - \frac{2a}{r} f(\alpha, \phi, \theta) \right)^2 + \dots \right]$$

$$\frac{1}{|\vec{r}_m|} \doteq \frac{1}{r} \left[1 - \frac{a^2}{2r^2} + \frac{a}{r} f(\alpha, \phi, \theta) + \frac{3}{8} \left[\frac{a^4}{r^4} + \frac{4a^2}{r^2} f^2(\alpha, \phi, \theta) - \frac{4a^3}{r^3} f(\alpha, \phi, \theta) \right] \right]$$

$$dm = \sigma da \quad \sigma = \frac{1}{3} \sigma_0 (1 - 3\cos^2\alpha) \quad da = a \sin\alpha d\phi d\alpha$$

$$= \frac{1}{3} \sigma_0 a^2 \sin\alpha (1 - 3\cos^2\alpha) d\alpha d\phi$$

$$\mathcal{G} = G_{\text{surf}} = \int \frac{G dm}{|\vec{r}_m|}$$

$$\doteq \frac{G \sigma_0 a^3}{3r} \int \sin\alpha (1 - 3\cos^2\alpha) \left[1 - \frac{a^2}{2r^2} + \frac{a}{r} f(\alpha, \phi, \theta) + \frac{3}{8} \left[\frac{4a^2}{r^2} f^2(\alpha, \phi, \theta) \right] \right] \text{ to order } \frac{a^3}{r^3}$$

$$\doteq \frac{2G \sigma_0 a^3}{3r} \int_0^\pi \int_0^\pi (\sin\alpha - 3\cos^2\alpha \sin\alpha) \left[1 - \frac{a^2}{2r^2} + \frac{a}{r} f(\alpha, \phi, \theta) + \frac{3}{2} \frac{a^2}{r^2} f^2(\alpha, \phi, \theta) \right] d\alpha d\phi$$

$$\begin{aligned} \text{i)} \int_0^\pi (\sin\alpha - 3\cos^2\alpha \sin\alpha) d\alpha &= \int_0^\pi \sin\alpha d\alpha - 3 \int_0^\pi \cos^2\alpha \sin\alpha d\alpha \\ &= -\cos\alpha \Big|_0^\pi + \cos^3\alpha \Big|_0^\pi \\ &= -(-1-1) + (-1-1) \\ &= 0 \end{aligned}$$

$$\text{ii)} \int_0^\pi (\sin\alpha - 3\cos^2\alpha \sin\alpha) f(\alpha, \phi, \theta) d\alpha = \int_0^\pi (\sin\alpha - 3\cos^2\alpha \sin\alpha) (\sin\alpha \cos\phi \sin\theta + \cos\alpha \cos\theta) d\alpha$$

$$= \int_0^\pi (\sin^2\alpha \cos\phi \sin\theta + \sin\alpha \cos\alpha \cos\theta - 3\cos^3\alpha \sin^2\alpha \cos\phi \sin\theta - 3\cos^3\alpha \sin\alpha \cos\theta) d\alpha$$

$$= \int_0^\pi \frac{1}{2}(1+\cos 2\alpha) d\alpha \cos\phi \sin\theta + \int_0^\pi \sin\alpha \cos\alpha d\alpha \cos\theta - 3 \int_0^\pi \cos^3\alpha \sin^2\alpha d\alpha \cos\phi \sin\theta -$$

$$3 \int_0^\pi \cos^3\alpha \sin\alpha d\alpha \cos\theta$$

$$= \left(\frac{\pi}{2} + \frac{1}{4} \sin 2\alpha \Big|_0^\pi \right) \cos\phi \sin\theta + \frac{\sin^2\alpha}{2} \Big|_0^\pi \cos\theta - 3 \int_0^\pi \frac{1}{2}(1+\cos 2\alpha)^{1/2} (1-\cos 2\alpha) d\alpha \cos\phi \sin\theta +$$

$$\cos^4\alpha \Big|_0^\pi \cos\theta$$

$$= \frac{\pi}{2} \cos\phi \sin\theta + 0 - \frac{3}{4} \int_0^\pi (1-\cos^2 2\alpha) d\alpha \cos\phi \sin\theta + 0$$

$$= \frac{\pi}{2} \cos\phi \sin\theta - \frac{3}{4} \int_0^\pi \left(1 - \frac{1}{2}(1+\cos 4\alpha) \right) d\alpha \cos\phi \sin\theta$$

$$= \frac{\pi}{2} \cos\phi \sin\theta - \frac{3}{4} \int_0^\pi \left(\frac{1}{2} - \frac{1}{2} \cos 4\alpha \right) d\alpha \cos\phi \sin\theta$$

$$= \frac{\pi}{2} \cos \phi \sin \theta - \frac{3}{4} \left(\frac{\pi}{2} - \frac{1}{8} \sin^4 \alpha \Big|_0^\pi \right) \cos \phi \sin \theta$$

$$= \frac{\pi}{2} \cos \phi \sin \theta - \frac{3\pi}{8} \cos \phi \sin \theta$$

$$= \left(\frac{\pi}{2} - \frac{3\pi}{8} \right) \cos \phi \sin \theta$$

$$= \frac{\pi}{8} \cos \phi \sin \theta$$

$$\begin{aligned} \text{iii) } \int_0^\pi (\sin \alpha - 3 \cos^3 \alpha \sin \alpha) f^2(\alpha, \phi, \theta) d\alpha &= \int_0^\pi (\sin \alpha - 3 \cos^3 \alpha \sin \alpha) (\sin \alpha \cos \phi \sin \theta + \cos \alpha \cos \theta)^2 d\alpha \\ &= \int_0^\pi (\sin \alpha - 3 \cos^3 \alpha \sin \alpha) (\sin^2 \alpha \cos^2 \phi \sin^2 \theta + \cos^2 \alpha \cos^2 \theta + 2 \sin \alpha \cos \alpha \cos \phi \sin \theta \cos \theta) d\alpha \\ &= \int_0^\pi \sin^3 \alpha \cos^2 \phi \sin^2 \theta d\alpha + \int_0^\pi \cos^5 \alpha \sin \alpha \cos^2 \theta d\alpha + 2 \int_0^\pi \sin^2 \alpha \cos \alpha \cos \phi \sin \theta \cos \theta d\alpha \\ &\quad - 3 \int_0^\pi \sin^3 \alpha \cos^3 \alpha \cos^2 \phi \sin^2 \theta d\alpha - 3 \int_0^\pi \cos^4 \alpha \sin \alpha \cos^2 \theta d\alpha - 6 \int_0^\pi \cos^3 \alpha \sin^2 \alpha \cos \phi \sin \theta \cos \theta d\alpha \\ &= \int_0^\pi \sin \alpha (1 - \cos^2 \alpha) d\alpha \cos^2 \phi \sin^2 \theta - \frac{\cos^3 \alpha}{3} \Big|_0^\pi \cos^2 \theta + 2 \frac{\sin^3 \alpha}{3} \Big|_0^\pi \cos \phi \sin \theta \cos \theta \\ &\quad - 3 \int_0^\pi \sin \alpha (1 - \cos^2 \alpha) \cos^2 \alpha d\alpha \cos^2 \phi \sin^2 \theta + 3 \frac{\cos^5 \alpha}{5} \Big|_0^\pi \cos^2 \theta - 6 \int_0^\pi \cos \alpha (1 - \sin^2 \alpha) \sin^2 \alpha d\alpha \cos \phi \sin \theta \cos \theta \\ &= \int_0^\pi [\sin \alpha - \cos^2 \alpha \sin \alpha] d\alpha \cos^2 \phi \sin^2 \theta - \left(-\frac{1}{3} - \frac{1}{3} \right) \cos^2 \theta + 0 - 3 \int_0^\pi [\cos^3 \alpha \sin \alpha - \cos^5 \alpha \sin \alpha] d\alpha \cos^2 \phi \sin^2 \theta \\ &\quad + \frac{3}{5} (-1 - 1) \cos^2 \theta - 6 \int_0^\pi [\sin^2 \alpha \cos \alpha - \sin^4 \alpha \cos \alpha] d\alpha \cos \phi \sin \theta \cos \theta \\ &= \left[-\cos \alpha \Big|_0^\pi + \frac{\cos^3 \alpha}{3} \Big|_0^\pi \right] \cos^2 \phi \sin^2 \theta + \frac{2}{3} \cos^2 \theta - 3 \left[\frac{-\cos^3 \alpha}{3} \Big|_0^\pi + \frac{\cos^5 \alpha}{5} \Big|_0^\pi \right] \cos^2 \phi \sin^2 \theta \\ &\quad - \frac{6}{5} \cos^2 \theta - 6 \left[\frac{\sin^3 \alpha}{3} \Big|_0^\pi - \frac{\sin^5 \alpha}{5} \Big|_0^\pi \right] \cos \phi \sin \theta \cos \theta \\ &= \left[-(-1 - 1) + \left(-\frac{1}{3} - \frac{1}{3} \right) \right] \cos^2 \phi \sin^2 \theta + \frac{2}{3} \cos^2 \theta - 3 \left[\frac{-(-1 - 1)}{3} + \left(-\frac{1}{5} - \frac{1}{5} \right) \right] \cos^2 \phi \sin^2 \theta \\ &\quad - \frac{6}{5} \cos^2 \theta - 0 \\ &= \left[2 - \frac{2}{3} \right] \cos^2 \phi \sin^2 \theta + \frac{2}{3} \cos^2 \theta - 3 \left[\frac{2}{3} - \frac{2}{5} \right] \cos^2 \phi \sin^2 \theta - \frac{6}{5} \cos^2 \theta \\ &= \frac{4}{3} \cos^2 \phi \sin^2 \theta + \frac{2}{3} \cos^2 \theta - 3 \left[\frac{4}{15} \right] \cos^2 \phi \sin^2 \theta - \frac{6}{5} \cos^2 \theta \\ &= \left[\frac{4}{3} - \frac{12}{15} \right] \cos^2 \phi \sin^2 \theta + \left[\frac{2}{3} - \frac{6}{5} \right] \cos^2 \theta \\ &= \frac{8}{15} \cos^2 \phi \sin^2 \theta - \frac{8}{15} \cos^2 \theta \end{aligned}$$

$$G_{\text{surf}} = \frac{2Gma^3}{3r} \int_0^\pi \left[\frac{a}{r} \frac{\pi}{8} \cos\phi \sin\theta + \frac{3a^2}{2r^2} \left[\frac{8}{15} \cos^2\phi \sin^2\theta - \frac{8}{15} \cos^2\theta \right] \right] d\phi$$

$$\int_0^\pi \cos\phi d\phi \sin\theta = \sin\phi \Big|_0^\pi \sin\theta = 0$$

$$\int_0^\pi \cos^2\phi d\phi \sin^2\theta = \frac{1}{2} \int_0^\pi (1 + \cos 2\phi) d\phi \sin^2\theta = \left[\frac{\phi}{2} + \frac{1}{2} \sin 2\phi \Big|_0^\pi \right] \sin^2\theta = \frac{\pi}{2} \sin^2\theta$$

$$G_{\text{surf}} = \frac{2Gma^3}{3r} \left[\frac{3a^2}{2r^2} \left[\frac{8}{15} \frac{\pi}{2} \sin^2\theta - \frac{8}{15} \cos^2\theta \cdot \pi \right] \right]$$

$$= \frac{4\pi a^3 G m a^2}{3r^3} \left[\frac{1}{5} \sin^2\theta - \frac{2}{5} \cos^2\theta \right]$$

$$= \frac{MGma^2}{r^3} \left[\frac{1}{5} (1 - \cos^2\theta) - \frac{2}{5} \cos^2\theta \right] \quad \{ a = R, \text{ radius of shell} \}$$

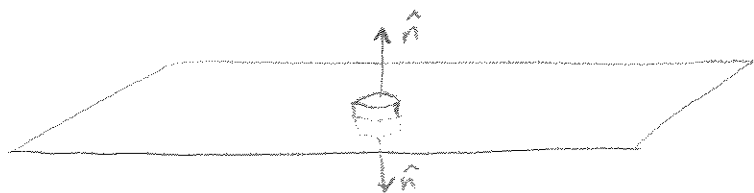
$$= \frac{MGma^2}{r^3} \left[\frac{1}{5} + \left(-\frac{1}{5} - \frac{2}{5} \right) \cos^2\theta \right]$$

$$= \frac{MGma^2}{r^3} \left[\frac{1}{5} - \frac{3}{5} \cos^2\theta \right]$$

$$G_{\text{surf}} = \frac{1}{5} \pi \frac{MGa^2}{r^3} [1 - 3\cos^2\theta]$$

$$\boxed{dG = \frac{1}{5} \pi \frac{MGa^2}{r^3} [1 - 3\cos^2\theta]}$$

6-19



$$\begin{aligned}
 \text{a) } \iint \hat{n} \cdot \vec{g} dS &= -4\pi G \iint dm \\
 &= -4\pi G \iint \sigma dS \\
 g \iint dS &= -4\pi G \sigma \iint dS \\
 g(2A) &= -4\pi G \sigma A \\
 g &= -2\pi G \sigma
 \end{aligned}$$

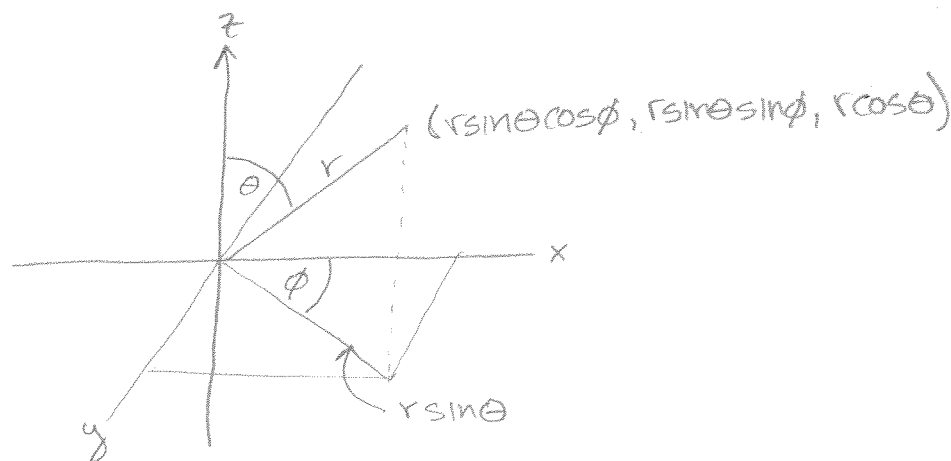


For $r \geq a$ the field behaves as if all the mass were at the center of the shell. At $r = a$,

$$\begin{aligned}
 \iint \hat{n} \cdot \vec{g} dS &= -4\pi G \iint dm \\
 &= -4\pi G \sigma \iint dS \\
 g \iint dS &= -4\pi G \sigma 4\pi a^2 \\
 g 4\pi a^2 &= -4\pi G \sigma 4\pi a^2 \\
 g &= -4\pi G \sigma
 \end{aligned}$$

Half of the field comes from the adjacent matter and half comes from the distant matter of the shell.

6-21
a)



$$\nabla^2 f = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2}$$

In spherical coordinates

$$\nabla^2 f = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 f}{\partial \phi^2}$$

For azimuthal symmetry, $\frac{\partial f}{\partial \phi} = 0$, and Laplace's Equation is $\nabla^2 f = 0$ giving

$$1) \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{\sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial f}{\partial \theta} \right) = 0$$

$$f = \mathcal{G} = \frac{1}{5} \pi M G a^2 \frac{(1 - 3 \cos^2 \theta)}{r^3}$$

$$= K \frac{(1 - 3 \cos^2 \theta)}{r^3}, \quad K = \frac{1}{5} \pi M G a^2$$

$$\frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) = K \frac{\partial}{\partial r} \left(r^2 \frac{\partial}{\partial r} \left(\frac{1 - 3 \cos^2 \theta}{r^3} \right) \right) = K \frac{\partial}{\partial r} \left(\frac{r^2 (-3)(1 - 3 \cos^2 \theta)}{r^4} \right) = K \frac{\partial}{\partial r} \left(\frac{-3(1 - 3 \cos^2 \theta)}{r^2} \right)$$

$$= \frac{-6K(1 - 3 \cos^2 \theta)}{r^3}$$

$$\frac{1}{\sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial f}{\partial \theta} \right) = \frac{K}{\sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial}{\partial \theta} \left(\frac{(1 - 3 \cos^2 \theta)}{r^3} \right) \right) = \frac{K}{r^3 \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta (6 \cos \theta \sin \theta))$$

$$= \frac{6K}{r^3 \sin \theta} \frac{\partial}{\partial \theta} (\sin^2 \theta \cos \theta) = \frac{6K}{r^3 \sin \theta} (-\sin^3 \theta + 2 \sin \theta \cos^2 \theta)$$

$$= \frac{6K}{r^3} (2 \cos^2 \theta - \sin^2 \theta) = \frac{6K}{r^3} (2 \cos^2 \theta - (1 - \cos^2 \theta))$$

$$= \frac{6K}{r^3} (-1 + 3 \cos^2 \theta)$$

$$= -\frac{6K}{r^3} (1 - 3 \cos^2 \theta)$$

Substituting the partial derivative expressions into Eq. 1 gives

$$\frac{GK}{r^3}(1-3\cos^2\theta) - \frac{GK}{r^3}(1-3\cos^2\theta) = 0$$

Therefore, ϕG satisfies Laplace's Equation $\nabla^2 \phi = 0$

b) Poisson's Equation:

$$\nabla^2 G = -4\pi G \rho$$

$$\rho = f(r)(1-3\cos^2\theta)$$

Given a solution of $G = h(r)(1-3\cos^2\theta)$ find $\nabla^2 G$ for azimuthal symmetry

$$\begin{aligned}\nabla^2 G &= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial G}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial G}{\partial \theta} \right) \\&= \frac{1}{r^2} \frac{d}{dr} \left(r^2 \frac{dh}{dr} \right) (1-3\cos^2\theta) + \frac{1}{r^2 \sin \theta} \frac{d}{d\theta} (h \sin \theta (6\cos\theta \sin\theta)) \\&= \frac{1}{r^2} \left(r^2 \frac{d^2 h}{dr^2} + 2r \frac{dh}{dr} \right) (1-3\cos^2\theta) + \frac{6h}{r^2 \sin \theta} \frac{d}{d\theta} (\sin^2 \theta \cos \theta) \\&= \left[\frac{d^2 h}{dr^2} + \frac{2}{r} \frac{dh}{dr} \right] (1-3\cos^2\theta) + \frac{6h}{r^2 \sin \theta} [-\sin^3 \theta + 2\sin \theta \cos^2 \theta] \\&= \left[\frac{d^2 h}{dr^2} + \frac{2}{r} \frac{dh}{dr} \right] (1-3\cos^2\theta) + \frac{6h}{r^2} [2\cos^2 \theta - \sin^2 \theta] \\&= \left[\frac{d^2 h}{dr^2} + \frac{2}{r} \frac{dh}{dr} \right] (1-3\cos^2\theta) + \frac{6h}{r^2} [2\cos^2 \theta - (1-\cos^2 \theta)] \\&= \left[\frac{d^2 h}{dr^2} + \frac{2}{r} \frac{dh}{dr} \right] (1-3\cos^2\theta) + \frac{6h}{r^2} [-1 + 3\cos^2 \theta]\end{aligned}$$

$$\nabla^2 G = \left[\frac{d^2 h}{dr^2} + \frac{2}{r} \frac{dh}{dr} - \frac{6h}{r^2} \right] (1-3\cos^2\theta)$$

$$\nabla^2 G = -4\pi G \rho$$

$$\left[\frac{d^2 h}{dr^2} + \frac{2}{r} \frac{dh}{dr} - \frac{6h}{r^2} \right] (1-3\cos^2\theta) = -4\pi G f(1-3\cos^2\theta)$$

$$\boxed{\frac{d^2 h}{dr^2} + \frac{2}{r} \frac{dh}{dr} - \frac{6h}{r^2} = -4\pi G f}$$

$$c) \quad h = r^{-3}, \quad f = 0$$

$$\frac{d^2}{dr^2}(r^{-3}) + \frac{2}{r} \frac{d}{dr}(r^{-3}) - \frac{6}{r^2}(r^{-3}) =$$

$$\frac{d}{dr}(-3r^{-4}) + \frac{2}{r}(-3r^{-4}) - \frac{6}{r^5} =$$

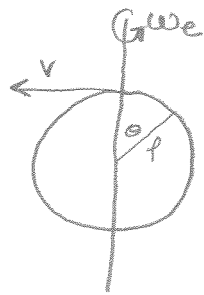
$$\frac{12}{r^5} - \frac{6}{r^5} - \frac{6}{r^5} = 0$$

$\therefore$ when $h(r) = r^{-3}$, Laplace's Equation will be satisfied ($f=0$).

Conclusion:

when $G = Kh(r)(1-3\cos^2\theta)$ where $h(r) = r^{-3}$, Laplace's Equation will be satisfied. Therefore G is valid everywhere outside of the mass distribution ($f = f(r)(1-3\cos^2\theta)$ and $f(r) = 0$).

7-9



$$\omega_e = \frac{2\pi \text{ rad}}{24 \text{ hr}} \cdot \frac{\text{hr}}{3600 \text{ s}} = 7.27 \times 10^{-5} \frac{1}{\text{s}}$$

The equation of motion for a rotating coordinate system is

$$m \frac{d^2 \vec{r}}{dt^2} = \vec{F} + m(\vec{g} - \vec{\omega} \times (\vec{\omega} \times \vec{r})) - 2m\vec{\omega} \times \frac{d\vec{r}}{dt}$$

First, the Coriolis acceleration is found. Using spherical coordinates

$$\frac{d\vec{r}}{dt} = v_r \hat{r} + v_\theta \hat{\theta} + v_\phi \hat{\phi}$$

$$v_r = v_\phi = 0 \quad \{ \text{relative to moving coordinate system} \}$$

$$v_\theta = 500 \frac{\text{mi}}{\text{hr}} \times 5280 \frac{\text{ft}}{\text{mi}} \times \frac{12 \text{ in}}{5 \text{ ft}} \times \frac{0.254 \text{ m}}{1 \text{ in}} \times \frac{\text{hr}}{3600 \text{ s}} = 223.5 \frac{\text{m}}{\text{s}}$$

$$\vec{a}_{\text{cor}} = -2\vec{\omega}_e \times \vec{v}_\theta$$

$$|a_{\text{cor}}| = 2\omega_e v_\theta \quad \{ \vec{\omega}_e \perp \vec{v}_\theta \}$$

$$= 2(7.27 \times 10^{-5} \frac{1}{\text{s}})(223.5 \frac{\text{m}}{\text{s}})$$

$$|a_{\text{cor}}| = 3.25 \times 10^{-2} \frac{\text{m}}{\text{s}^2}$$

Since the moving plumb bob is supported by a string no compressive forces exist in the string. Therefore, a centrifugal force displaces the plumb bob.

$$\vec{a}_{\text{cen}} = \vec{\omega}_p \times (\vec{\omega}_p \times \vec{r}_e)$$

$$= \omega_p^2 r_e \hat{r}$$

$$= \frac{v_p^2}{r_e}$$

$$= 7.86 \times 10^{-3} \frac{\text{m}}{\text{s}^2} \hat{r}$$

$$\omega_p = \frac{v_p}{r_e}, \quad r_e = R_e \text{ at the pole}$$

$$= 6357 \times 10^3 \text{ m}$$

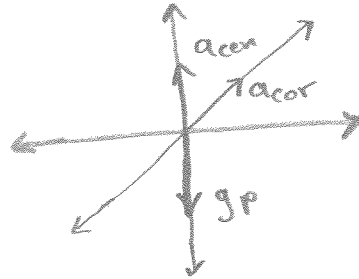
$$= \frac{223.5 \frac{\text{m}}{\text{s}}}{6357 \times 10^3 \text{ m}} = 3.52 \times 10^{-5} \frac{1}{\text{s}}$$

(2)

At the pole the gravitational acceleration is

$$g_p = 9.87 \frac{\text{m}}{\text{s}^2}$$

The accelerations present on the moving plumb bob are



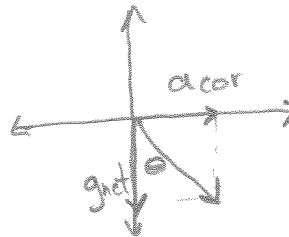
$$g_{\text{net}} = a_{\text{cen}} - g_p$$

$$= 9.86 \frac{\text{m}}{\text{s}^2}$$

$$\theta = \tan^{-1} \left(\frac{a_{\text{cor}}}{g_{\text{net}}} \right)$$

$$= \tan^{-1} \left(\frac{3.75 \times 10^{-2}}{9.86} \right)$$

$$\theta = 3.30 \times 10^{-3} \text{ rad}$$



The plumb bob at rest situated at the pole does not experience a Coriolis force because $\frac{d\vec{r}}{dt} = 0$

Therefore, the angle between the moving plumb bob and the freely hanging one situated at the pole is

$$\boxed{\theta = 3.30 \times 10^{-3} \text{ rad}}$$

Note: answer in text is $5.25 \times 10^{-4} \text{ rad}$

Part 1. $V' = \frac{m(M_1+M_2)G}{a} \left\{ \frac{\xi_2}{[(\xi-\xi_1)^2+n^2]^{1/2}} - \frac{\xi_1}{[(\xi-\xi_2)^2+n^2]^{1/2}} - \frac{1}{2}(\xi^2-n^2) \right\}$

$$\xi_2 = \frac{x}{a}, \quad \xi_1 = \frac{M_2}{M_1+M_2}, \quad \xi_2 = -\frac{M_1}{M_1+M_2} = \xi_1 - 1$$

$$n = \frac{y}{a}$$

$$\begin{aligned} \frac{\partial V'}{\partial \xi} &= \frac{m(M_1+M_2)G}{a} \left\{ -\frac{1}{2}\xi_2 [(\xi-\xi_1)^2+n^2]^{-3/2} 2(\xi-\xi_1) - \frac{1}{2}\xi_1 [(\xi-\xi_2)^2+n^2]^{-3/2} 2(\xi-\xi_2) - \xi \right\} \\ &= \frac{m(M_1+M_2)G}{a} \left\{ -\xi_2(\xi-\xi_1)[(\xi-\xi_1)^2+n^2]^{-3/2} + \xi_1(\xi-\xi_2)[(\xi-\xi_2)^2+n^2]^{-3/2} - \xi \right\} \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 V'}{\partial \xi^2} &= \frac{m(M_1+M_2)G}{a} \left\{ -\xi_2(\xi-\xi_1)(-\frac{3}{2})[(\xi-\xi_1)^2+n^2]^{-5/2} 2(\xi-\xi_1) + [(\xi-\xi_1)^2+n^2]^{-3/2}(-\xi_2) + \right. \\ &\quad \left. \xi_1(\xi-\xi_2)(-\frac{3}{2})[(\xi-\xi_2)^2+n^2]^{-5/2} 2(\xi-\xi_2) + [(\xi-\xi_2)^2+n^2]^{-3/2}(\xi_1) - 1 \right\} \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 V'}{\partial \xi^2} &= \frac{m(M_1+M_2)G}{a} \left\{ 3\xi_2(\xi-\xi_1)^2[(\xi-\xi_1)^2+n^2]^{-5/2} - \xi_2[(\xi-\xi_1)^2+n^2]^{-3/2} - \right. \\ &\quad \left. 3\xi_1(\xi-\xi_2)^2[(\xi-\xi_2)^2+n^2]^{-5/2} + \xi_1[(\xi-\xi_2)^2+n^2]^{-3/2} - 1 \right\} \end{aligned}$$

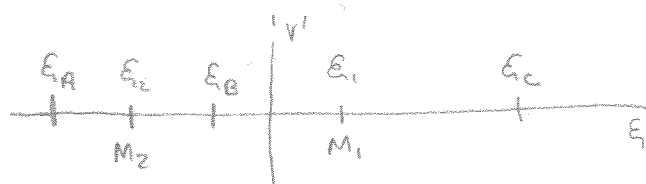
$$\begin{aligned} \frac{\partial V'}{\partial n} &= \frac{m(M_1+M_2)G}{a} \left\{ -\frac{1}{2}\xi_2 [(\xi-\xi_1)^2+n^2]^{-1/2} 2n - \frac{1}{2}\xi_1 [(\xi-\xi_2)^2+n^2]^{-1/2} 2n + n \right\} \\ &= \frac{m(M_1+M_2)G}{a} \left\{ -\xi_2 n [(\xi-\xi_1)^2+n^2]^{-1/2} + \xi_1 n [(\xi-\xi_2)^2+n^2]^{-1/2} + n \right\} \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 V'}{\partial n^2} &= \frac{m(M_1+M_2)G}{a} \left\{ -\xi_2 n(-\frac{1}{2})[(\xi-\xi_1)^2+n^2]^{-3/2} 2n - \xi_2 [(\xi-\xi_1)^2+n^2]^{-1/2} + \right. \\ &\quad \left. \xi_1 n(-\frac{1}{2})[(\xi-\xi_2)^2+n^2]^{-3/2} 2n + \xi_1 [(\xi-\xi_2)^2+n^2]^{-1/2} + 1 \right\} \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 V'}{\partial n^2} &= \frac{m(M_1+M_2)G}{a} \left\{ 3\xi_2 n^2 [(\xi-\xi_1)^2+n^2]^{-3/2} - \xi_2 [(\xi-\xi_1)^2+n^2]^{-1/2} - \right. \\ &\quad \left. 3\xi_1 n^2 [(\xi-\xi_2)^2+n^2]^{-3/2} + \xi_1 [(\xi-\xi_2)^2+n^2]^{-1/2} + 1 \right\} \end{aligned}$$

$$\frac{\partial}{\partial \xi} \frac{\partial V'}{\partial n} = \frac{m(M_1+M_2)G}{a} \left\{ -\xi_2 n(-\frac{1}{2})[(\xi-\xi_1)^2+n^2]^{-3/2} 2(\xi-\xi_1) + \xi_1 n(-\frac{1}{2})[(\xi-\xi_2)^2+n^2]^{-3/2} 2(\xi-\xi_2) \right\}$$

$$\xi_A < \xi_2 < \xi_B < 0 < \xi_1 < \xi_C$$



$$\text{Let } K = \frac{m(M_1 + M_2)G}{a}, m=0, \xi_L = \xi_{A,B,C}, \xi_z = \xi_i - 1$$

$$\frac{d^2 V'}{d\xi^2} = K \left\{ \frac{3\xi_z(\xi_L - \xi_i)^2}{|\xi_L - \xi_i|^5} - \frac{3\xi_i(\xi_L - \xi_z)^2}{|\xi_L - \xi_z|^5} - \frac{\xi_z}{|\xi_L - \xi_i|^3} + \frac{\xi_i}{|\xi_L - \xi_z|^3} - 1 \right\}$$

$$\frac{(\xi_L - \xi_i)^2}{|\xi_L - \xi_i|^5} = \frac{[(\xi_L - \xi_i)^2]'}{[(\xi_L - \xi_i)^2]^{5/2}} = [(\xi_L - \xi_i)^2]^{-3/2} = \frac{1}{|\xi_L - \xi_i|^3}$$

$$\begin{aligned} \frac{d^2 V'}{d\xi^2} &= K \left\{ \frac{3\xi_z}{|\xi_L - \xi_i|^3} - \frac{3\xi_i}{|\xi_L - \xi_z|^3} - \frac{\xi_z}{|\xi_L - \xi_i|^3} + \frac{\xi_i}{|\xi_L - \xi_z|^3} - 1 \right\} \\ &= K \left\{ \frac{2\xi_z}{|\xi_L - \xi_i|^3} - \frac{2\xi_i}{|\xi_L - \xi_z|^3} - 1 \right\} \end{aligned}$$

Since $\xi_z < 0$ and $\xi_i > 0$ it follows that each term is always less than zero.

So,

$$\boxed{\frac{d^2 V'}{d\xi^2} < 0}$$

$$\frac{d^2 V'}{dm^2} = K \left\{ \frac{-\xi_z}{|\xi_L - \xi_i|^3} + \frac{\xi_i}{|\xi_L - \xi_z|^3} + 1 \right\}$$

Since $\xi_z < 0$ and $\xi_i > 0$ it follows that each term is always greater than zero.

So,

$$\boxed{\frac{d^2 V'}{dm^2} > 0}$$

$$\frac{d^2 V'}{d\xi dm} = K \{0\} \quad \{m=0 \text{ at points A, B, and C}\}$$

$$\boxed{\frac{d^2 V'}{d\xi dm} = 0}$$

Part 2.

Equations of motion for m :

$$\ddot{x} - 2\omega \dot{y} = - \frac{M_1 G (x - x_1)}{[(x - x_1)^2 + y^2]^{3/2}} - \frac{M_2 G (x - x_2)}{[(x - x_2)^2 + y^2]^{3/2}} + \frac{(M_1 + M_2) G x}{a^3}$$

$$\ddot{y} + 2\omega \dot{x} = - \frac{M_1 G y}{[(x - x_1)^2 + y^2]^{3/2}} - \frac{M_2 G y}{[(x - x_2)^2 + y^2]^{3/2}} + \frac{(M_1 + M_2) G y}{a^3}$$

Since a conservative force exists

$$\ddot{x} - 2\omega \dot{y} = - \frac{dV'}{dx}$$

$$\ddot{y} + 2\omega \dot{x} = - \frac{dV'}{dy}$$

where

$$V' = - \frac{M_1 G}{[(x - x_1)^2 + y^2]^{1/2}} - \frac{M_2 G}{[(x - x_2)^2 + y^2]^{1/2}} - \frac{\omega^2}{2} (x^2 + y^2)$$

It's noteworthy to show a constant of motion exists.

$$\ddot{x} \dot{x} - 2\omega \dot{y} \dot{x} = - \dot{x} \frac{dV'}{dx}$$

$$\ddot{y} \dot{y} + 2\omega \dot{y} \dot{x} = - \dot{y} \frac{dV'}{dy}$$

Summing these two equations gives

$$\ddot{x} \dot{x} + -2\omega \dot{y} \dot{x} + \ddot{y} \dot{y} + 2\omega \dot{y} \dot{x} = - \dot{x} \frac{dV'}{dx} - \dot{y} \frac{dV'}{dy}$$

$$\begin{aligned} \ddot{x} \dot{x} + \ddot{y} \dot{y} &= - \frac{dx}{dt} \frac{dV'}{dx} - \frac{dy}{dt} \frac{dV'}{dy} \\ &= - \frac{dV'}{dt} \end{aligned}$$

$$\frac{d}{dt} \left[\frac{1}{2} (\dot{x}^2 + \dot{y}^2) \right] = - \frac{dV'}{dt}$$

$$\frac{d}{dt} \left[\frac{1}{2} (\dot{x}^2 + \dot{y}^2) + V' \right] = 0$$

$$\frac{d}{dt} E' = 0 \quad \{ E' = \frac{1}{2} (\dot{x}^2 + \dot{y}^2) + V' \}$$

Therefore, the total energy, E , in the moving coordinate system is a constant of the motion.

The Taylor expansion is about a point $(\xi_{AB}, 0)$

$$V'(\xi, \eta) \approx V'(\xi_{AB}, 0) + V'_{\xi}(\xi_{AB}, 0) + V'_{\eta}(\xi_{AB}, 0) + \frac{1}{2} V'_{\xi\xi}(\xi_{AB}, 0) (\xi - \xi_{AB})^2 + \frac{1}{2} V'_{\xi\eta}(\xi_{AB}, 0) (\xi - \xi_{AB})(\eta) + \frac{1}{2} V'_{\eta\eta}(\xi_{AB}, 0) (\eta)^2$$

The equations of motion can be rewritten using the substitutions

$$\xi = \frac{x}{a}, \quad \eta = \frac{y}{a}, \quad \xi_1 = \frac{x_1}{a} = \frac{M_2}{M_1 + M_2}, \quad \xi_2 = \frac{x_2}{a} = -\frac{M_1}{M_1 + M_2}$$

$$\ddot{x} - 2\omega \dot{y} = -\frac{\partial V'}{\partial x} \rightarrow \ddot{\xi} a - 2\omega \dot{\eta} a = -\frac{\partial V'}{\partial \xi} a$$

$$\ddot{y} + 2\omega \dot{x} = -\frac{\partial V'}{\partial y} \rightarrow \ddot{\eta} a - 2\omega \dot{\xi} a = -\frac{\partial V'}{\partial \eta} a$$

Giving

$$\ddot{\xi} - 2\omega \dot{\eta} = -\frac{\partial V'}{\partial \xi}$$

$$\ddot{\eta} + 2\omega \dot{\xi} = -\frac{\partial V'}{\partial \eta}$$

$$\text{Define } V'_{\xi\xi} = \frac{\partial^2 V'}{\partial \xi^2}(\xi_{AB}, 0) \text{ and } V'_{\eta\eta} = \frac{\partial^2 V'}{\partial \eta^2}(\xi_{AB}, 0).$$

Also,

$$V'_{\xi}(\xi_{AB}, 0) = V'_{\eta}(\xi_{AB}, 0) = V'_{\xi\eta}(\xi_{AB}, 0) = 0$$

So, the expanded $V'(\xi, \eta)$ first derivative is

$$\frac{\partial V'}{\partial \xi} = V'_{\xi\xi}(\xi - \xi_{AB}) = V'_{\xi\xi}(\xi'), \quad \frac{\partial V'}{\partial \eta} = V'_{\eta\eta}(\eta)$$

Now, the equations of motion are

$$\ddot{\xi} - 2\omega \dot{\eta} = -V'_{\xi\xi}(\xi') \rightarrow \ddot{\xi} - 2\omega \dot{\eta} + V'_{\xi\xi}(\xi') = 0$$

$$\ddot{\eta} + 2\omega \dot{\xi} = -V'_{\eta\eta}(\eta) \rightarrow \ddot{\eta} + 2\omega \dot{\xi} + V'_{\eta\eta}(\eta) = 0$$

$$\xi' = \xi - \xi_{AB}$$

$$\dot{\xi}' = \dot{\xi}, \quad \ddot{\xi}' = \ddot{\xi}$$

$$\ddot{\xi}' - 2\omega \dot{\eta}' + {}^1V'_{\xi\xi} \xi' = 0$$

$$\dot{\eta}' + 2\omega \xi' + {}^1V'_{\eta\eta} \eta' = 0$$

Let

$$\xi' = C_1 e^{pt}, \eta' = C_2 e^{pt}$$

$$C_1 p^2 - 2\omega C_2 p + C_1 {}^1V'_{\xi\xi} = 0 \rightarrow C_1 (p^2 + {}^1V'_{\xi\xi}) = 2\omega C_2 p$$

$$C_2 p^2 + 2\omega C_1 p + C_2 {}^1V'_{\eta\eta} = 0 \rightarrow C_2 (p^2 + {}^1V'_{\eta\eta}) = -2\omega C_1 p$$

$$\frac{C_2}{C_1} = \frac{p^2 + {}^1V'_{\xi\xi}}{2\omega p}, \quad \frac{C_2}{C_1} = \frac{-2\omega p}{p^2 + {}^1V'_{\eta\eta}}$$

$$\frac{p^2 + {}^1V'_{\xi\xi}}{2\omega p} = \frac{-2\omega p}{p^2 + {}^1V'_{\eta\eta}}$$

$$(p^2 + {}^1V'_{\xi\xi})(p^2 + {}^1V'_{\eta\eta}) = -4\omega^2 p^2$$

$$p^4 + p^2({}^1V'_{\xi\xi} + {}^1V'_{\eta\eta} + 4\omega^2) + {}^1V'_{\xi\xi} {}^1V'_{\eta\eta} = 0$$

Let $\lambda = p^2$

$$\lambda^2 + \lambda({}^1V'_{\xi\xi} + {}^1V'_{\eta\eta} + 4\omega^2) + {}^1V'_{\xi\xi} {}^1V'_{\eta\eta} = 0$$

Since the solution for p must be imaginary for stability then λ must have real negative roots.

Let

$$A = \frac{\xi_1}{p_2^3} - \frac{\xi_2}{p_1^3}$$

$$p_1^2 = (\xi - \xi_1)^2 + \eta^2, \quad p_2^2 = (\xi - \xi_2)^2 + \eta^2$$

$$B = 3 \left[\frac{\xi_2 (\xi - \xi_1)^2}{p_1^5} - \frac{\xi_1 (\xi - \xi_2)^2}{p_2^5} \right]$$

$$C = 3 \left[\frac{\xi_2}{p_1^5} - \frac{\xi_1}{p_2^5} \right] \eta^2$$

Then since

$$V'_{EE} = 2K \left\{ \frac{E_2}{P_1^3} - \frac{E_1}{P_2^3} - 1 \right\}$$

it follows that

$$V'_{EE} = -2A - 1$$

Also,

$$V'_{nn} = K \left\{ \frac{-E_2}{P_1^3} + \frac{E_1}{P_2^3} + 1 \right\}$$

$$V'_{nn} = A - 1$$

Now we have

$$\lambda^2 + \lambda(-2A - 1 + A - 1 + 4) + (1 - A)(2A + 1) = 0 \quad \{\omega = 1\}$$

$$\lambda^2 + \lambda(2 - A) + (1 - A)(2A + 1) = 0$$

$$\lambda = \frac{A - 2 \pm \sqrt{(2 - A)^2 - 4(1 - A)(2A + 1)}}{2}$$

$$= \frac{A - 2 \pm \sqrt{4 - 4A + A^2 - 4(2A + 1 - 2A^2 - A)}}{2}$$

$$= \frac{A - 2 \pm \sqrt{4 - 4A + A^2 - 8A - 4 + 8A^2 + 4A}}{2}$$

$$= \frac{A - 2 \pm \sqrt{9A^2 - 8A}}{2}$$

$$\lambda = \frac{A - 2 \pm \sqrt{A(9A - 8)}}{2}$$

$$A - 2 + \sqrt{A(9A - 8)} \leq 0 \quad \text{and} \quad A - 2 - \sqrt{A(9A - 8)} \leq 0$$

$$A - 2 \leq -\sqrt{A(9A - 8)} \quad \text{and} \quad A - 2 \leq \sqrt{A(9A - 8)}$$

$$A^2 - 4A + 4 \leq 9A^2 - 8A$$

$$-8A^2 + 4A + 4 \leq 0$$

$$-4(2A^2 - A - 1) \leq 0$$

$$2A^2 - A - 1 \leq 0$$

$$(2A + 1)(A - 1) \leq 0$$

$$A \leq 1$$

The discriminant must be greater than zero

$$9A^2 - 8A \geq 0$$

$$9A^2 \geq 8A$$

$$A \geq \frac{8}{9}$$

Therefore,

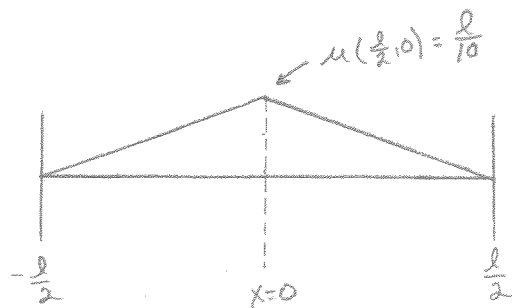
$$\frac{8}{9} \leq A \leq 1$$

$$\frac{8}{9} \leq \frac{\epsilon_1}{p_2^3} - \frac{\epsilon_2}{p_1^3} \leq 1$$

$$\frac{8}{9} \leq \frac{\epsilon_1}{|\epsilon_{A,B} - \epsilon_2|^3} - \frac{\epsilon_2}{|\epsilon_{A,B} - \epsilon_1|^3} \leq 1$$

$$\frac{8}{9} \leq \frac{\epsilon_1}{|\epsilon_{A,B} - \epsilon_1 + 1|^3} - \frac{\epsilon_1 - 1}{|\epsilon_{A,B} - \epsilon_1|^3} \leq 1$$

8-11



$$u(x,t) = f(x-ct) + g(x+ct) \\ = f(\xi) + g(\eta), \quad \xi = x-ct, \quad \eta = x+ct$$

$$u(x,0) = u_0(x) = \begin{cases} 0, & |x| > \frac{l}{2} \\ \frac{l}{10}(1 + \frac{2x}{l}), & -\frac{l}{2} \leq x \leq 0 \\ \frac{l}{10}(1 - \frac{2x}{l}), & 0 \leq x \leq \frac{l}{2} \end{cases}$$

$$1) \quad f(x) + g(x) = u_0(x) \\ -c \frac{df}{d\xi} + c \frac{dg}{d\eta} = v_0(x) = 0$$

$$2) \quad f(x) = g(x) + C$$

Substituting 2) into 1) gives

$$2g(x) + C = u_0(x) \\ g(x) = \frac{1}{2} u_0(x) - \frac{C}{2}$$

Solving for $g(x)$ in 2) and substituting into 1) gives

$$2f(x) - C = u_0(x) \\ f(x) = \frac{1}{2} u_0(x) + \frac{C}{2}$$

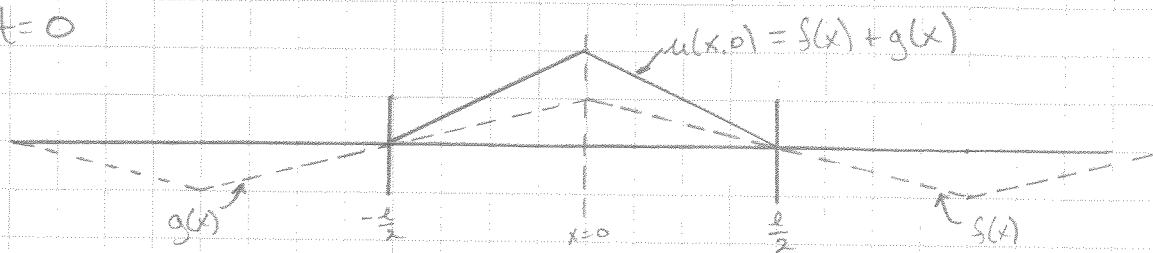
$$u(x,t) = f(x-ct) + g(x+ct)$$

$$u(x,t) = \frac{1}{2} u_0(x-ct) + \frac{1}{2} u_0(x+ct)$$

Thus, $u(x,t)$ represents two triangular waveforms, one traveling to the right and one traveling to the left.

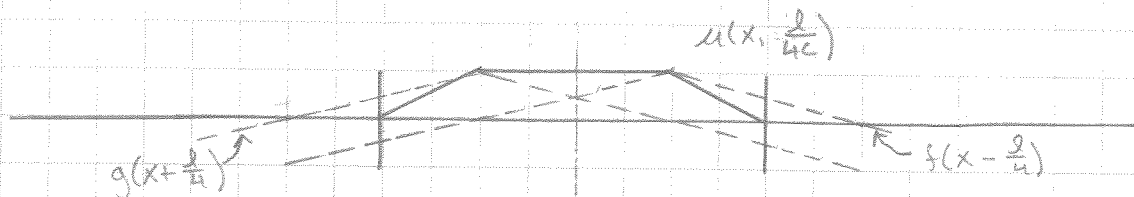
$$u(x,t) = \frac{l}{20} \left(1 - \frac{2(x-ct)}{l}\right)_{0 \leq x-ct \leq \frac{l}{2}} + \frac{l}{20} \left(1 + \frac{2(x+ct)}{l}\right)_{-\frac{l}{2} \leq x+ct \leq 0}$$

At $t=0$

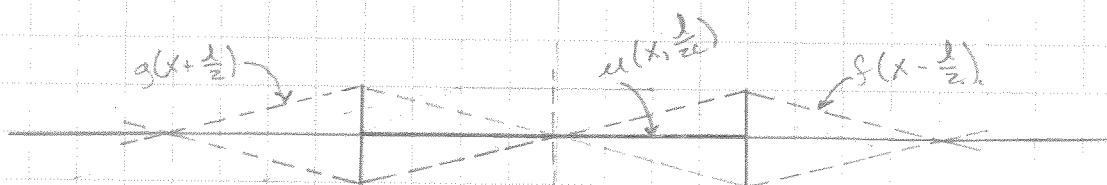


$$T = \frac{T}{c} = \frac{2l}{c}$$

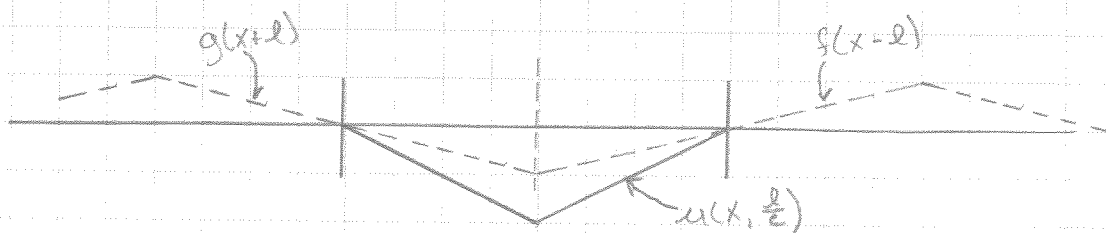
At $t = \frac{1}{4} \frac{l}{c}$ each waveform has shifted $\frac{l}{4}$ from $x=0$



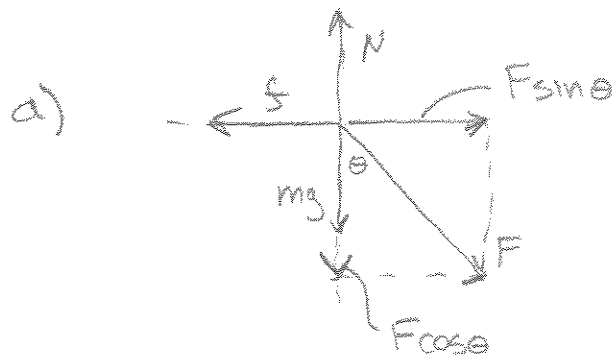
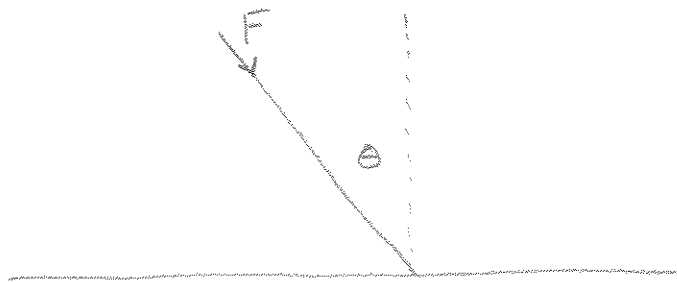
At $t = \frac{1}{2} \frac{l}{c}$ each waveform has shifted $\frac{l}{2}$ from $x=0$



At $t = \frac{l}{c}$ each waveform has shifted l from $x=0$



1-7



$$b) \quad V_x = 0 \rightarrow a_x = 0 \rightarrow \sum F_x = 0$$

$$0 = F \sin \theta - f \quad f = \mu N \quad N = F \cos \theta + mg$$

$$= \mu F \cos \theta + \mu mg$$

$$F \sin \theta = f$$

$$= \mu F \cos \theta + \mu mg$$

$$F(\sin \theta - \mu \cos \theta) = \mu mg$$

$$F = \frac{\mu mg}{\sin \theta - \mu \cos \theta}$$

$$c) \quad \tan \theta_r = \mu_s \rightarrow \sin \theta_r = \mu_s \cos \theta_r \quad \cos \theta_r = \frac{\sin \theta_r}{\mu_s}$$

Neglecting mass of map

$$f_s = \mu_s N \quad N = F \cos \theta_r \quad F_x = F \sin \theta_r$$

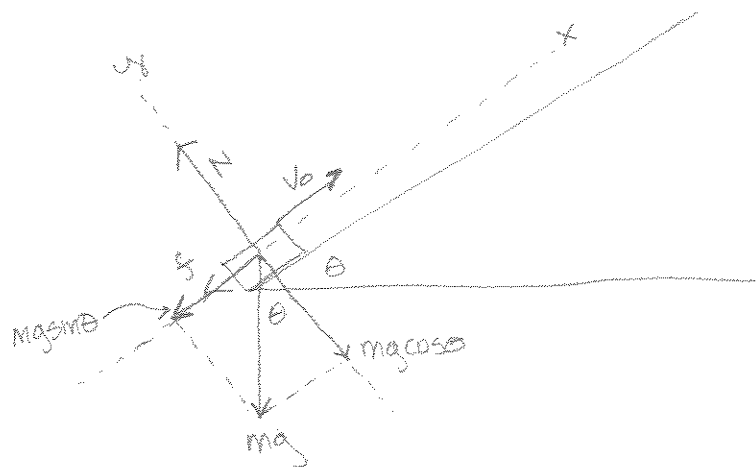
$$= \mu_s F \cos \theta_r \quad = F \mu_s \cos \theta_r$$

$$\sum F_x = F_x - f$$

$$= F \mu_s \cos \theta_r - \mu_s F \cos \theta_r$$

$$\sum F_x = 0$$

1-9



$$ma = -mg \sin \theta - f \quad f = \mu N$$

$$ma = -mg \sin \theta - \mu mg \cos \theta \quad = -\mu mg \cos \theta$$

Distance up ramp:

$$V^2 = V_0^2 + 2a(x - x_0)$$

$$0 = V_0^2 + 2a(x - x_0)$$

$$x - x_0 = \frac{V_0^2}{-2a}$$

$$x - x_0 = \frac{V_0^2}{2g(\sin \theta + \mu \cos \theta)}$$

Time up ramp:

$$x - x_0 = V_0 t + \frac{1}{2} a t^2$$

$$0 = -(x - x_0) + V_0 t + \frac{1}{2} a t^2$$

$$a t^2 + 2V_0 t - 2(x - x_0) = 0$$

$$-g(\sin \theta + \mu \cos \theta) t^2 + 2V_0 t - \frac{V_0^2}{g(\sin \theta + \mu \cos \theta)} = 0$$

$$g(\sin\theta + \mu\cos\theta)t^2 - 2v_0t + \frac{v_0^2}{g(\sin\theta + \mu\cos\theta)} = 0$$

$$g^2(\sin\theta + \mu\cos\theta)^2 t^2 - 2gv_0(\sin\theta + \mu\cos\theta) + v_0^2 = 0$$

$$t_u = \frac{2gv_0(\sin\theta + \mu\cos\theta) \pm \sqrt{4g^2v_0^2(\sin\theta + \mu\cos\theta)^2 - 4g^2v_0^2(\sin\theta + \mu\cos\theta)^2}}{2g^2(\sin\theta + \mu\cos\theta)^2}$$

$$t_u = \frac{v_0}{g}(\sin\theta + \mu\cos\theta)^{-1}$$

Time down the ramp

$$\sum F_x = -mg\sin\theta + f$$

$$ma = -mg\sin\theta + \mu mg\cos\theta$$

$$a = -g\sin\theta + \mu g\cos\theta$$

$$x_0 = \frac{v_0^2}{2g(\sin\theta + \mu\cos\theta)}$$

$$x = x_0 + v_0t + \frac{1}{2}at^2$$

$$0 = x_0 + v_0t + \frac{1}{2}at^2$$

$$at^2 + 2v_0t + 2x_0 = 0 \quad v_0 = 0$$

$$-g(\sin\theta - \mu\cos\theta)t^2 + \frac{v_0^2}{g(\sin\theta + \mu\cos\theta)} = 0$$

$$-g(\sin\theta - \mu\cos\theta)t^2 = \frac{-v_0^2}{g(\sin\theta + \mu\cos\theta)}$$

$$t^2 = \frac{v_0^2}{g^2(\sin\theta - \mu\cos\theta)(\sin\theta + \mu\cos\theta)}$$

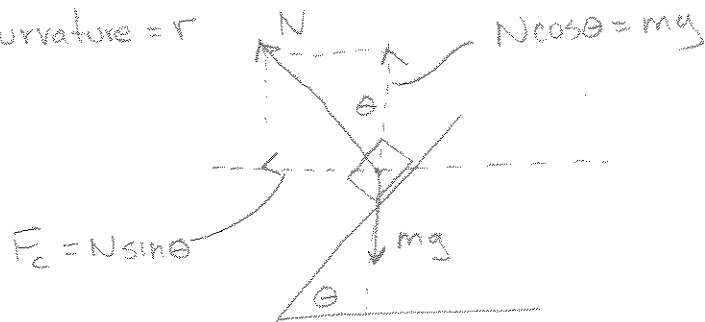
$$t_d = \frac{v_0}{g}(\sin^2\theta - \mu^2\cos^2\theta)^{-1/2}$$

$$t = t_u + t_d$$

$$t = \frac{v_0}{g} \left[(\sin\theta + \mu\cos\theta)^{-1} + (\sin^2\theta - \mu^2\cos^2\theta)^{-1/2} \right]$$

Banked Curve Velocities

1) No Friction

Radius of curvature = r 

$$F_c = N \sin \theta$$

$$\frac{mv^2}{r} = N \sin \theta$$

$$= mg \frac{\sin \theta}{\cos \theta}$$

$$N \cos \theta = mg$$

$$N = \frac{mg}{\cos \theta}$$

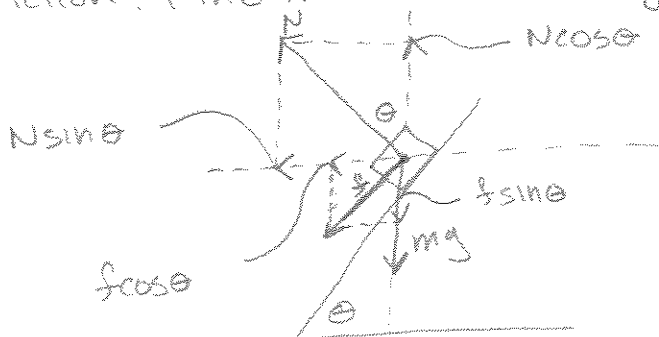
$$\frac{mv^2}{r} = mg \tan \theta$$

$$\frac{v^2}{r} = g \tan \theta$$

$$v^2 = gr \tan \theta$$

$$v = (gr \tan \theta)^{1/2} \text{ (ideal velocity)}$$

2) Friction: Find maximum velocity



$$F_c = N \sin \theta + f \cos \theta$$

$$= N \sin \theta + \mu N \cos \theta$$

$$= N (\sin \theta + \mu \cos \theta)$$

$$= mg \frac{(\sin \theta + \mu \cos \theta)}{\cos \theta - \mu \sin \theta}$$

$$F_c = mg \frac{\tan \theta + \mu}{1 - \mu \tan \theta}$$

$$\frac{mv^2}{r} = mg \frac{\tan \theta + \mu}{1 - \mu \tan \theta}$$

$$v^2 = gr \frac{\tan \theta + \mu}{1 - \mu \tan \theta}$$

$$v = \left(gr \frac{\tan \theta + \mu}{1 - \mu \tan \theta} \right)^{1/2}$$

$$N \cos \theta = mg + f \sin \theta$$

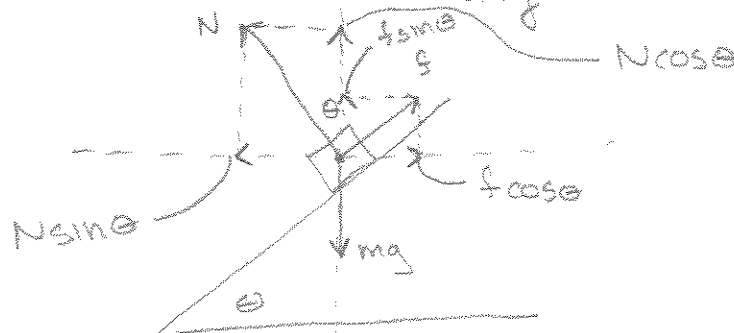
$$= mg + \mu N \sin \theta$$

$$N \cos \theta - \mu N \sin \theta = mg$$

$$N (\cos \theta - \mu \sin \theta) = mg$$

$$N = \frac{mg}{\cos \theta - \mu \sin \theta}$$

3) Friction: Find minimum velocity



$$F_c = N \sin \theta - f \cos \theta$$

$$= N \sin \theta - \mu N \cos \theta$$

$$= N (\sin \theta - \mu \cos \theta)$$

$$= mg \frac{(\sin \theta - \mu \cos \theta)}{(\cos \theta + \mu \sin \theta)}$$

$$F_c = mg \frac{(\tan \theta - \mu)}{(1 + \mu \tan \theta)}$$

$$\frac{mv^2}{r} = mg \frac{(\tan \theta - \mu)}{(1 + \mu \tan \theta)}$$

$$v^2 = gr \frac{\tan \theta - \mu}{1 + \mu \tan \theta}$$

$$v = \left(gr \frac{\tan \theta - \mu}{1 + \mu \tan \theta} \right)^{1/2}$$

$$mg = N \cos \theta + f \sin \theta$$

$$= N \cos \theta + \mu N \sin \theta$$

$$= N (\cos \theta + \mu \sin \theta)$$

$$N = \frac{mg}{\cos \theta + \mu \sin \theta}$$

3-45

$$V(r) = \frac{1}{2} Kr^2$$

$$\int_{r_0}^{r'} \frac{dr}{\left[E - V(r) - \frac{L^2}{2mr^2}\right]^{1/2}} = \sqrt{\frac{2}{m}} t$$

$$E - V(r) - \frac{L^2}{2mr^2} = E - \frac{1}{2} Kr^2 - \frac{L^2}{2mr^2}$$

$$= \frac{2Emr^2 - Kmr^4 - L^2}{2mr^2}$$

$$= \frac{-Kmr^4 + 2Emr^2 - L^2}{2mr^2}$$

$$= \frac{-km(r^4 - 2\frac{E}{K}r^2 + \frac{L^2}{Km})}{2mr^2}$$

$$= -\frac{K}{2r^2} \left(r^4 - \frac{2E}{K}r^2 + \frac{E^2}{K^2} + \frac{L^2}{Km} - \frac{E^2}{K^2} \right)$$

$$= -\frac{K}{2r^2} \left[\left(r^2 - \frac{E}{K} \right)^2 - \frac{E^2}{K^2} + \frac{L^2}{Km} \right]$$

$$= \frac{K}{2r^2} \left[\frac{E}{K^2} - \frac{L^2}{Km} - \left(r^2 - \frac{E}{K} \right)^2 \right]$$

$$\int_{r_0}^{r'} \frac{dr}{\left[E - V(r) - \frac{L^2}{2mr^2}\right]^{1/2}} = \int_{r_0}^{r'} \frac{dr}{\left[\frac{K}{2r^2} \left(\frac{E^2}{K^2} - \frac{L^2}{Km} - \left(r^2 - \frac{E}{K} \right)^2 \right)\right]^{1/2}}$$

$$= \sqrt{\frac{2}{K}} \int_{r_0}^{r'} \frac{r dr}{\left[\frac{E^2}{K^2} - \frac{L^2}{Km} - \left(r^2 - \frac{E}{K} \right)^2 \right]^{1/2}} \quad \text{let } r^2 - \frac{E}{K} = \frac{\sqrt{E^2 - \frac{L^2 K}{m}}}{K} \cos 2\alpha$$

$$2r dr = -\frac{\sqrt{E^2 - \frac{L^2 K}{m}}}{K} \sin 2\alpha \cdot 2d\alpha$$

$$-r dr = \frac{\sqrt{E^2 - \frac{L^2 K}{m}}}{K} \sin 2\alpha d\alpha$$

$$= -\sqrt{\frac{2}{K}} \int_{\alpha_0}^{\alpha} \frac{\frac{\sqrt{E^2 - \frac{L^2 K}{m}}}{K} \sin 2\alpha' d\alpha'}{\frac{\sqrt{E^2 - \frac{L^2 K}{m}}}{K} (1 - \cos^2 2\alpha')^{1/2}}$$

$$= -\sqrt{\frac{2}{K}} \int_{\alpha_0}^{\alpha} d\alpha'$$

$$= -\sqrt{\frac{2}{K}} (\alpha - \alpha_0)$$

$$-\sqrt{\frac{2}{K}} (\alpha - \alpha_0) = \sqrt{\frac{2}{m}} t$$

$$-(\alpha - \alpha_0) = \sqrt{\frac{K}{m}} t$$

$$= \omega t$$

$$-\alpha = \omega t + \alpha_0$$

$$\cos(-\alpha) = \cos(\alpha) \quad \{\text{even function}\}$$

$$r^2 - \frac{E}{K} = \frac{(E^2 - \frac{L^2 K}{m})^{1/2}}{K} \cos 2\alpha$$

$$r^2 = \frac{E}{K} + \frac{(E^2 - L^2 \omega^2)^{1/2}}{K} \cos 2(\omega t + \alpha_0)$$

$$Kr^2 = E + (E^2 - L^2 \omega^2)^{1/2} \cos(2\omega t + 2\alpha_0), \quad \omega = \sqrt{\frac{K}{m}}$$

$$\Theta = \Theta_0 + \int_0^t \frac{L}{mr^2} dt$$

$$\begin{aligned} \Theta - \Theta_0 &= \int_0^t \frac{L}{\frac{m}{K} [E + (E^2 - L^2 \omega^2)^{1/2} \cos(2\omega t + 2\alpha_0)]} dt, \quad \frac{m}{K} = \frac{1}{\omega^2} \\ &= \int_0^t \frac{L \omega^2}{E + (E^2 - L^2 \omega^2)^{1/2} \cos(2\omega t + 2\alpha_0)} dt \end{aligned}$$

$$\text{Let } a = E, \quad b = (E^2 - L^2 \omega^2)^{1/2}$$

$$\begin{aligned} \Theta - \Theta_0 &= L \omega^2 \int_0^t \frac{dt}{a + b \cos(2(\omega t + \alpha_0))} \\ &= \frac{L \omega^2}{\omega} \int_{u_0}^u \frac{du}{(1+u^2)(a + b \frac{(1-u^2)}{(1+u^2)})} \end{aligned}$$

$$= L \omega \int_{u_0}^u \frac{du}{a(1+u^2) + b(1-u^2)}$$

$$= L \omega \int_{u_0}^u \frac{du}{a + a u^2 + b - b u^2}$$

$$= L \omega \int_{u_0}^u \frac{du}{(a+b) + (a-b)u^2}$$

$$= \frac{L \omega}{a-b} \int_{u_0}^u \frac{du}{\frac{a+b}{a-b} + u^2}$$

$$= \frac{L \omega}{a-b} \int_{u_0}^u \frac{du}{c^2 + u^2}$$

$$= \frac{L \omega}{a-b} \int_{\beta_0}^{\beta} \frac{c \sec^2 \beta d\beta}{c^2 (1 + \tan^2 \beta)}$$

$$= \frac{L \omega}{(a-b)c} \int_{\beta_0}^{\beta} d\beta$$

$$= \frac{L \omega}{(a-b)c} \tan^{-1}\left(\frac{u}{c}\right) \Big|_{u_0}^u$$

$$= \frac{L \omega}{(a-b)c} \tan^{-1}\left(\frac{\tan \frac{x}{2}}{\left(\frac{a+b}{a-b}\right)^{1/2}}\right) \Big|_{x_0}^x$$

$$\text{Let } u = \tan\left(\frac{x}{2}\right), \quad x = 2(\omega t + \alpha_0)$$

$$du = \frac{1}{2} \sec^2\left(\frac{x}{2}\right) 2\omega dt$$

$$= (1 + \tan^2\left(\frac{x}{2}\right)) \omega dt$$

$$= (1 + u^2) \omega dt$$

$$\frac{du}{\omega(1+u^2)} = dt$$

$$\cos x = \frac{1-u^2}{1+u^2} \quad \left\{ \text{this is THE TRICK} \right\}$$

$$\text{Let } c^2 = \frac{(a+b)}{(a-b)}$$

$$\text{Let } u = c \tan \beta$$

$$du = c \sec^2 \beta d\beta$$

$$\theta - \theta_0 = \frac{L\omega}{(a-b)c} \tan^{-1} \left(\frac{\tan(\omega t + \alpha_0)}{\left(\frac{a+b}{a-b}\right)^{1/2}} \right) \Big|_0^t$$

$$\begin{aligned} (a-b)c &= [(a-b)(a+b)]^{1/2} \\ &= [a^2 - b^2]^{1/2} \\ &= [E^2 - (E^2 - L^2\omega^2)]^{1/2} \\ &= L\omega \end{aligned}$$

$$\theta - \theta_0 = \frac{L\omega}{L\omega} \tan^{-1} \left(\frac{\tan(\omega t + \alpha_0)}{\left(\frac{a+b}{a-b}\right)^{1/2}} \right) \Big|_0^t$$

$$\theta - \theta_0 = \tan^{-1} \left(\tan(\omega t + \alpha_0) \left(\frac{a-b}{a+b}\right)^{1/2} \right) \Big|_0^t$$

$$\theta - \theta_0 = \tan^{-1} \left(\tan(\omega t + \alpha_0) \frac{[E - (E^2 - L^2\omega^2)^{1/2}]}{L\omega} \right)$$

$$\boxed{\tan(\theta - \theta_0) = (L\omega)^{-1} [E - (E^2 - L^2\omega^2)^{1/2}] \tan(\omega t + \alpha_0)}$$

$$r^2 = x^2 + y^2 + z^2$$

$$kr^2 = E + (E^2 - L^2\omega^2)^{1/2} \cos(2\omega t + 2\alpha_0)$$

$$r^2 \propto \cos(2\omega t + 2\alpha_0)$$

$$\tan(\theta - \theta_0) \propto \tan(\omega t + \alpha_0)$$

$$\theta - \theta_0 \propto \omega t + \alpha_0$$

$$\boxed{\begin{aligned} \omega_x = \omega_y = \omega_z \text{ \{ given as isotropic from Problem 3-43 \} } \\ \text{and } \omega_r = 2\omega_\theta, \text{ the motion is an ellipse} \end{aligned}}$$

$$\begin{aligned} \left(\frac{a-b}{a+b}\right)^{1/2} &= \left[\frac{a-b}{a+b} \cdot \frac{a-b}{a-b} \right]^{1/2} \\ &= \left[\frac{(a-b)^2}{a^2 - b^2} \right]^{1/2} \end{aligned}$$

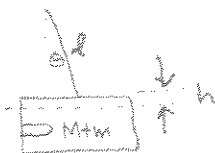
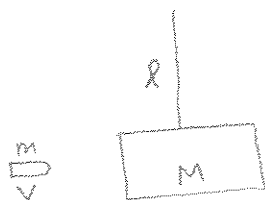
$$= \frac{a-b}{(a^2 - b^2)^{1/2}}$$

$$= \frac{E - (E^2 - L^2\omega^2)^{1/2}}{[E^2 - (E^2 - L^2\omega^2)]^{1/2}}$$

$$= \frac{E - (E^2 - L^2\omega^2)^{1/2}}{(L^2\omega^2)^{1/2}}$$

$$= \frac{E - (E^2 - L^2\omega^2)^{1/2}}{L\omega}$$

4-3



$$E = T + V$$

$$E_i = \frac{1}{2} m v^2$$

$$E_f = (M+m) g h$$

$$= (M+m) g l (1 - \cos \theta)$$

$$E_i = E_f$$

$$\frac{1}{2} m v^2 = (M+m) g l (1 - \cos \theta)$$

$$v^2 = (1 - \cos \theta) 2 g l \left(\frac{M+m}{m} \right)$$

$$v = \left[(1 - \cos \theta) 2 g l \left(\frac{M+m}{m} \right) \right]^{1/2}$$

$$= \left[4 \sin^2 \frac{\theta}{2} g l \left(1 + \frac{M}{m} \right) \right]^{1/2}$$

$$v = 2 \left[\left(1 + \frac{M}{m} \right) g l \right]^{1/2} \sin \frac{\theta}{2}$$

$$\cos \theta = \frac{x}{l}$$

$$x = l \cos \theta$$

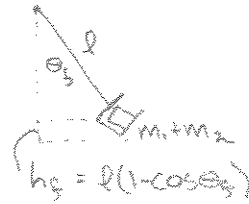
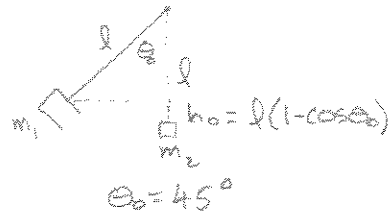
$$h = l - x$$

$$= l - l \cos \theta$$

$$= l (1 - \cos \theta)$$

$$2 \sin^2 \frac{\theta}{2} = (1 - \cos \theta)$$

4-5



$$T + V = E$$

$$E_0 = m_1 g h_0$$

$$= m_1 g l (1 - \cos\theta_0)$$

$$E_3 = (m_1 + m_2) g h_3$$

$$= (m_1 + m_2) g l (1 - \cos\theta_3)$$

Velocity just prior to impact

$$\frac{1}{2} m_1 V_0^2 = E_0 = m_1 g h_0$$

$$V_0^2 = 2 g h_0$$

Angular momentum just prior to impact

$$L_0 = m_1 V_0 l$$

Angular momentum just after impact

$$L_3 = (m_1 + m_2) V_3 l$$

Conservation of angular momentum

$$L_0 = L_3$$

$$m_1 V_0 l = (m_1 + m_2) V_3 l$$

$$V_3 = V_0 \frac{m_1}{m_1 + m_2}$$

Energy just after impact

$$E_3 = \frac{1}{2} (m_1 + m_2) V_3^2$$

Conservation of Energy after impact

$$\frac{1}{2} (m_1 + m_2) V_3^2 = (m_1 + m_2) g l (1 - \cos\theta_3)$$

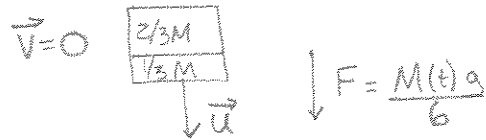
$$1 - \cos\theta_3 = \frac{1}{2} \frac{V_3^2}{g l} \quad ; \quad V_3^2 = V_0^2 \left(\frac{m_1}{m_1 + m_2} \right)^2$$

$$\cos\theta_3 = 1 - (1 - \cos\theta_0) \left(\frac{m_1}{m_1 + m_2} \right)^2 = 2 g l (1 - \cos\theta_0) \left(\frac{m_1}{m_1 + m_2} \right)^2$$

$$\theta_3 = \cos^{-1} \left[1 - (1 - \cos\theta_0) \left(\frac{m_1}{m_1 + m_2} \right)^2 \right] \quad , \quad 1 - \cos\theta_0 = 1 - .707 = .293$$

$$\boxed{\theta_3 = \cos^{-1} \left[1 - .293 \left(\frac{m_1}{m_1 + m_2} \right)^2 \right]}$$

4-7



$$\frac{d}{dt}(M\vec{V}) - \frac{dM}{dt}(\vec{V} + \vec{u}) = F$$

$$\vec{F} = -\frac{dM}{dt}\vec{u}$$

$$\frac{Mg}{6} = -\frac{dM}{dt}u$$

$$-\frac{g}{6u}dt = \frac{dM}{M}$$

$$-\frac{g}{6u} \int_0^t dt = \int_{\frac{2}{3}M}^M \frac{dM}{M}$$

$$-\frac{gt}{6u} = \ln M \Big|_{\frac{2}{3}M}$$

$$= \ln \frac{2M}{3} - \ln M$$

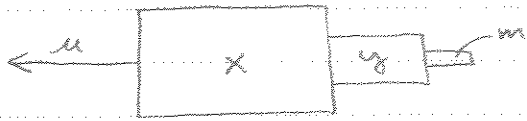
$$= \ln \frac{2}{3}$$

$$t = \frac{6u}{g} \ln \frac{3}{2}, \quad u = 1500 \text{ m/s}$$

$$= \frac{6(1500)}{9.81} \ln \frac{3}{2}$$

$$t = 372 \text{ s}$$

4-9



$$V_0 = 0$$

$$V_5 = 6000 \text{ m/s}$$

$$u = 1500 \text{ m/s}$$

$$r = 10$$

$$\frac{d}{dt}(M\vec{v}) - \frac{dM}{dt}(\vec{v} + \vec{u}) = F$$

$$\frac{dM}{dt}\vec{v} + M\frac{d\vec{v}}{dt} - \frac{dM}{dt}\vec{v} - \frac{dM}{dt}\vec{u} = 0 \quad \{F=0\}$$

$$M\frac{d\vec{v}}{dt} - \frac{dM}{dt}\vec{u} = 0$$

$$Mdv = -u dM$$

$$dv = -u \frac{dM}{M}$$

$$\int_{V_0}^{V_1} dv = -u \int_{M_0}^{M_1}$$

$$V_1 - V_0 = u \ln \frac{M_0}{M_1}$$

a) First stage

$$V_1 = u \ln \frac{x+y+m}{rx+y+m}$$

Second stage

$$V_2 = u \ln \frac{y+m}{ry+m}$$

$$V_5 = V_1 + V_2$$

$$= u \ln \left[\frac{x+y+m}{rx+y+m} \cdot \frac{y+m}{ry+m} \right]$$

$$e^{\frac{V_5}{u}} = \frac{x+y+m}{rx+y+m} \cdot \frac{y+m}{ry+m}$$

$$(rx+y+m)(ry+m)e^k = (x+y+m)(y+m), k = \frac{y}{x}$$

$$rx(ry+m)e^k + (y+m)(ry+m)e^k = x(y+m) + (y+m)^2$$

$$(y+m)(ry+m)e^k - (y+m)^2 = x(y+m) - rx(ry+m)e^k$$

$$= x(y+m - r(ry+m)e^k)$$

$$x = \frac{(y+m)(ry+m)e^k - (y+m)^2}{y+m - r(ry+m)e^k}$$

$$= \frac{(y+m)[(ry+m)e^k - (y+m)]}{y+m - r(ry+m)e^k}$$

$$M_r = x + y + m$$

$$= \frac{(y+m)[(ry+m)e^k - (y+m)]}{y+m - r(ry+m)e^k} + y + m$$

$$\frac{dM_r}{dy} = \frac{d}{dy} \left[\frac{(y+m)[(ry+m)e^k - (y+m)]}{y+m - r(ry+m)e^k} \right] + 1$$

$$\frac{dx}{dy} = \frac{[(y+m) - (ry+m)re^k] \cdot [(y+m)(re^k - 1) + [(ry+m)e^k - (y+m)] - [(y+m)[(ry+m)e^k - (y+m)][1 - r^2e^k]]}{D^2}$$

$$D^2 \frac{dx}{dy} = (y+m)^2(re^k - 1) + (y+m)(ry+m)e^k - (y+m)^2 - (y+m)(ry+m)(re^k - 1)re^k - (ry+m)^2re^{2k} + (y+m)(ry+m)re^k - [(y+m)(ry+m)e^k - (y+m)^2 - (y+m)(ry+m)r^2e^{2k} + (y+m)^2r^2e^k]$$

$$= (y+m)^2re^k - (y+m)^2 + (y+m)(ry+m)e^k - (y+m)^2 - (y+m)(ry+m)r^2e^{2k} + (y+m)(ry+m)re^k - (ry+m)^2re^{2k} + (y+m)(ry+m)re^k - (y+m)(ry+m)e^k + (y+m)^2 + (y+m)(ry+m)r^2e^{2k} - (y+m)^2r^2e^k$$

$$= (y+m)^2 r e^k - (y+m)^2 + 2(y+m)(r y+m) r e^k - (r y+m)^2 r e^{2k} - (y+m)^2 r^2 e^k$$

Minimize M_T

$$M_T = x + y + m$$

$$\frac{dM_T}{dy} = \frac{dx}{dy} + 1$$

$$0 = D^2 \frac{dx}{dy} + D^2$$

$$0 = (y+m)^2 r e^k - (y+m)^2 + 2(y+m)(r y+m) r e^k - (r y+m)^2 r e^{2k} - (y+m)^2 r^2 e^k + ((y+m) - (r y+m) r e^k)^2$$

$$= (y+m)^2 r e^k - (y+m)^2 + 2(y+m)(r y+m) r e^k - (r y+m)^2 r e^{2k} - (y+m)^2 r^2 e^k + (y+m)^2 - 2(y+m)(r y+m) r e^k + (r y+m)^2 r^2 e^{2k}$$

$$= (y+m)^2 r e^k - (r y+m)^2 r e^{2k} - (y+m)^2 r^2 e^k + (r y+m)^2 r^2 e^{2k}$$

$$= (y^2 + 2my + m^2) r e^k - (r^2 y^2 + 2rmy + m^2) r e^{2k} - (y^2 + 2my + m^2) r^2 e^k + (r^2 y^2 + 2rmy + m^2) r^2 e^{2k}$$

$$= y^2 (r e^k - r^3 e^{2k} + r^2 e^k + r^4 e^{2k}) + y (2mr e^k - 2mr^2 e^{2k} - 2mr^2 e^k + 2mr^3 e^{2k}) + m^2 r e^k - m^2 r e^{2k} - m^2 r^2 e^k + m^2 r^2 e^{2k}$$

$$= y^2 r e^k (1 + r - r^2 e^k + r^3 e^k) + y 2mr e^k (1 - r e^k - r + r^2 e^k) + m^2 r e^k (1 - e^k - r + r e^k)$$

$$0 = y^2 + \frac{2mr e^k (1 - r e^k - r + r^2 e^k)}{r e^k (1 + r - r^2 e^k + r^3 e^k)} + \frac{m^2 r e^k (1 - e^k - r + r e^k)}{r e^k (1 + r - r^2 e^k + r^3 e^k)}$$

$$\left(y + \frac{m(1-r-e^k+r^2e^k)}{(1+r-r^2e^k+r^3e^k)}\right)^2 = \left[\frac{m(1-r-e^k+r^2e^k)}{(1+r-r^2e^k+r^3e^k)}\right]^2 -$$

$$\frac{m^2(1-r-e^k+r^2e^k)}{(1+r-r^2e^k+r^3e^k)}$$

$$y = \frac{-m(1-r-e^k+r^2e^k)}{(1+r-r^2e^k+r^3e^k)} \pm \left[\left[\frac{m(1-r-e^k+r^2e^k)}{(1+r-r^2e^k+r^3e^k)} \right]^2 + \frac{m^2(1+r+e^k-re^k)}{1+r-r^2e^k+r^3e^k} \right]^{1/2}$$

$$= m \left[\frac{-(1-r-e^k+r^2e^k)}{1+r-r^2e^k+r^3e^k} \pm \left[\left(\frac{1-r-e^k+r^2e^k}{1+r-r^2e^k+r^3e^k} \right)^2 + \frac{1+r+e^k-re^k}{1+r-r^2e^k+r^3e^k} \right]^{1/2} \right]$$

$$\frac{1-r-e^k+r^2e^k}{1+r-r^2e^k+r^3e^k} = \frac{-4.01}{.409} = -9.804$$

$$\frac{1+r+e^k-re^k}{1+r-r^2e^k+r^3e^k} = \frac{50.238}{.409} = 122.83$$

$$y = m \left[9.804 \pm \left[96.126 + 122.83 \right]^{1/2} \right]$$

$$= m [9.804 + 14.80]$$

$$= m [24.60]$$

$$y = 2460 \text{ kg}$$

$$\begin{aligned}
 x &= \frac{(y+m)(ry+m)e^k - (y+m)^2}{y+m - r(ry+m)e^k} \\
 &= \frac{(2460+100)(246+100)e^4 - (2460+100)^2}{2460+100 - 0.1(246+100)e^4} \\
 &= \frac{(2560)(346)e^4 - (2560)^2}{2560 - 0.1(346)e^4}
 \end{aligned}$$

$$x = 62315 \text{ Kg}$$

b) For a single stage

$$V_s = u \ln \frac{x+m}{rx+m}$$

$$e^{\frac{V_s}{u}} = \frac{x+m}{rx+m} \quad K = \frac{V_s}{u} = 4$$

$$(rx+m)e^k = x+m$$

$$me^k - m = x - rx e^k$$

$$m(e^k - 1) = x(1 - re^k)$$

$$x = \frac{m(e^k - 1)}{1 - re^k}$$

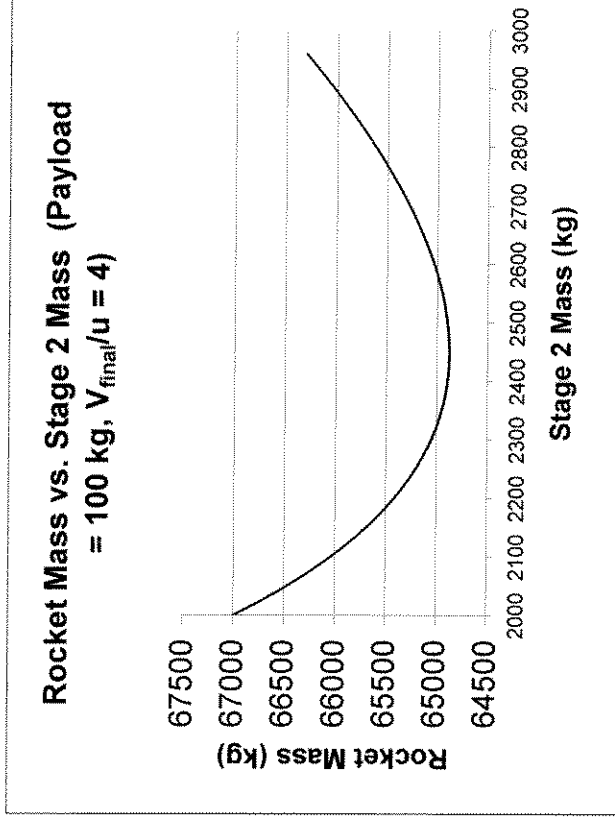
$re^k < 1$ condition must hold. But

$r = 0.1$ and $e^k = 54.6$. So

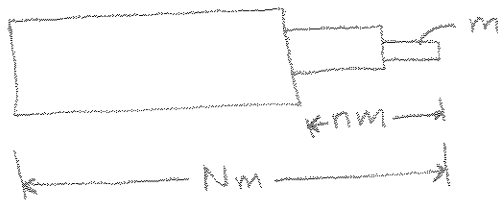
$$re^k = 5.46 > 1$$

Therefore, a single stage rocket cannot achieve 4 times the exhaust velocity when $r = 0.1$.

2442	41309237	662.7317	62331.77	64873.77
2444	41364430	663.6397	62329.65	64873.65
2446	41419658	664.5477	62327.59	64873.59
2448	41474923	665.4558	62325.59	64873.59
2450	41530222	666.3638	62323.65	64873.65
2452	41585558	667.2719	62321.76	64873.76
2454	41640929	668.1799	62319.94	64873.94
2456	41696336	669.0879	62318.17	64874.17
2458	41751779	669.996	62316.46	64874.46
2460	41807257	670.904	62314.81	64874.81
2462	41862771	671.812	62313.22	64875.22
2464	41918321	672.7201	62311.68	64875.68
2466	41973906	673.6281	62310.21	64876.21
2468	42029527	674.5362	62308.78	64876.78
2470	42085184	675.4442	62307.42	64877.42
2472	42140877	676.3522	62306.11	64878.11
2474	42196605	677.2603	62304.86	64878.86
2476	42252368	678.1683	62303.66	64879.66
2478	42308168	679.0763	62302.52	64880.52
2480	42364003	679.9844	62301.44	64881.44
2482	42419874	680.8924	62300.41	64882.41
2484	42475780	681.8005	62299.43	64883.43
2486	42531722	682.7085	62298.51	64884.51
2488	42587700	683.6165	62297.65	64885.65
2490	42643714	684.5246	62296.83	64886.83
2492	42699763	685.4326	62296.08	64888.08
2494	42755848	686.3406	62295.38	64889.38
2496	42811968	687.2487	62294.73	64890.73
2498	42868125	688.1567	62294.13	64892.13
2500	42924317	689.0647	62293.59	64893.59
2502	42980544	689.9728	62293.1	64895.1
2504	43036807	690.8808	62292.66	64896.66
2506	43093106	691.7889	62292.28	64898.28
2508	43149441	692.6969	62291.95	64899.95
2510	43205811	693.6049	62291.67	64901.67
2512	43262217	694.513	62291.45	64903.45
2514	43318659	695.421	62291.27	64905.27



4-9



$$r = \frac{\text{empty canister}}{\text{empty canister} + \text{fuel}} = .10$$

$$m = 100 \text{ kg}$$

$$V_0 = 0$$

$$V_g = 6000 \text{ m/s}$$

$$u = 1500 \text{ m/s}$$

$$\vec{F} = 0$$

$$\frac{d}{dt}(M\vec{v}) - \frac{dM}{dt}(\vec{v} + \vec{u}) = \vec{F}$$

$$\frac{dM}{dt}\vec{v} + M\frac{d\vec{v}}{dt} - \frac{dM}{dt}\vec{v} - \frac{dM}{dt}\vec{u} = 0$$

$$M\frac{d\vec{v}}{dt} - \frac{dM}{dt}\vec{u} = 0$$

$$M\frac{dv}{dt} = -u\frac{dM}{dt}$$

$$dv = -u\frac{dM}{M}$$

$$\int_{V_0}^{V_1} dv = -u \int_{m_i}^{m_f} \frac{dM}{M}$$

$$V_1 = -u \ln \frac{m_f}{m_i}$$

$$V_1 = u \ln \frac{m_i}{m_f}$$

$$V_1 = u \ln \frac{Nm}{m[r(N-n)+n]}$$

$$V_1 = u \ln \frac{N}{rN+n(1-r)}$$

$$V_2 = u \ln \frac{m'_1}{m_2}$$

$$= u \ln \frac{nm}{m[rn-r+1]}$$

$$V_2 = u \ln \frac{n}{rn-r+1}$$

$$m_i = Nm$$

$$m_f = r(Nm-nm) + nm$$

$$= m[r(N-n)+n]$$

$$m'_1 = nm$$

$$m_2 = r(nm-m) + m$$

$$= m[r(n-1)+1]$$

$$= m[rn-r+1]$$

$$V_3 = V_1 + V_2$$

$$= u \ln \left(\frac{N}{rN+n(1-r)} \cdot \frac{n}{rn-r+1} \right)$$

N and r are constants. To find n giving a maximum velocity, take $\frac{d}{dn}$ and set $\frac{dV_3}{dn} = 0$.

$$\frac{d}{dx} \ln u = \frac{1}{u} \frac{du}{dx}$$

$$\frac{d}{dn} \ln(f(n)) = \frac{1}{f(n)} \frac{df(n)}{dn}$$

$$= \frac{(rN+n(1-r))(rn-r+1)}{Nn} \cdot \frac{\left[(rN+n(1-r))(rn-r+1)N - Nn \frac{d}{dn} [(rN+n(1-r))(rn-r+1)] \right]}{[(rN+n(1-r))(rn-r+1)]^2}$$

$$= \frac{1}{Nn} \left[\frac{N}{D} - \frac{Nn[(rN+n(1-r))(r) + (rn-r+1)(1-r)]}{D^2} \right]$$

$$0 = \frac{1}{nD} - \frac{(rN+n(1-r))(r) + (rn-r+1)(1-r)}{D^2}$$

$$\frac{(rN+n(1-r))(r) + (rn-r+1)(1-r)}{D^2} = \frac{1}{nD}$$

$$n[r^2N + rn(1-r) + (rn-r+1)(1-r)] = D$$

$$n[r^2N + rn - r^2n + rn - r + 1 - r^2n + r^2 - r] = D$$

$$n[r^2N + 2rn - 2r^2n - 2r + r^2 + 1] = D$$

$$r^2Nn + 2rn^2 - 2r^2n^2 - 2rn + r^2n + n = (rN + n(1-r))(rn-r+1)$$

$$= (rN + n - nr)(rn-r+1)$$

$$r^2Nn + 2rn^2 - 2r^2n^2 - 2rn + r^2n + n = r^2Nn - r^2N + rN + rn^2 - rn + n - n^2r^2 + n^2r - nr$$

$$rn^2 - r^2n^2 = rN - r^2N$$

$$n^2(r-r^2) = N(r-r^2)$$

$$n^2 = N$$

$$n = N^{1/2}$$

$$\begin{aligned}
 V_g &= u \ln \left(\frac{N}{rN + \sqrt{N}(1-r)} \cdot \frac{N^{1/2}}{rN^{1/2} - r + 1} \right) \\
 &= u \ln \left(\frac{N}{N^{1/2}(rN^{1/2} + 1 - r)} \cdot \frac{N^{1/2}}{rN^{1/2} + 1 - r} \right) \\
 &= u \ln \left(\frac{N^{1/2}}{rN^{1/2} + 1 - r} \cdot \frac{N^{1/2}}{rN^{1/2} + 1 - r} \right)
 \end{aligned}$$

$$V_g = 2u \ln \left(\frac{N^{1/2}}{rN^{1/2} + 1 - r} \right)$$

$$\frac{V_g}{2u} = \ln \left(\frac{N^{1/2}}{rN^{1/2} + 1 - r} \right)$$

$$e^k = \frac{N^{1/2}}{rN^{1/2} + 1 - r}, \quad k = \frac{V_g}{2u}$$

$$e^k r N^{1/2} + e^k - r e^k = N^{1/2}$$

$$\begin{aligned}
 e^k - r e^k &= N^{1/2} - e^k r N^{1/2} \\
 &= N^{1/2} (1 - r e^k)
 \end{aligned}$$

$$\frac{e^k - r e^k}{1 - r e^k} = N^{1/2}$$

$$\frac{e^k (1 - r)}{1 - r e^k} = N^{1/2}$$

$$N = \frac{e^{2k} (1 - r)^2}{(1 - r e^k)^2}$$

$$= \frac{e^4 (0.9)^2}{(1 - 0.1 e^2)^2}$$

$$= \frac{44.22}{0.068}$$

$$N = 648.66 \rightarrow$$

$$\boxed{1^{st} \text{ stage mass} = 64866 \text{ kg} - 2547 \text{ kg} = 62319 \text{ kg}}$$

$$n = N^{1/2}$$

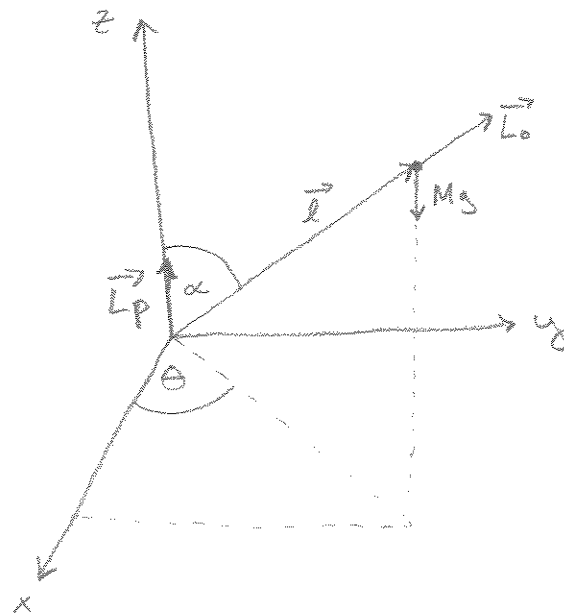
$$n = 25.47 \rightarrow$$

$$\boxed{2^{nd} \text{ stage mass} = 2547 \text{ kg} - 100 \text{ kg} = 2447 \text{ kg}}$$

$$2k = \frac{V_g}{u} = 4$$

$k = 2$ { each stage provides half the final velocity }

4-11



$$\vec{L} = \vec{L}_o + \vec{L}_p$$

$$\vec{L}_o = MR^2 \omega_o (\cos \theta \sin \alpha \hat{i} + \sin \theta \sin \alpha \hat{j} + \cos \alpha \hat{k})$$

$$\vec{L}_p = M(l \sin \alpha)^2 \omega_p \hat{k}$$

$$\frac{d\vec{L}}{dt} = MR^2 \omega_o \left(\left[\cos \theta \cos \alpha \frac{d\alpha}{dt} - \sin \theta \sin \alpha \frac{d\theta}{dt} \right] \hat{i} + \left[\sin \theta \cos \alpha \frac{d\alpha}{dt} + \cos \theta \sin \alpha \frac{d\theta}{dt} \right] \hat{j} - \sin \alpha \frac{d\alpha}{dt} \hat{k} \right) + Ml^2 \left[\sin^2 \alpha \frac{d\omega_p}{dt} + 2 \sin \alpha \cos \alpha \frac{d\alpha}{dt} \right] \hat{k}$$

$$\vec{N} = \vec{l} \times M \vec{g} \quad \vec{l} = l (\cos \theta \sin \alpha \hat{i} + \sin \theta \sin \alpha \hat{j} + \cos \alpha \hat{k})$$

$$= Ml \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \cos \theta \sin \alpha & \sin \theta \sin \alpha & \cos \alpha \\ 0 & 0 & -g \end{vmatrix}$$

$$= Ml (-g \sin \theta \sin \alpha \hat{i} + g \cos \theta \sin \alpha \hat{j})$$

$$\frac{d\vec{L}}{dt} = \vec{N}, \text{ for } \omega_o \text{ large, nutation is small} \rightarrow \frac{d\alpha}{dt} \approx 0, \text{ and } \frac{d\theta}{dt} = \omega_p$$

Equating components:

$$R^2 \omega_0 [-\sin \theta \sin \alpha \omega_p] = -g l \sin \theta \sin \alpha$$

$$R^2 \omega_0 [\cos \theta \sin \alpha \omega_p] = g l \cos \theta \sin \alpha$$

Each equation gives

$$\omega_p = \frac{g l}{R^2 \omega_0}$$

when $\frac{d\alpha}{dt} \approx 0$

4-13

$$L_o = L_{sp_o} + L_{p_o}$$

$$L_{sp_o} = Mr_o^2 \omega_{y_o}, \quad \omega_{y_o} = \text{angular velocity of present year}$$

$$= Mr_o^2 2\pi/Y_o, \quad Y_o \text{ is present year}$$

$$L_{p_o} = \frac{2}{5} Ma^2 \omega_o$$

$$L_i = L_{sp_i} + L_{p_i}$$

$$L_{sp_i} = Mr^2 \omega_y$$

$$L_{p_i} = \frac{2}{5} Ma^2 \omega$$

$$L_o = L_i$$

$$r_o^2 \omega_{y_o} + \frac{2}{5} a^2 \omega_o = r^2 \omega_y + \frac{2}{5} a^2 \omega$$

$$\frac{2}{5} a^2 (\omega_o - \omega) + r_o^2 \omega_{y_o} = r^2 \omega_y$$

$$= r v_{tan}$$

$$\frac{2}{5} \frac{a^2 (\omega_o - \omega)}{r_o^2 \omega_{y_o}} + 1 = \frac{r v_{tan}}{r_o v_{tan_o}}$$

$$\frac{Y_o}{5\pi} \frac{a^2 (\omega_o - \omega)}{r_o^2} + 1 = \frac{r \sqrt{\frac{MG}{r}}}{r_o \sqrt{\frac{MG}{r_o}}}$$

$$= \frac{r^{1/2}}{r_o^{1/2}}$$

$$r^{1/2} = r_o^{1/2} \left(1 + \frac{a^2 (\omega_o - \omega) Y_o}{5\pi r_o^2} \right)$$

$$\boxed{r = r_o \left(1 + \frac{a^2 (\omega_o - \omega) Y_o}{5\pi r_o^2} \right)^2}$$

$$a = 3960 \text{ mi}$$

$$r_o = 9.29 \times 10^7 \text{ mi}$$

$$\omega_o = \frac{2\pi}{24 \text{ hr}} = 7.27 \times 10^{-5} /s$$

$$Y_o = 3.15 \times 10^7 \text{ s}$$

$$\omega_{y_o} = \frac{2\pi}{Y_o}$$

$$F = ma$$

$$= \frac{mM}{r^2} G$$

$$a = \frac{MG}{r^2}$$

$$\frac{v^2}{r} = \frac{MG}{r^2}$$

$$v_{tan} = \sqrt{\frac{MG}{r}}$$

$$r = r_0 \left(1 + \frac{1}{5\pi} \frac{a^2}{r_0^2} (\omega_0 - \omega_{y_0}) Y_0 \right)^2$$

$$= r_0 \left(1 + \frac{1}{5\pi} \frac{a^2}{r_0^2} (\omega_0 Y_0 - 2\pi) \right)^2$$

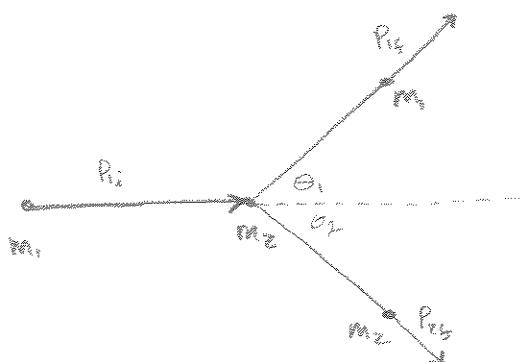
$$= (9.29 \times 10^7 \text{ mi}) \left(1 + \frac{1}{5\pi} \left(\frac{3960}{9.29 \times 10^7} \right)^2 ((1.27 \times 10^{-5})(3.15 \times 10^7) - 2\pi) \right)^2$$

$$r = 92900049 \text{ mi}$$

r increases 49 miles

If the moon was taken into account the change in distance from the sun would be less due to tidal friction from the moon.

4-15



$$p_{1i} = p_{1f} \cos \theta_1 + p_{2f} \cos \theta_2$$

$$p_{1f} \sin \theta_1 = p_{2f} \sin \theta_2$$

$$p_{1i} - p_{2f} \cos \theta_2 = p_{1f} \cos \theta_1$$

$$p_{1f}^2 \sin^2 \theta_1 = p_{2f}^2 \sin^2 \theta_2$$

$$p_{1i}^2 - 2 p_{1i} p_{2f} \cos \theta_2 + p_{2f}^2 \cos^2 \theta_2 = p_{1f}^2 \cos^2 \theta_1$$

$$p_{2f}^2 \sin^2 \theta_2 = p_{1f}^2 \sin^2 \theta_1$$

$$p_{1i}^2 - 2 p_{1i} p_{2f} \cos \theta_2 + p_{2f}^2 = p_{1f}^2$$

$$\frac{p_{1i}^2}{2m_1} = \frac{p_{1f}^2}{2m_1} + \frac{p_{2f}^2}{2m_2}$$

$$\frac{p_{1i}^2 - p_{1f}^2}{m_1} = \frac{p_{2f}^2}{m_2}$$

$$\frac{p_{1i}^2 - (p_{1i}^2 - 2 p_{1i} p_{2f} \cos \theta_2 + p_{2f}^2)}{m_1} = \frac{p_{2f}^2}{m_2}$$

$$\frac{2 p_{1i} p_{2f} \cos \theta_2 - p_{2f}^2}{m_1} = \frac{p_{2f}^2}{m_2}$$

$$p_{2f}^2 \left(\frac{1}{m_2} + \frac{1}{m_1} \right) = \frac{2 p_{1i} p_{2f} \cos \theta_2}{m_1}$$

$$p_{2f} \left[\frac{m_1 + m_2}{m_1 m_2} p_{2f} - \frac{2 p_{1i} \cos \theta_2}{m_1} \right] = 0$$

$$p_{2f} = \frac{m_1 m_2}{m_1 + m_2} \frac{2 p_{1i} \cos \theta_2}{m_1}$$

$$p_{2f} = \frac{2 m_2 \cos \theta_2}{m_1 + m_2} p_{1i}$$

$$T_{zf} = \frac{P_{zf}^2}{2m_z}$$

$$= \frac{4 \left(\frac{m_z}{m_1+m_z} \right)^2 \cos^2 \theta_z P_i^2}{2m_z}$$

$$T_{zf} = 2 \frac{m_z}{(m_1+m_z)^2} \cos^2 \theta_z P_i^2$$

T_{zf} is a max at $\theta_z = 0$ since $\cos^2 \theta_z = 1$ at $\theta_z = 0$ provided m_1 does not miss m_z

When T_{zf} is a max

$$T_{1i} = T_{1f} + T_{zf}$$

$$T_{1i} - T_{1f} = T_{zf}$$

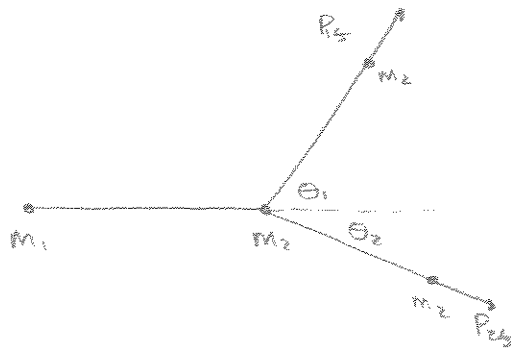
$$= \frac{2m_z}{(m_1+m_z)^2} P_i^2$$

$$\frac{P_i^2}{2m_1} = T_{1i}$$

$$= \frac{2m_z}{(m_1+m_z)} 2m_1 T_{1i}$$

$$T_{1i} - T_{1f} = \frac{4m_1 m_z}{(m_1+m_z)^2} T_{1i}$$

4-17



$$p_{1i} = p_{1f} \cos \theta_1 + p_{2f} \cos \theta_2 \quad p_{1f} \sin \theta_1 = p_{2f} \sin \theta_2$$

$$\frac{p_{1i}^2}{m_1} - \frac{p_{1f}^2}{m_1} = \frac{p_{2f}^2}{m_2}$$

$$p_{1i} - p_{1f} \cos \theta_1 = p_{2f} \cos \theta_2$$

$$p_{1i}^2 - 2p_{1i}p_{1f} \cos \theta_1 + p_{1f}^2 \cos^2 \theta_1 = p_{2f}^2 \cos^2 \theta_2$$

$$p_{1f}^2 \sin^2 \theta_1 = p_{2f}^2 \sin^2 \theta_2$$

$$p_{2f}^2 = m_2 \left(\frac{p_{1i}^2 - p_{1f}^2}{m_1} \right)$$

$$p_{1i}^2 + p_{1f}^2 - 2p_{1i}p_{1f} \cos \theta_1 = p_{2f}^2$$

$$= m_2 \left(\frac{p_{1i}^2 - p_{1f}^2}{m_1} \right)$$

$$m_2 = \frac{m_1}{p_{1i}^2 - p_{1f}^2} (p_{1i}^2 + p_{1f}^2 - 2p_{1i}p_{1f} \cos \theta_1)$$

$$= \frac{m_1}{p_{1i}^2 - p_{1f}^2} p_{1i}^2 \left(1 + \frac{p_{1f}^2}{p_{1i}^2} - 2 \frac{p_{1f}}{p_{1i}} \cos \theta_1 \right)$$

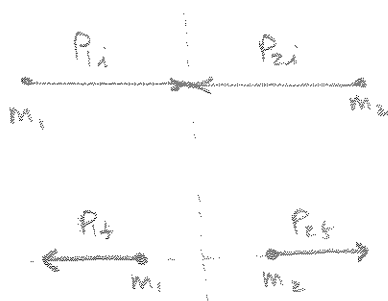
$$= \frac{m_1}{\frac{p_{1i}^2 - p_{1f}^2}{p_{1i}^2}} \left(1 + \frac{p_{1f}^2}{p_{1i}^2} - 2 \frac{p_{1f}}{p_{1i}} \cos \theta_1 \right)$$

$$= \frac{m_1}{1 - \frac{p_{1f}^2}{p_{1i}^2}} \left(1 + \frac{p_{1f}^2}{p_{1i}^2} - 2 \frac{p_{1f}}{p_{1i}} \cos \theta_1 \right)$$

$$m_2 = \frac{m_1}{1 - \alpha} (1 + \alpha^2 - 2\alpha \cos \theta_1), \quad \alpha = \frac{p_{1f}}{p_{1i}}$$

To verify the elastic collision measure θ_2 and confirm.

4-19



$$\begin{aligned}
 P_{1i} - P_{2i} &= -P_{1f} + P_{2f} & \frac{P_{1i}^2}{m_1} + \frac{P_{2i}^2}{m_2} &= \frac{P_{1f}^2}{m_1} + \frac{P_{2f}^2}{m_2} \\
 m_1 V_{1i} - m_2 V_{2i} &= -m_1 V_{1f} + m_2 V_{2f} & m_1 V_{1i}^2 + m_2 V_{2i}^2 &= m_1 V_{1f}^2 + m_2 V_{2f}^2 \\
 m_1 V_{1i} + m_1 V_{1f} &= m_2 V_{2i} + m_2 V_{2f} & m_1 (V_{1i}^2 - V_{1f}^2) &= m_2 (V_{2f}^2 - V_{2i}^2) \\
 m_1 (V_{1i} + V_{1f}) &= m_2 (V_{2i} + V_{2f}) & m_1 (V_{1i} - V_{1f})(V_{1i} + V_{1f}) &= m_2 (V_{2f} - V_{2i})(V_{2f} + V_{2i})
 \end{aligned}$$

$$\frac{m_1 (V_{1i} - V_{1f})(V_{1i} + V_{1f})}{m_1 (V_{1i} + V_{1f})} = \frac{m_2 (V_{2f} - V_{2i})(V_{2f} + V_{2i})}{m_2 (V_{2f} + V_{2i})}$$

$$V_{1i} - V_{1f} = V_{2f} - V_{2i}$$

$$V_{2f} + V_{1f} = V_{1i} + V_{2i}$$

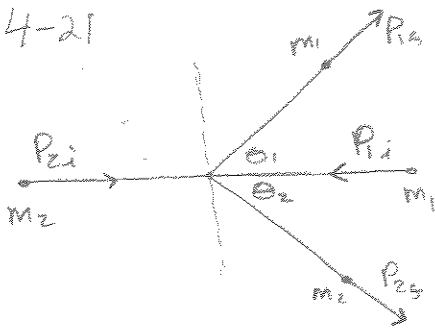
$$V_{2f} - (-V_{1f}) = V_{1i} - (-V_{2i})$$

comparing to 4.85

$$V_{2f} - V_{1f} = e(V_{1i} - V_{2i})$$

e must equal 1

4-21

Given: $m_1, m_2, P_{1i}, P_{2i}, \theta_1$ Find: P_{1f}

$$P_{2i} - P_{1i} = P_{1f} \cos \theta_1 + P_{2f} \cos \theta_2, \quad P_{1f} \sin \theta_1 = P_{2f} \sin \theta_2, \quad \frac{P_{1i}^2}{m_1} + \frac{P_{2i}^2}{m_2} = \frac{P_{1f}^2}{m_1} + \frac{P_{2f}^2}{m_2}$$

$$(P_{2i} - P_{1i}) - P_{1f} \cos \theta_1 = P_{2f} \cos \theta_2$$

$$(P_{2i} - P_{1i})^2 - 2(P_{2i} - P_{1i})P_{1f} \cos \theta_1 + P_{1f}^2 \cos^2 \theta_1 = P_{2f}^2 \cos^2 \theta_2$$

$$P_{1f}^2 \sin^2 \theta_1 = P_{2f}^2 \sin^2 \theta_2$$

$$(P_{2i} - P_{1i})^2 + P_{1f}^2 - 2(P_{2i} - P_{1i})P_{1f} \cos \theta_1 = P_{2f}^2, \quad \frac{P_{2f}^2}{m_2} = \frac{P_{1i}^2 - P_{1f}^2}{m_1} + \frac{P_{2i}^2}{m_2}$$

$$P_{2f}^2 = \frac{m_2}{m_1} (P_{1i}^2 - P_{1f}^2) + P_{2i}^2$$

$$(P_{2i} - P_{1i})^2 + P_{1f}^2 - 2(P_{2i} - P_{1i})P_{1f} \cos \theta_1 = \frac{m_2}{m_1} (P_{1i}^2 - P_{1f}^2) + P_{2i}^2$$

$$= \frac{m_2}{m_1} P_{1i}^2 - \frac{m_2}{m_1} P_{1f}^2 + P_{2i}^2$$

$$P_{1f}^2 + \frac{m_1}{m_2} P_{1f}^2 - 2(P_{2i} - P_{1i}) \cos \theta_1 P_{1f} = \frac{m_2}{m_1} P_{1i}^2 + P_{2i}^2 - (P_{2i} - P_{1i})^2$$

$$(1 + \frac{m_1}{m_2}) P_{1f}^2 - 2(P_{2i} - P_{1i}) \cos \theta_1 P_{1f} = \frac{m_2}{m_1} P_{1i}^2 + P_{2i}^2 - (P_{2i} - P_{1i})^2$$

$$P_{1f}^2 - \frac{2(P_{2i} - P_{1i}) \cos \theta_1 P_{1f}}{1 + \gamma} + \frac{(P_{2i} - P_{1i})^2 \cos^2 \theta_1}{(1 + \gamma)^2} = \frac{\gamma P_{1i}^2 + P_{2i}^2}{1 + \gamma} - \frac{(P_{2i} - P_{1i})^2}{(1 + \gamma)^2}$$

$$\left(P_{1f} - \frac{(P_{2i} - P_{1i}) \cos \theta_1}{1 + \gamma} \right)^2 = \frac{(1 + \gamma) [\gamma P_{1i}^2 + P_{2i}^2] - (1 + \gamma)(P_{2i} - P_{1i})^2 + (P_{2i} - P_{1i})^2 \cos^2 \theta_1}{(1 + \gamma)^2} \quad \gamma = \frac{m_2}{m_1}$$

$$= \frac{[\gamma P_{1i}^2 + P_{2i}^2 + \gamma^2 P_{1i}^2 + \gamma P_{2i}^2 - \gamma(P_{2i} - P_{1i})^2 - (P_{2i} - P_{1i})^2 + (P_{2i} - P_{1i})^2 \cos^2 \theta_1]}{(1 + \gamma)^2}$$

$$= \frac{[\gamma P_{1i}^2 + P_{2i}^2 + \gamma^2 P_{1i}^2 + \gamma P_{2i}^2 - \gamma[P_{2i}^2 - 2P_{2i}P_{1i} + P_{1i}^2] - (P_{2i} - P_{1i})^2(1 - \cos^2 \theta_1)]}{(1 + \gamma)^2}$$

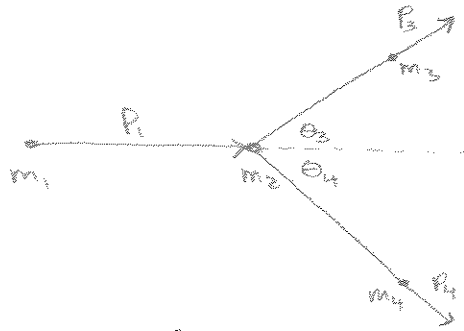
$$= \frac{[\gamma P_{1i}^2 + P_{2i}^2 + \gamma^2 P_{1i}^2 + \gamma P_{2i}^2 - \gamma P_{2i}^2 + 2\gamma P_{2i}P_{1i} - \gamma P_{1i}^2 - (P_{2i} - P_{1i})^2 \sin^2 \theta_1]}{(1 + \gamma)^2}$$

$$= \frac{[\gamma^2 P_{1i}^2 + 2\gamma P_{2i}P_{1i} + P_{2i}^2 - (P_{2i} - P_{1i})^2 \sin^2 \theta_1]}{(1 + \gamma)^2}$$

$$= \frac{[(\gamma P_{1i} + P_{2i})^2 - (P_{2i} - P_{1i})^2 \sin^2 \theta_1]}{(1 + \gamma)^2}$$

$$(1 + \gamma) P_{1f} = (P_{2i} - P_{1i}) \cos \theta_1 \pm [(\gamma P_{1i} + P_{2i})^2 - (P_{2i} - P_{1i})^2 \sin^2 \theta_1]^{1/2}$$

4-23



$$Q + \frac{P_1^2}{2m_1} = \frac{P_3^2}{2m_2} + \frac{P_4^2}{2m_4}$$

$$P_1 = P_3 \cos \theta_3 + P_4 \cos \theta_4 \quad P_3 \sin \theta_3 = P_4 \sin \theta_4$$

$$\begin{aligned} P_1 &= P_3 \cos \theta_3 + \frac{P_3 \sin \theta_3 \cos \theta_4}{\sin \theta_4} \\ &= P_3 \left(\frac{\cos \theta_3 \sin \theta_4 + \sin \theta_3 \cos \theta_4}{\sin \theta_4} \right) \end{aligned}$$

$$P_3 = \frac{P_1 \sin \theta_4}{\sin(\theta_3 + \theta_4)} \quad \sin(A+B) = \cos A \sin B + \sin A \cos B$$

$$\frac{P_4 \sin \theta_4}{\sin \theta_3} = \frac{P_1 \sin \theta_4}{\sin(\theta_3 + \theta_4)}$$

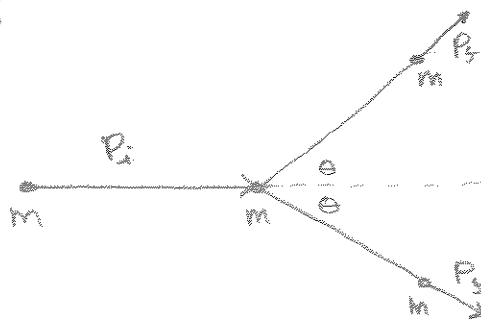
$$P_4 = \frac{P_1 \sin \theta_3}{\sin(\theta_3 + \theta_4)}$$

$$Q = \frac{P_3^2}{2m_3} + \frac{P_4^2}{2m_4} - \frac{P_1^2}{2m_1}$$

$$= \frac{P_1^2 \sin^2 \theta_4}{2m_3 \sin^2(\theta_3 + \theta_4)} + \frac{P_1^2 \sin^2 \theta_3}{2m_4 \sin^2(\theta_3 + \theta_4)} - \frac{P_1^2}{2m_1}$$

$$Q = \frac{P_1^2}{2m_1} \left[\frac{(m_1/m_3) \sin^2 \theta_4 + (m_1/m_4) \sin^2 \theta_3}{\sin^2(\theta_3 + \theta_4)} - 1 \right]$$

4-25



$$P_i = P_f \cos \theta + P_f \cos \theta$$

$$P_f \sin \theta = P_f \sin \theta$$

$$P_i = 2P_f \cos \theta$$

$$\frac{P_i^2}{2m} = \frac{P_f^2}{2m} + \frac{P_f^2}{2m} + Q$$

$$= \frac{P_f^2}{m} + Q$$

$$= \frac{P_i^2}{4m \cos^2 \theta} + Q$$

$$Q = \frac{P_i^2}{2m} - \frac{P_i^2}{4m \cos^2 \theta}$$

$$Q = \frac{P_i^2}{2m} \left(1 - \frac{1}{2} \cos^{-2} \theta \right)$$

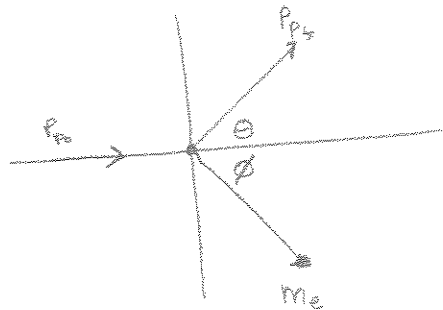
4-27

$$T_p = \frac{hc}{\lambda} \quad P_p = \frac{h}{\lambda}$$

$$T_e = mc^2 \left(\left[1 - \frac{v^2}{c^2} \right]^{-1/2} - 1 \right)$$

Conservation of momentum

$$\vec{P}_0 = \vec{P}_p + \vec{P}_e \quad \{ P_{e0} = 0 \}$$



$$P_0 = P_p \cos \theta + P_e \cos \phi$$

$$P_0 - P_p \cos \theta = P_e \cos \phi$$

$$P_0^2 - 2P_0 P_p \cos \theta + P_p^2 \cos^2 \theta = P_e^2 \cos^2 \phi$$

$$P_0^2 \sin^2 \theta = P_e^2 \sin^2 \phi$$

$$P_p \sin \theta = P_e \sin \phi$$

$$P_p^2 \sin^2 \theta = P_e^2 \sin^2 \phi$$

$$P_0^2 + P_p^2 - 2P_0 P_p \cos \theta = P_e^2 \quad (1)$$

Conservation of energy

$$T_0 + T_e = T_p + T_e$$

Expressing T in terms of P gives

$$T_p = \frac{hc}{\lambda} \quad , \quad P_p = \frac{h}{\lambda}$$

$$P_p c = \frac{hc}{\lambda} = T_p$$

$$\frac{P_{e_s}^2}{2m} = T_{e_s} + \frac{T_{e_s}^2}{2mc^2} \quad \{ \text{Eq. 4.75} \}$$

$$P_{e_s}^2 c^2 = 2mc^2 T_{e_s} + T_{e_s}^2$$

$$T_{e_s}^2 + 2mc^2 T_{e_s} = P_{e_s}^2 c^2$$

$$T_{e_s}^2 + 2mc^2 T_{e_s} + (mc^2)^2 = P_{e_s}^2 c^2 + (mc^2)^2$$

$$(T_{e_s} + mc^2)^2 = P_{e_s}^2 c^2 + (mc^2)^2$$

$$T_{e_s} = (P_{e_s}^2 c^2 + (mc^2)^2)^{1/2} - mc^2$$

$$T_{e_0} = 0$$

$$T_{P_0} = T_{P_s} + (P_{e_s}^2 c^2 + (mc^2)^2)^{1/2} - mc^2$$

$$P_{P_0} c - P_{P_s} c + mc^2 = (P_{e_s}^2 c^2 + (mc^2)^2)^{1/2}$$

$$c(P_{P_0} - P_{P_s}) + mc^2 = (P_{e_s}^2 c^2 + (mc^2)^2)^{1/2}$$

$$c^2(P_{P_0} - P_{P_s})^2 + 2c(P_{P_0} - P_{P_s})mc^2 + (mc^2)^2 = P_{e_s}^2 c^2 + (mc^2)^2$$

$$(P_{P_0} - P_{P_s})^2 + \frac{2mc^2(P_{P_0} - P_{P_s})}{c} = P_{e_s}^2 \quad (2)$$

Eliminating $P_{e_s}^2$ by using Eqs. (1) and (2) gives

$$P_{P_0}^2 + P_{P_s}^2 - 2P_{P_0}P_{P_s}\cos\theta = P_{P_0}^2 + P_{P_s}^2 - 2P_{P_0}P_{P_s} + \frac{2mc^2(P_{P_0} - P_{P_s})}{c}$$

$$-2P_{P_0}P_{P_s}\cos\theta = -2P_{P_0}P_{P_s} + \frac{2mc^2(P_{P_0} - P_{P_s})}{c}$$

$$P_{P_0}P_{P_s}(1 - \cos\theta) = \frac{mc^2(P_{P_0} - P_{P_s})}{c}$$

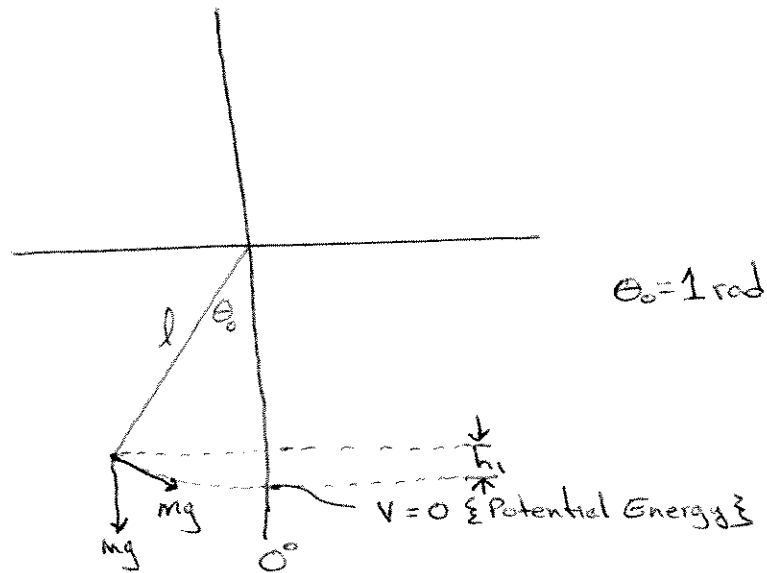
$$\frac{h}{\lambda_0} \frac{h}{\lambda_s} (1 - \cos\theta) = \frac{mc^2(\frac{h}{\lambda_0} - \frac{h}{\lambda_s})}{c}$$

$$= \frac{mc^2 h (\frac{1}{\lambda_0} - \frac{1}{\lambda_s})}{c}$$

$$\frac{h}{mc} (1 - \cos\theta) = \lambda_0 \lambda_s (\frac{1}{\lambda_0} - \frac{1}{\lambda_s})$$

$$\boxed{\frac{h}{mc} (1 - \cos\theta) = \lambda_s - \lambda_0}$$

5-11



a) Total Energy at $\theta = 0^\circ = 0 \text{ rad}$

① Potential: $mgh_1 = mgl(1 - \cos\theta_0)$

② work done by $F = mg$ along arc from θ_0 to 0

$$\begin{aligned} W &= - \int mg dr \\ &= - \int_{\theta_0}^0 mgl d\theta \\ &= +mgl\theta_0 \end{aligned}$$

③ $E_T = mgh_1 + W$
 $= mgl(1 - \cos\theta_0) + mgl\theta_0$
 $= mgl(1 - \cos\theta_0 + \theta_0) \quad \{ \theta_0 = 1 \text{ rad} \}$

$$E_T = mgl(2 - \cos(1))$$

when $\dot{\theta} = 0$ all energy is potential

$$PE = E_T$$

$$mgl(1 - \cos\theta) = mgl(2 - \cos(1))$$

$$1 - \cos\theta = 2 - \cos(1)$$

$$\cos\theta = \cos(1) - 1$$

$$\cos\theta = -.46$$

$$\boxed{\theta = 2.05 \text{ rad} = 117^\circ}$$

$$b) I\ddot{\Theta} = -mgl\sin\Theta - mgl, \quad \Theta_0 < \Theta < 0$$

$$ml^2\ddot{\Theta} = -mgl\sin\Theta - mgl$$

$$\ddot{\Theta} = -\frac{g}{l}\sin\Theta - \frac{g}{l}$$

$$\ddot{\Theta} + \frac{g}{l}\sin\Theta = -\frac{g}{l}$$

$$\ddot{\Theta} + \frac{g}{l}\Theta = -\frac{g}{l} \quad \{ \text{assume } \sin\Theta \doteq \Theta \text{ for } \Theta < 1 \}$$

$$\Theta_h = A\cos\omega_0 t + B\sin\omega_0 t, \quad \omega_0 = \left(\frac{g}{l}\right)^{1/2}$$

$$\text{let } \Theta_p = A$$

$$\frac{g}{l}A = -\frac{g}{l}$$

$$A = -1$$

$$\Theta(t) = A\cos\omega_0 t + B\sin\omega_0 t - 1$$

$$\Theta(0) = \Theta_0 = 1 = A - 1$$

$$1 = A - 1$$

$$A = 2$$

$$\dot{\Theta}(t) = -A\omega_0\sin\omega_0 t + B\omega_0\cos\omega_0 t$$

$$\dot{\Theta}(0) = 0 = B\omega_0$$

$$B = 0$$

$$\Theta = 2\cos\omega_0 t - 1$$

$$0 = 2\cos\omega_0 t - 1$$

$$\cos\omega_0 t = \frac{1}{2}$$

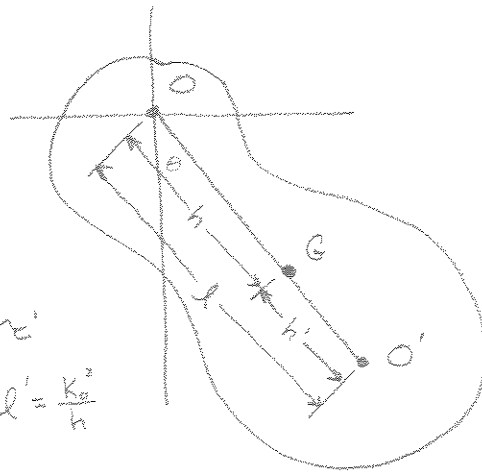
$$\omega_0 t = \cos^{-1}\left(\frac{1}{2}\right)$$

$$\omega_0 t = \frac{\pi}{3}$$

$$t = \frac{\pi}{3}\omega_0^{-1}$$

$$\boxed{t = \frac{\pi}{3}\left(\frac{l}{g}\right)^{1/2}}$$

5-13



$$a) \omega = \left(\frac{g}{l}\right)^{1/2}$$

$$\omega^2 = \frac{g}{l}$$

$$\frac{4\pi^2}{\tau^2} = \frac{g}{l}$$

$$\tau^2 = 4\pi^2 \frac{l}{g}$$

$$\tau^2 = \frac{4\pi^2}{g} \frac{K_O^2}{h}$$

$$K_O^2 = K_G^2 + h^2 \quad \{ \text{parallel axis theorem} \}$$

$$\tau^2 = \frac{4\pi^2}{g} \frac{(K_G^2 + h^2)}{h}$$

$$hh' = K_G^2$$

$$\tau^2 = \frac{4\pi^2}{g} \frac{(hh' + h^2)}{h}$$

$$= \frac{4\pi^2}{g} (h' + h)$$

$$g = \frac{4\pi^2 (h' + h)}{\tau^2}$$

$$b) \tau' = \tau(1 + \delta), \quad \delta \ll 1$$

$$l \neq l'$$

$$K_O^2 = K_G^2 + h^2, \quad K_{O'}^2 = K_G^2 + h'^2$$

$$l = \frac{K_O^2}{h}, \quad l' = \frac{K_{O'}^2}{h'}$$

$$\tau^2 = \frac{4\pi^2}{g} \frac{K_O^2}{h}$$

$$= \frac{4\pi^2}{g} \frac{(K_G^2 + h^2)}{h}$$

$$K_G^2 = \frac{\tau^2 gh}{4\pi^2} - h^2$$

$$\tau'^2 = \frac{4\pi^2}{g} \frac{K_{O'}^2}{h'}$$

$$\tau'^2 = \frac{4\pi^2}{g} \frac{(K_G^2 + h'^2)}{h'}$$

$$= \frac{4\pi^2}{g} \left[\frac{\left(\frac{\tau^2 gh}{4\pi^2} - h^2 \right) + h'^2}{h'} \right]$$

$$= \frac{\tau^2 gh}{gh'} - \frac{4\pi^2 h^2}{gh'} + \frac{4\pi^2 h'^2}{gh'}$$

$$\tau'^2 = \tau^2 (1 + \delta)^2 \approx \tau^2 (1 + 2\delta)$$

$$\tau^2 (1 + 2\delta) h' = \frac{\tau^2 gh}{g} - \frac{4\pi^2 (h^2 - h'^2)}{g}$$

$$\tau^2 [(1 + 2\delta) h' - h] = - \frac{4\pi^2}{g} (h + h')(h - h')$$

$$g [h' + 2h'\delta - h] = - \frac{4\pi^2}{\tau^2} (h + h')(h - h')$$

$$g(h' + 2h'\delta) - gh = -g(h - h')$$

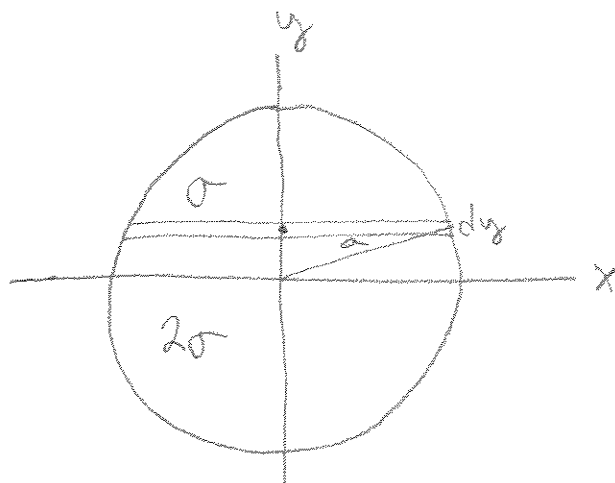
$$(h' - h) + 2h'\delta = h' - h$$

$$1 + \frac{2h'\delta}{h - h} = 1 \rightarrow$$

correction factor is

$$1 + \frac{2h'\delta}{h - h}$$

15. A circular disk of radius a lies in the xy -plane with its center at the origin. The half of the disk above the x -axis has a density σ per unit area, and the half below the x -axis has a density 2σ . Find the center of mass G , and the moments of inertia about the x -, y -, and z -axes, and about parallel axes through G . Make as much use of labor-saving theorems as possible.



$$x^2 + y^2 = a^2$$

$$x = \sqrt{a^2 - y^2}$$

$$l = 2x$$

$$= 2\sqrt{a^2 - y^2}$$

$$\boxed{\bar{x} = 0}$$

$$\bar{y} = \frac{\int \tilde{y} dm}{\int dm}$$

$$\tilde{y} = y$$

$$dm_1 = \sigma da$$

$$dm_2 = 2\sigma da$$

$$= \sigma x dy$$

$$= 2\sigma x dy$$

$$= \frac{\int_0^a y dm_1 - \int_0^{-a} y dm_2}{M_1 + M_2}$$

$$= 2\sigma(a^2 - y^2)^{1/2} dy = 4\sigma(a^2 - y^2)^{1/2} dy$$

$$M_1 = \frac{\sigma \pi a^2}{2}$$

$$M_2 = \sigma \pi a^2$$

$$= \frac{2\sigma \int_0^a y(a^2 - y^2)^{1/2} dy - 4\sigma \int_0^{-a} y(a^2 - y^2)^{1/2} dy}{\frac{3}{2} \sigma \pi a^2}$$

$$u = a^2 - y^2$$

$$du = -2y dy$$

$$-du = 2y dy$$

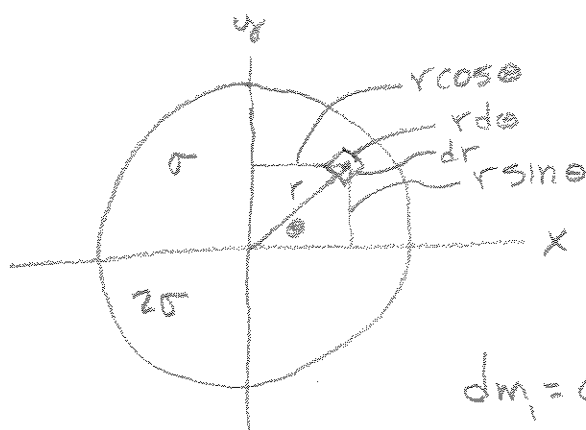
$$= \frac{-\int u^{1/2} du + 2 \int u^{1/2} du}{\frac{3}{2} \pi a^2}$$

$$= \frac{-\frac{2}{3}(a^2 - y^2)^{3/2} \Big|_0^a + \frac{4}{3}(a^2 - y^2)^{3/2} \Big|_0^{-a}}{\frac{3}{2} \pi a^2}$$

$$\bar{y} = \frac{\frac{2}{3}a^3 - \frac{4}{3}a^3}{\frac{3}{2}\pi a^2}$$

$$= \frac{-\frac{2}{3}a^3}{\frac{3}{2}\pi a^2}$$

$$\boxed{\bar{y} = \frac{-4a}{9\pi}}$$



$$dm_1 = \sigma da \quad dm_2 = 2\sigma da$$

$$= \sigma r dr d\theta = 2\sigma r dr d\theta$$

$$I_x = \int r^2 dm$$

$$= \int_0^\pi \int_0^a (r^2 \sin^2 \theta) \sigma r dr d\theta + \int_\pi^{2\pi} \int_0^a (r^2 \sin^2 \theta) 2\sigma r dr d\theta$$

$$\sin^2 \theta = \frac{1}{2}(1 - \cos 2\theta)$$

$$= \sigma \int_0^\pi \int_0^a r^3 dr \sin^2 \theta d\theta + 2\sigma \int_\pi^{2\pi} \int_0^a r^3 dr \sin^2 \theta d\theta$$

$$= \sigma \frac{a^4}{4} \int_0^\pi \frac{1}{2}(1 - \cos 2\theta) d\theta + \frac{\sigma a^4}{2} \int_\pi^{2\pi} \frac{1}{2}(1 - \cos 2\theta) d\theta$$

$$= \frac{\sigma a^4}{8} \left[\theta \Big|_0^\pi - \frac{1}{2} \sin 2\theta \Big|_0^\pi \right] + \frac{\sigma a^4}{4} \left[\theta \Big|_\pi^{2\pi} - \frac{1}{2} \sin 2\theta \Big|_\pi^{2\pi} \right]$$

$$= \frac{\sigma a^4 \pi}{8} + \frac{\sigma a^4 \pi}{4}$$

$$\boxed{I_x = \frac{3\sigma a^4 \pi}{8}}$$

$$I_y = \int_0^\pi \int_0^a (r^2 \cos^2 \theta) \sigma r dr d\theta + \int_\pi^{2\pi} \int_0^a (r^2 \cos^2 \theta) 2\sigma r dr d\theta$$

$$= \sigma \int_0^\pi \int_0^a r^3 dr \cos^2 \theta d\theta + 2\sigma \int_\pi^{2\pi} \int_0^a r^3 dr \cos^2 \theta d\theta \quad \cos^2 \theta = \frac{1}{2}(1 + \cos 2\theta)$$

$$\text{Since } \int_0^\pi \cos 2\theta d\theta = \int_\pi^{2\pi} \cos 2\theta d\theta = 0$$

$$\boxed{I_y = I_x}$$

$$I_z = I_x + I_y \quad \{ \text{perpendicular axis theorem} \}$$

$$= 2I_x$$

$$\boxed{I_z = \frac{3\sigma a^4 \pi}{4}}$$

$$\text{Since } G = (0, \frac{a}{2})$$

$$I_{Gy} = I_y$$

$$\boxed{I_{Gy} = \frac{3\sigma a^4 \pi}{8}}$$

$$\text{// axis theorem: } I_x = I_{Gx} + Mh^2$$

$$I_{Gx} = I_x - Mh^2 \quad h = \frac{4a}{9\pi}$$

$$= \frac{3\sigma a^4 \pi}{8} - \frac{3\pi a^2 \sigma \left(\frac{4a}{9\pi}\right)^2}{2}$$

$$= \frac{3\sigma a^4 \pi}{8} - \frac{3}{2} \pi a^2 \sigma \left(\frac{16a^2}{81\pi}\right)$$

$$\boxed{I_{Gx} = \frac{3\sigma a^4 \pi}{8} - \frac{8\sigma a^4}{27\pi} = (81\pi^2 - 64)\sigma a^4 / 216\pi}$$

$$I_{Gz} = I_{Gx} + I_{Gy} \quad \{ \perp \text{ axis theorem} \}$$

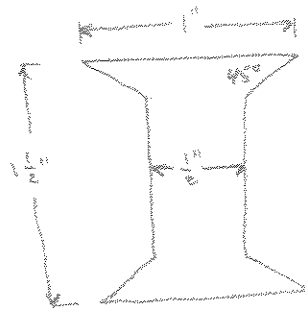
$$= \frac{(81\pi^2 - 64)\sigma a^4}{216\pi} + \frac{3\sigma a^4 \pi}{8}$$

$$= \frac{(81\pi^2 - 64)\sigma a^4}{216\pi} + \frac{81\sigma a^4 \pi^2}{216\pi}$$

$$= \frac{2(81\pi^2 - 32)\sigma a^4}{216\pi}$$

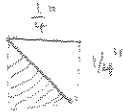
$$I_{Gz} = \frac{(81\pi^2 - 32)\sigma a^4}{108\pi}$$

5-19

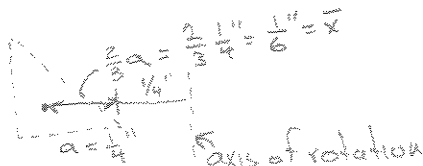
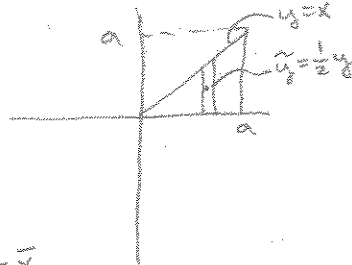


$$d_1 = 0.03''$$

Theorem of Pappus applied to triangle section



Centroid of triangle



$$r = \frac{1}{6}'' + \frac{1}{4}''$$

$$r = \frac{5}{12}''$$

$$\begin{aligned} V_{\Delta} &= A \pi (2r) \\ &= \frac{1}{2} \left(\frac{1}{4}\right)^2 \pi (2 \times \frac{5}{12}) \\ &= \frac{1}{2} \cdot \frac{1}{16} \cdot \pi \cdot \frac{5}{6} \\ &= \frac{5\pi}{192} \text{ in.}^3 \end{aligned}$$

$$\begin{aligned} V_{\square} &= A \pi (2r) \\ A &= (1'') \left(\frac{1}{4}''\right) = \frac{1}{4} \text{ in.}^2 \\ r &= \frac{1}{4}'' + \frac{1}{8}'' \quad \left\{ r = \frac{3}{8}'' \right\} \end{aligned}$$

$$V_{\square} = \frac{1}{4} \pi (2) \left(\frac{3}{8}\right)$$

$$V_{\square} = \frac{3\pi}{16} \text{ in.}^3$$

$$\begin{aligned} V &= 2V_{\Delta} + V_{\square} \\ &= \left(\frac{5\pi}{96} + \frac{3\pi}{16}\right) \text{ in.}^3 \end{aligned}$$

$$V = \frac{23\pi}{96} \text{ in.}^3$$

$$\begin{aligned} \bar{y} &= \frac{1}{M} \int \tilde{y} dm \\ &= \frac{1}{M} \int \tilde{y} \rho dA \\ &= \frac{\rho}{M} \int \tilde{y} y dx, \quad M = \rho A \\ &= \frac{1}{A} \int \frac{1}{2} y y dx \\ &= \frac{1}{2A} \int y^2 dx \\ &= \frac{1}{2A} \int_0^a x^2 dx \\ &= \frac{1}{2A} \left. \frac{x^3}{3} \right|_0^a \\ &= \frac{1}{2A} \frac{a^3}{3} \quad A = \frac{1}{2} b h \\ &= \frac{1}{2 \left(\frac{1}{2} a^2\right)} \frac{a^3}{3} \\ &= \frac{a}{3} \end{aligned}$$

Assuming 100% packing density & thread is deformable:

$$V = A \cdot l$$

$$l = \frac{V}{A} \quad A = \pi \left(\frac{d_1}{2}\right)^2$$

$$= \frac{23\pi}{96} \cdot \frac{1}{\pi \left(\frac{d_1}{2}\right)^2}$$

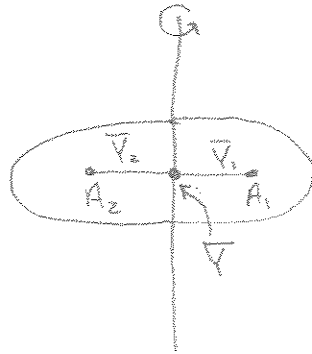
$$= \frac{23}{96} \cdot \frac{4}{d_1^2}$$

$$= \frac{23}{24} \cdot \frac{1}{(0.03)^2}$$

$$l = 1064.8 \text{ in} = 29.6 \text{ yd.} = 30 \text{ yd.}$$

5-21

Take the case of the axis of rotation passing through the axis of symmetry of a regular object



Theorem of Pappus #2

Entire object: $V = A_2 2\pi \bar{V}$

$$V = A_2 2\pi (0)$$

$$V = 0$$

Left side of object

$$V_2 = A_2 2\pi \bar{V}_2$$

Right side of object

$$V_1 = A_1 2\pi \bar{V}_1$$

Since the volume generated using $\bar{V}$ equals 0 then

$$V = V_1 + V_2$$

$$0 = V_1 + V_2$$

$$-V_1 = V_2$$

Therefore one volume is considered a negative volume. This negative volume can be viewed as a volume that erases the positive volume generated. So, in general

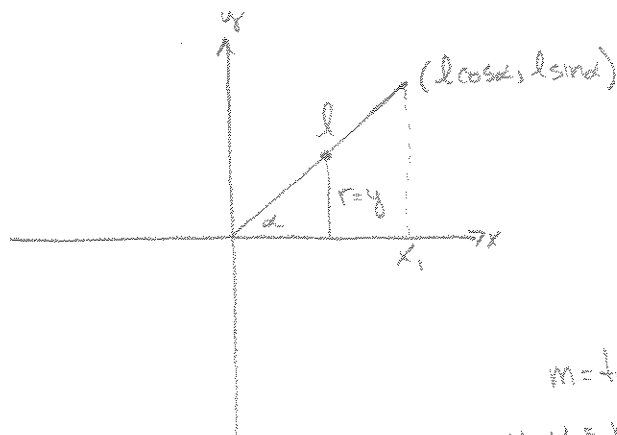


$$V = |V_1 - V_2|$$

$$V = |2\pi (A_1 \bar{V}_1 - A_2 \bar{V}_2)|$$

5-23

a)



$$dm = \rho ds$$

$$ds^2 = dx^2 + dy^2$$

$$m = \tan \alpha$$

$$y - y_1 = m(x - x_1)$$

$$y - l \sin \alpha = \tan \alpha (x - l \cos \alpha)$$

$$y - l \sin \alpha = x \tan \alpha - l \sin \alpha$$

$$y = x \tan \alpha$$

$$ds^2 = dx^2 + dx^2 \tan^2 \alpha$$

$$= dx^2 (1 + \tan^2 \alpha)$$

$$ds = dx \sec \alpha$$

$$I_x = \int r^2 dm$$

$$= \int_0^{x_1} y^2 dm$$

$$= \int_0^{x_1} (x \tan \alpha)^2 \rho ds$$

$$= \rho \tan^2 \alpha \int_0^{x_1} x^2 dx \sec \alpha$$

$$= \rho \tan^2 \alpha \sec \alpha \int_0^{x_1} x^2 dx$$

$$= \rho \tan^2 \alpha \sec \alpha \left. \frac{x^3}{3} \right|_0^{x_1} \quad x_1 = l \cos \alpha$$

$$= \rho \tan^2 \alpha \sec \alpha \frac{(l \cos \alpha)^3}{3}$$

$$= \frac{\rho l^3}{3} \frac{\sin^2 \alpha}{\cos^2 \alpha} \frac{1}{\cos \alpha} \frac{\cos^3 \alpha}{1}$$

$$I_x = \frac{\rho l^3}{3} \sin^2 \alpha$$

$$MK^2 = I_x$$

$$M = \rho l$$

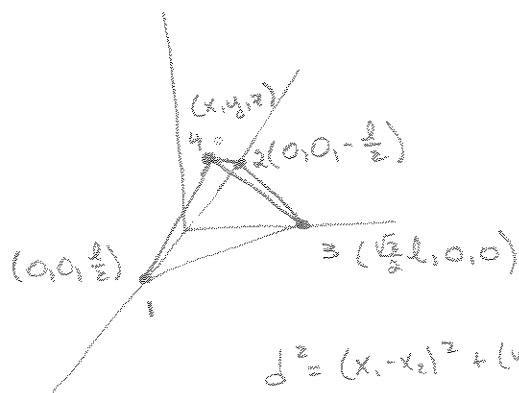
$$\rho l K^2 = \frac{\rho l^3}{3} \sin^2 \alpha$$

$$K^2 = \frac{l^2 \sin^2 \alpha}{3}$$

$$K = \frac{l \sin \alpha}{\sqrt{3}}$$

b)

1) Determine vertices coordinates



$$d^2 = (x_1 - x_2)^2 + (y_1 - y_2)^2 + (z_1 - z_2)^2$$

$$1) d_{4-1}^2 = l^2 = x^2 + y^2 + (z - \frac{l}{2})^2$$

$$2) d_{4-2}^2 = l^2 = x^2 + y^2 + (z + \frac{l}{2})^2$$

$$3) d_{4-3}^2 = l^2 = (x - \frac{\sqrt{3}}{2}l)^2 + y^2 + z^2$$

$$Eq. 1) = Eq. 2)$$

$$x^2 + y^2 + z^2 - lz + \frac{l^2}{4} = x^2 + y^2 + z^2 + lz + \frac{l^2}{4}$$

$$0 = 2lz$$

$$\boxed{z = 0}$$

$$Eq. 1) = Eq. 3); z = 0$$

$$x^2 + y^2 + \frac{l^2}{4} = x^2 - \sqrt{3}lx + \frac{3}{4}l^2 + y^2$$

$$\frac{l^2}{4} = -\sqrt{3}lx + \frac{3}{4}l^2$$

$$\frac{l^2}{2} = \sqrt{3}lx$$

$$\boxed{x = \frac{\sqrt{3}l}{6}}$$

$$Eq. 3); z = 0, x = \frac{\sqrt{3}l}{6}$$

$$l^2 = (\frac{\sqrt{3}}{6}l - \frac{\sqrt{3}}{2}l)^2 + y^2$$

$$= (\frac{\sqrt{3}l}{6} - \frac{3\sqrt{3}}{6}l)^2 + y^2$$

$$= (-\frac{2\sqrt{3}l}{6})^2 + y^2$$

$$= \frac{12l^2}{36} + y^2$$

$$\frac{36-12}{36}l^2 = y^2 \Rightarrow \frac{24}{36}l^2 = y^2 \Rightarrow y = \frac{2\sqrt{6}}{6}l \Rightarrow \boxed{\frac{\sqrt{6}}{3}l = y} \text{ pt. 4 } (\frac{\sqrt{3}}{6}l, \frac{\sqrt{6}}{3}l, 0)$$

The midpoint of each rod (centroid) is:

$$R_{12} = (0, 0, 0) \quad R_{13} = \left(\frac{\sqrt{3}}{4}l, 0, \frac{l}{4}\right) \quad R_{23} = \left(\frac{\sqrt{3}}{4}l, 0, -\frac{l}{4}\right)$$

$$R_{14} = \left(\frac{\sqrt{3}}{12}l, \frac{\sqrt{6}}{6}l, \frac{l}{4}\right) \quad R_{24} = \left(\frac{\sqrt{3}}{12}l, \frac{\sqrt{6}}{6}l, -\frac{l}{4}\right) \quad R_{34} = \left(\frac{\sqrt{3}}{3}l, \frac{\sqrt{6}}{6}l, 0\right)$$

$\bar{z} = 0$ due to symmetry.

$$\bar{x} = \frac{1}{M} \sum_{k=1}^6 M_k \bar{x}_k = \frac{1}{5} \sum_{k=1}^6 S_k \bar{x}_k$$

$$= \frac{1}{6l} \left[\frac{\sqrt{3}}{4}l^2 + \frac{\sqrt{3}}{4}l^2 + \frac{\sqrt{3}}{12}l^2 + \frac{\sqrt{3}}{12}l^2 + \frac{\sqrt{3}}{3}l^2 \right]$$

$$= \frac{l}{6} \left[\frac{2\sqrt{3}}{4} + \frac{2\sqrt{3}}{12} + \frac{\sqrt{3}}{3} \right]$$

$$= \frac{l}{6} \left[\frac{6\sqrt{3} + 2\sqrt{3} + 4\sqrt{3}}{12} \right]$$

$$= \frac{l}{6} \left[\sqrt{3} \right]$$

$$\bar{x} = \frac{\sqrt{3}l}{6}$$

$$\bar{y} = \frac{1}{5} \sum_{k=1}^6 S_k \bar{y}_k$$

$$= \frac{l}{6} \left[\frac{\sqrt{6}}{6} + \frac{\sqrt{6}}{6} + \frac{\sqrt{6}}{6} \right]$$

$$= \frac{l}{6} \left[\frac{\sqrt{6}}{2} \right]$$

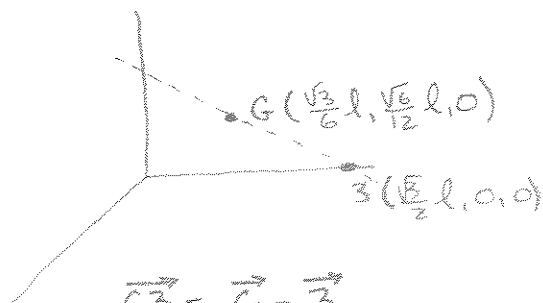
$$\bar{y} = \frac{\sqrt{6}l}{12}$$

Centroid of object:

$$\bar{x}, \bar{y}, \bar{z} = \frac{\sqrt{3}l}{6}, \frac{\sqrt{6}l}{12}, 0$$

Axis of Rotation:

For convenience choose vertex 3:

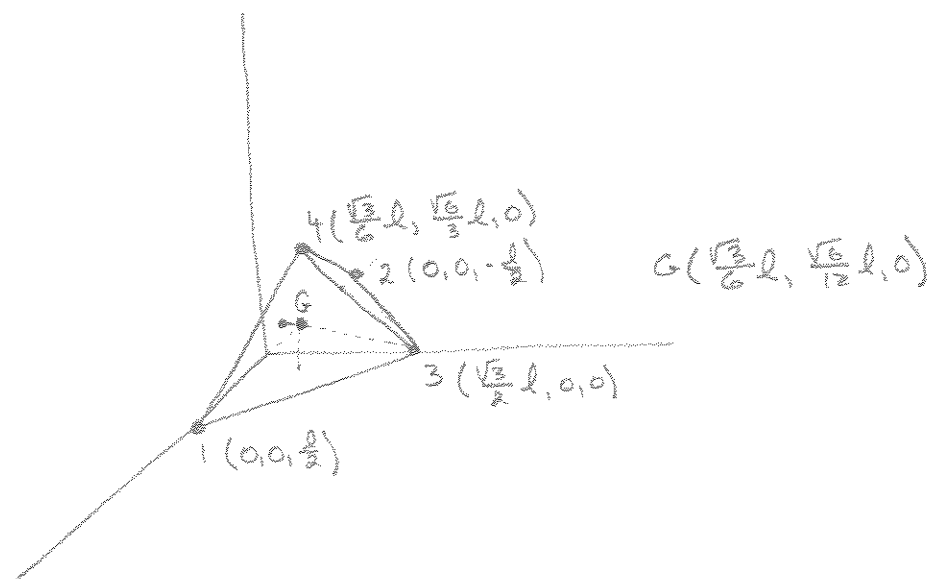


$$\vec{G3} = \vec{r} - \vec{r}_3$$

$$= \left(\frac{\sqrt{3}}{6}l - \frac{\sqrt{3}}{2}l\right)\hat{x} + \frac{\sqrt{6}}{12}l\hat{y}$$

$$\vec{G3} = -\frac{\sqrt{3}}{3}l\hat{x} + \frac{\sqrt{6}}{12}l\hat{y}$$

(4)



$$\vec{13} = \vec{1} - \vec{3} = -\frac{\sqrt{3}}{2}l\hat{i} + \frac{1}{2}l\hat{z} ; \vec{23} = \vec{2} - \vec{3} = -\frac{\sqrt{3}}{2}l\hat{i} - \frac{1}{2}l\hat{z} ; \vec{43} = \vec{4} - \vec{3} = \left(\frac{\sqrt{3}}{6} - \frac{\sqrt{3}}{2}\right)l\hat{i} + \frac{\sqrt{6}}{3}l\hat{j} = -\frac{\sqrt{3}}{3}l\hat{i} + \frac{\sqrt{6}}{3}l\hat{j}$$

Ans of rotation: $\vec{G3} = -\frac{\sqrt{3}}{3}l\hat{i} + \frac{\sqrt{6}}{12}l\hat{j}$

$$\cos\alpha = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|}$$

$$\begin{aligned} \cos\alpha_1 &= \frac{\vec{G3} \cdot \vec{13}}{|\vec{G3}| |\vec{13}|} \\ &= \frac{-\frac{\sqrt{3}}{3} \cdot -\frac{\sqrt{3}}{2}l^2 + 0 + 0}{\frac{\sqrt{6}}{4}l^2} \end{aligned}$$

$$= \frac{3}{6} \cdot \frac{4}{\sqrt{6}}$$

$$= \frac{2}{\sqrt{6}}$$

$$= \frac{\sqrt{6}}{3}$$

$$\cos^2\alpha_1 = \frac{6}{9} = \frac{2}{3}$$

$$\sin^2\alpha_1 = 1 - \cos^2\alpha_1$$

$$= 1 - \frac{2}{3}$$

$$\sin\alpha_1 = \frac{1}{3}$$

$$\sin\alpha_1 = \frac{\sqrt{3}}{3}$$

$$|\vec{G3}| = \left(\frac{3}{9} + \frac{6}{144}\right)^{1/2}l$$

$$= \left(\frac{1}{3} + \frac{1}{24}\right)^{1/2}l$$

$$= \left(\frac{9}{24}\right)^{1/2}l$$

$$|\vec{G3}| = \frac{3l}{\sqrt{24}} = \frac{3\sqrt{6}l}{24} = \frac{2\sqrt{6}l}{8} = \frac{\sqrt{6}}{4}l$$

$$\cos\alpha_2 = \frac{\vec{G3} \cdot \vec{23}}{|\vec{G3}| |\vec{23}|} = \cos\alpha_1$$

$$\sin\alpha_2 = \sin\alpha_1 = \frac{\sqrt{3}}{3}$$

$$\begin{aligned} \cos\alpha_3 &= \frac{\vec{G3} \cdot \vec{43}}{|\vec{G3}| |\vec{43}|} = \frac{\frac{3}{9} + \frac{6}{36}}{\frac{\sqrt{6}}{4}} = \frac{\frac{1}{3} + \frac{1}{6}}{\frac{\sqrt{6}}{4}} = \frac{\frac{1}{2} \cdot \frac{4}{\sqrt{6}}}{\frac{\sqrt{6}}{4}} \\ &= \frac{2}{\sqrt{6}} \\ &= \frac{\sqrt{6}}{3} \end{aligned}$$

$$\sin\alpha_1 = \sin\alpha_3 = \sin\alpha_1 = \frac{\sqrt{3}}{3}$$

(5)

Determine angle between axis of rotation and $\vec{4I}$

$$\cos \alpha = \frac{\vec{G3} \cdot \vec{4I}}{\frac{\sqrt{6}}{4} l^2}$$

$$\vec{4I} = \vec{4} - \vec{I}$$

$$= \frac{\sqrt{3}}{6} l \vec{x} + \frac{\sqrt{6}}{3} l \vec{y} - \frac{l}{2} \vec{z}$$

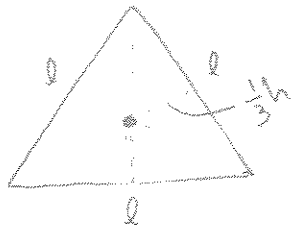
$$= \frac{\left(-\frac{\sqrt{3}}{3} l\right)\left(\frac{\sqrt{3}}{6} l\right) + \left(\frac{\sqrt{6}}{12} l\right)\left(\frac{\sqrt{6}}{3} l\right) + 0}{\frac{\sqrt{6}}{4} l^2}$$

$$= \frac{-\frac{3}{18} + \frac{6}{36}}{\frac{\sqrt{6}}{4}}$$

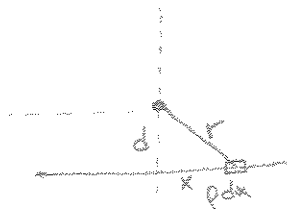
$$= \frac{-\frac{3}{18} + \frac{3}{18}}{\frac{\sqrt{6}}{4}}$$

$$= 0$$

Therefore, $\vec{G3} \perp \vec{4I}$, $\vec{G3} \perp \vec{I2}$, $\vec{G3} \perp \vec{42}$



$$\begin{aligned} h^2 &= l^2 - \frac{l^2}{4} \\ &= \frac{3l^2}{4} \\ &= \frac{l\sqrt{3}}{2} \end{aligned}$$



$$\begin{aligned} d &= \frac{1}{3} h \\ &= \frac{l\sqrt{3}}{6} \end{aligned}$$

$$r^2 = x^2 + d^2 \quad dm = \rho dx$$

$$\begin{aligned} I &= \int r^2 dm \\ &= \rho \int_{-l/2}^{l/2} (x^2 + d^2) dx \\ &= \rho \left[\int_{-l/2}^{l/2} x^2 dx + d^2 \int_{-l/2}^{l/2} dx \right] \\ &= \rho \left[\frac{x^3}{3} \Big|_{-l/2}^{l/2} + d^2 x \Big|_{-l/2}^{l/2} \right] \\ &= \rho \left[\frac{l^3}{24} + \frac{l^3}{24} + d^2 \frac{l}{2} \right] \\ &= \rho \left[\frac{l^3}{12} + d^2 l \right] \end{aligned}$$

$$\begin{aligned} I &= \frac{\rho l^3}{12} + \rho \left(\frac{l\sqrt{3}}{6} \right)^2 l \\ &= \frac{\rho l^3}{12} + \frac{\rho l^3}{36} \\ &= \frac{\rho l^3}{12} + \frac{\rho l^3}{12} \\ &= \frac{\rho l^3}{6} \end{aligned}$$

Each rod is oriented the same with respect to the axis of rotation.

⑥

$$\begin{aligned} I_{\Delta} &= 3I \\ &= 3 \frac{Ml^2}{6} \\ &= \frac{Ml^2}{2} \end{aligned}$$

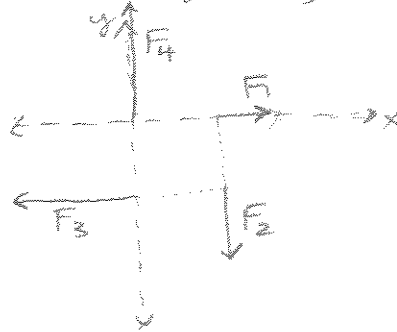
$$\begin{aligned} I_{\text{Pyr.}} &= I_{\Delta} + 3I_{\Delta} \\ &= \frac{Ml^2}{2} + 3 \frac{Ml^2}{3} \sin^2 \alpha \\ &= Ml^2 \left[\frac{1}{2} + \sin^2 \alpha \right] \\ &= Ml^2 \left[\frac{1}{2} + \frac{1}{3} \right] \\ &= Ml^2 \left(\frac{5}{6} \right) \end{aligned}$$

$$\begin{aligned} \sin^2 \alpha &= \sin^2 \alpha_1 \\ &= \left(\frac{\sqrt{3}}{3} \right)^2 \\ &= \frac{1}{3} \end{aligned}$$

$$I_{\text{Pyr.}} = \frac{5}{6} Ml^2$$

5.25

$$F_1 = 1 \text{ kg-wt}, F_2 = 2 \text{ kg-wt}, F_3 = 3 \text{ kg-wt}, F_4 = 4 \text{ kg-wt}$$



$$\vec{F} = \sum_i \vec{F}_i$$

$$(\vec{r} - \vec{r}_0) \times \vec{F} = \sum_i (\vec{r}_i - \vec{r}_0) \times \vec{F}_i$$

$$\begin{aligned} \vec{F} &= \sum_i \vec{F}_i; F_x = F_1 - F_3 & F_y &= -F_2 + F_4 \\ &= 1 - 3 & &= -2 + 4 \\ &= -2 & &= 2 \end{aligned}$$

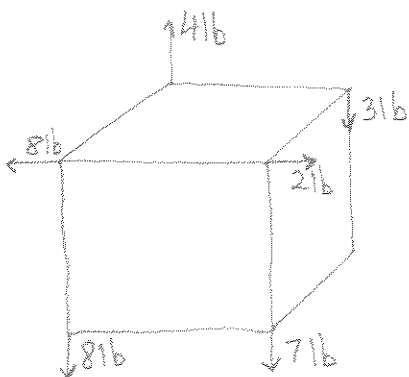
$$\vec{F} = -2\hat{x} + 2\hat{y}$$

$$-\vec{F} = \text{equilibrant}$$

$$\boxed{-\vec{F} = \vec{F}_{eq} = 2\hat{x} - 2\hat{y}}$$

5-27

①



1ft x 1ft x 1ft cube

a) Coordinate system at center of cube

$$F_1 = 4\text{lb}$$

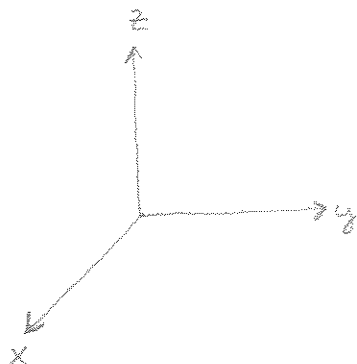
$$F_2 = 3\text{lb}$$

$$F_3 = 7\text{lb}$$

$$F_4 = 8\text{lb (down)}$$

$$F_5 = 8\text{lb}$$

$$F_6 = 2\text{lb}$$

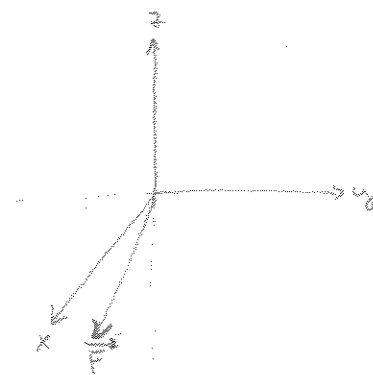


$$\vec{F}_1 = 4\hat{z} \quad \vec{F}_2 = -3\hat{z} \quad \vec{F}_3 = -7\hat{z} \quad \vec{F}_4 = -8\hat{z} \quad \vec{F}_5 = -8\hat{y} \quad \vec{F}_6 = 2\hat{y}$$

$$\vec{F}_0 = \sum_i \vec{F}_i$$

$$= 0\hat{x} + (-8+2)\hat{y} + (4-3-7-8)\hat{z}$$

$$\boxed{\vec{F}_0 = 0\hat{x} - 6\hat{y} - 14\hat{z}}$$



Torque at center of cube :

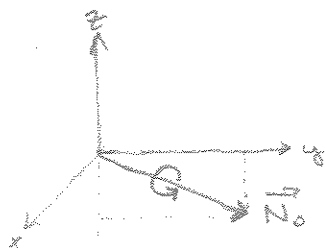
$$\vec{N}_0 = \sum_i \vec{N}_{0i}$$

$$= \sum_i \vec{r}_{0i} \times \vec{F}_i$$

$$= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ -\frac{1}{2} & -\frac{1}{2} & \frac{1}{2} \\ 0 & 0 & 4 \end{vmatrix} + \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ -\frac{1}{2} & \frac{1}{2} & \frac{1}{2} \\ 0 & 0 & -3 \end{vmatrix} + \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{1}{2} & \frac{1}{2} & -\frac{1}{2} \\ 0 & 0 & -7 \end{vmatrix} + \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{1}{2} & -\frac{1}{2} & -\frac{1}{2} \\ 0 & 0 & -8 \end{vmatrix} + \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{1}{2} & -\frac{1}{2} & \frac{1}{2} \\ 0 & -8 & 0 \end{vmatrix} + \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \\ 0 & 2 & 0 \end{vmatrix}$$

$$= -2\hat{x} + 2\hat{y} + \frac{3}{2}\hat{x} - \frac{3}{2}\hat{y} + \frac{7}{2}\hat{x} + \frac{7}{2}\hat{y} + 4\hat{x} + 4\hat{y} + 4\hat{x} - 4\hat{z} + -\hat{x} + \hat{z}$$

$$\vec{N}_0 = 0\hat{x} + 8\hat{y} - 3\hat{z}$$



Let O' be the right front corner and P' be the adjacent rear corner. Then

$$\begin{aligned}\vec{r} &= \vec{P}' - \vec{O}' \\ &= -\frac{1}{2}\hat{x} + \frac{1}{2}\hat{y} + \frac{1}{2}\hat{z} - \left(\frac{1}{2}\hat{x} + \frac{1}{2}\hat{y} + \frac{1}{2}\hat{z}\right) \\ &= -\hat{x}\end{aligned}$$

$$\vec{N}_O = \vec{r} \times \vec{F}_C \text{ where } \vec{F}_C \text{ acts at } P'$$

$$= -\hat{x} \times \vec{F}_C$$

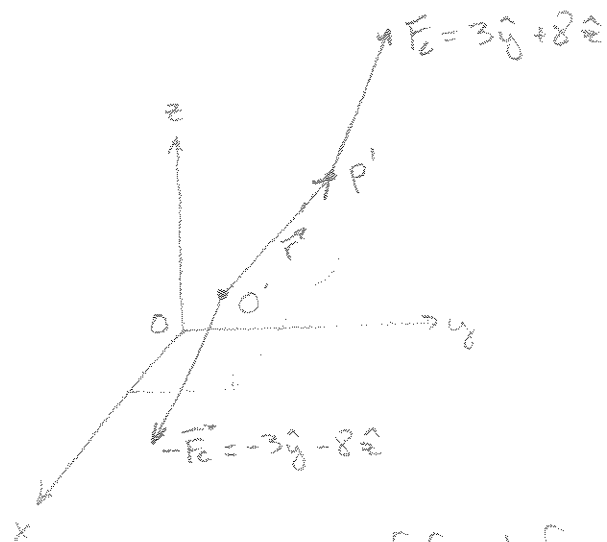
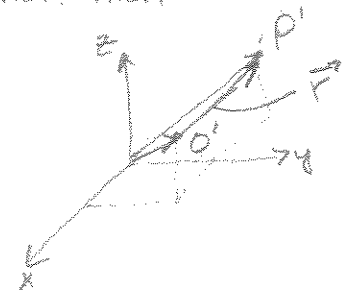
$$= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ -1 & 0 & 0 \\ F_x & F_y & F_z \end{vmatrix}$$

$$= F_z \hat{y} - F_y \hat{z}$$

$$8\hat{y} - 3\hat{z} = F_z \hat{y} - F_y \hat{z}$$

$$F_z = 8 \quad F_y = 3 \quad F_x = 0$$

$$\begin{aligned}\vec{F}_{C_{P'}} &= 0\hat{x} + 3\hat{y} + 8\hat{z} \\ -\vec{F}_{C_O} &= 0\hat{x} - 3\hat{y} - 8\hat{z}\end{aligned}$$



b) Compute the equivalent couple about O and center of front face P''

$$\begin{aligned}\vec{r} &= \vec{P}'' - \vec{O} \\ &= \frac{1}{2}\hat{x}\end{aligned}$$

$$\vec{N}_O = \vec{r} \times \vec{F}_C \text{ where } \vec{F}_C \text{ acts at } P''$$

$$= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{1}{2} & 0 & 0 \\ F_x & F_y & F_z \end{vmatrix}$$

$$= -\frac{F_z}{2}\hat{y} + \frac{F_y}{2}\hat{z}$$

$$8\hat{y} - 3\hat{z} = -\frac{F_z}{2}\hat{y} + \frac{F_y}{2}\hat{z}$$

$$F_z = -16 \quad F_y = -6$$

$$\vec{F}_{C_{P''}} = 0\hat{x} - 6\hat{y} - 16\hat{z}$$

$$-\vec{F}_{C_0} = 0\hat{x} + 6\hat{y} + 16\hat{z}$$

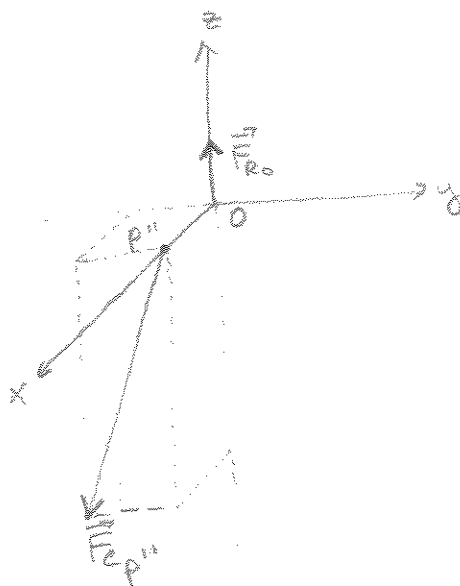
$-\vec{F}_{C_0}$ acts within the y - z plane through the cube center O

$$\vec{F}_{R_0} = \vec{F} + (-\vec{F}_{C_0})$$

$$= 0\hat{x} - 6\hat{y} - 14\hat{z} + 0\hat{x} + 6\hat{y} + 16\hat{z}$$

$$\vec{F}_{R_0} = 0\hat{x} + 0\hat{y} + 2\hat{z}$$

$$\boxed{\begin{aligned}\vec{F}_{R_0} &= 0\hat{x} + 0\hat{y} + 2\hat{z} \\ \vec{F}_{C_{P''}} &= 0\hat{x} - 6\hat{y} - 16\hat{z}\end{aligned}}$$



c) The force $\vec{F}$ at O is

$$\vec{F}_0 = 0\hat{x} - 6\hat{y} - 14\hat{z}$$

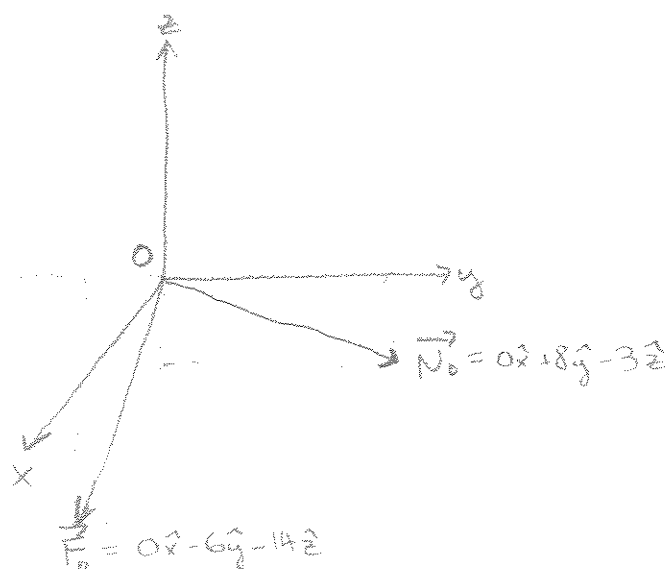
The torque $\vec{N}$ at O is

$$\vec{N}_0 = 0\hat{x} + 8\hat{y} - 3\hat{z}$$

Let $\vec{r}$ be a vector $\perp$ to $\vec{N}_0$.

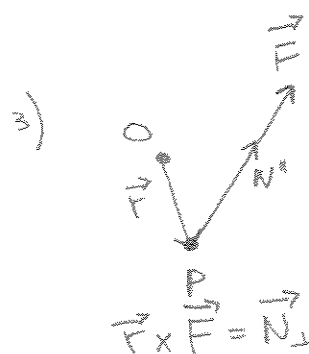
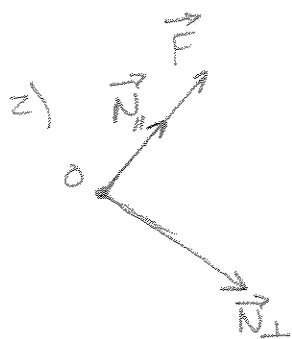
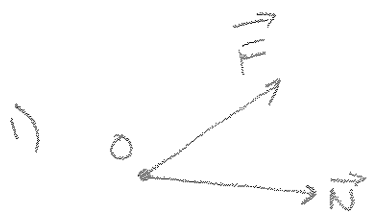
$\vec{r} = a\hat{x}$ since $\hat{x} \perp$ to y - z plane.

Determine the components of $\vec{N}_0$ parallel and normal to $\vec{F}_0$



(4)

Steps to find a single force plus a torque parallel to the force



$$\vec{F}_0 = -6\hat{y} - 14\hat{z} \quad \vec{N}_0 = 8\hat{y} - 3\hat{z}$$

Component of $\vec{N}_0$ on $\vec{F}_0$

$$N_{||} = |\vec{N}_0| \cos \theta = \frac{\vec{F}_0 \cdot \vec{N}_0}{|\vec{F}_0|}$$

$$= \frac{-48 + 42}{(36 + 196)^{1/2}}$$

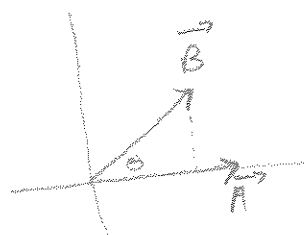
$$= \frac{-6}{\sqrt{232}}$$

$$\vec{N}_{||} = N_{||} \hat{F}_0$$

$$= \frac{-6}{\sqrt{232}} \frac{-6\hat{y} - 14\hat{z}}{\sqrt{232}}$$

$$= \frac{36}{232} \hat{y} + \frac{84}{232} \hat{z}$$

$$\boxed{\vec{N}_{||} = \frac{9}{58} \hat{y} + \frac{21}{58} \hat{z}}$$



$$|\vec{A}| |\vec{B}| \cos \theta = \vec{A} \cdot \vec{B}$$

$$|\vec{B}| \cos \theta = \frac{\vec{A} \cdot \vec{B}}{|\vec{A}|} = B_{||}$$

$$N_{\perp}^2 = N_0^2 - N_{||}^2$$

$$= 73 - \frac{522}{58^2}$$

$$= \frac{73 \cdot 58^2 - 522}{58^2}$$

$$= \frac{73 \cdot 58^2 - 9 \cdot 58}{58^2}$$

$$N_{\perp} = \frac{\sqrt{58(73 \cdot 58 - 9)}}{58}$$

$$N_0^2 = 64 + 9 = 73$$

$$N_{||}^2 = \frac{81 + 441}{58^2} = \frac{522}{58^2}$$

$\vec{r} = r \hat{x}$ since $\vec{F}_0$ and $\vec{N}_0$ are in y-z plane, and $r \hat{x} \times \vec{F}_0$ is in the $\vec{N}_{\perp}$ direction.

$$|\vec{r}| = \frac{|\vec{N}_{\perp}|}{|\vec{F}_0|} = \frac{N_{\perp}}{F_0}$$

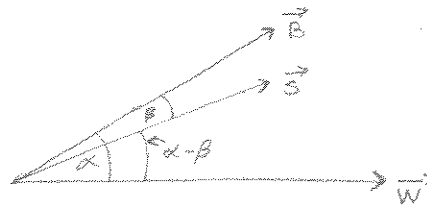
$$= \frac{\sqrt{58(73 \cdot 58 - 9)}}{58 \sqrt{232}}$$

$$= \frac{(73 \cdot 58 - 9)^{1/2}}{58 \cdot 2}$$

$$|\vec{r}| = \frac{65}{116}$$

$$\boxed{\vec{r} = \frac{65}{116} \hat{x}}$$

5-29



i) Component of $\vec{W} \perp$ to $\vec{S}$

$$W_{\perp} = |\vec{W}| \sin \theta$$

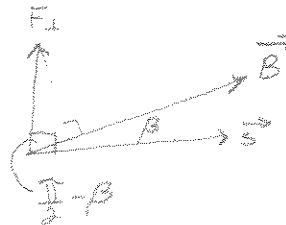
$$= W \sin(\alpha - \beta)$$

$$F_{\perp} = KW_{\perp}$$

$$= KW \sin(\alpha - \beta)$$

Component of $F_{\perp} \parallel$ to $\vec{B}$

$$F_{\parallel B} = F_{\perp} \cos\left(\frac{\pi}{2} - \beta\right)$$



$$F_{\parallel B} = KW \sin(\alpha - \beta) \cos\left(\frac{\pi}{2} - \beta\right)$$

$$= KW \sin(\alpha - \beta) \sin \beta$$

$$\sin(\alpha - \beta) = \sin \alpha \cos \beta - \cos \alpha \sin \beta$$

$$= KW \sin \beta (\sin \alpha \cos \beta - \cos \alpha \sin \beta)$$

$$= KW [\sin \alpha \sin \beta \cos \beta - \cos \alpha \sin^2 \beta]$$

$$\frac{dF_{\parallel B}}{d\beta} = KW [\sin \alpha (-\sin^2 \beta + \cos^2 \beta) - 2 \cos \alpha \sin \beta \cos \beta]$$

$$0 = \sin \alpha (\cos^2 \beta - \sin^2 \beta) - 2 \cos \alpha \sin \beta \cos \beta$$

$$2 \cos \alpha \sin \beta \cos \beta = \sin \alpha (\cos^2 \beta - \sin^2 \beta)$$

$$\frac{2 \sin \beta \cos \beta}{\cos^2 \beta - \sin^2 \beta} = \tan \alpha$$

$$2 \sin \beta \cos \beta = \sin 2\beta$$

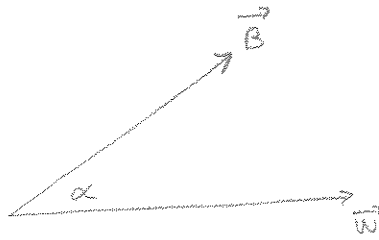
$$\cos^2 \beta = \frac{1}{2}(1 + \cos 2\beta)$$

$$\sin^2 \beta = \frac{1}{2}(1 - \cos 2\beta)$$

$$\frac{\sin 2\beta}{\cos 2\beta} = \tan \alpha$$

$$2\beta = \alpha$$

$$\boxed{\beta = \frac{1}{2}\alpha}$$



ii) Component of $\vec{B} \parallel$ to $\vec{W}$

$$B_{||} = W \cos \alpha$$

$$\vec{f} = -k_1 \vec{V} \quad \text{where } \vec{V} \text{ is boat velocity}$$

$$F_{||B} = k_2 W \sin(\alpha - \beta) \sin \beta, \quad \beta = \frac{1}{2} \alpha$$

Component of boat velocity $\parallel$ to wind

$$V_{B||} = V_B \cos \alpha$$

At maximum velocity

$$f = F_{||B}$$

$$k_1 V_B = k_2 W \sin(\alpha - \beta) \sin \beta$$

$$= k_2 W \sin(\alpha/2) \sin \alpha/2, \quad \beta = \frac{1}{2} \alpha$$

$$= k_2 W \sin^2(\alpha/2)$$

$$V_B = \frac{k_2}{k_1} W \sin^2(\alpha/2)$$

$$V_{B||} = \frac{k_2}{k_1} W \sin^2(\alpha/2) \cos \alpha$$

$$\frac{dV_{B||}}{d\alpha} = \frac{k_2}{k_1} W \left[-\sin^2(\alpha/2) \sin \alpha + \cos \alpha \sin(\alpha/2) \cos(\alpha/2) \right]$$

$$0 = -\sin^2(\alpha/2) \sin \alpha + \cos \alpha \sin(\alpha/2) \cos(\alpha/2)$$

$$\sin^2(\alpha/2) \sin \alpha = \cos \alpha \sin(\alpha/2) \cos(\alpha/2)$$

$$\frac{\sin(\alpha/2)}{\cos(\alpha/2)} = \frac{\cos \alpha}{\sin \alpha}$$

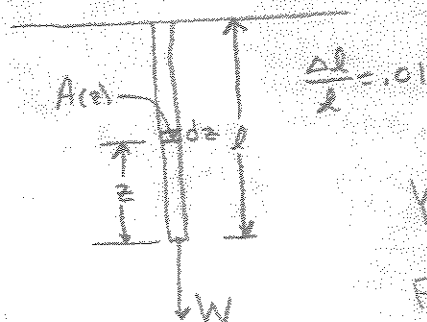
$$\tan 2u = \frac{2 \tan u}{1 - \tan^2 u}$$

$$\tan(\alpha/2) = \frac{1 - \tan^2(\alpha/2)}{2 \tan(\alpha/2)}$$

$$2 \tan^2(\alpha/2) = 1 - \tan^2(\alpha/2) \Rightarrow \tan(\alpha/2) = \frac{1}{\sqrt{3}} \Rightarrow \alpha/2 = 30^\circ \Rightarrow$$

$$\boxed{\alpha = 60^\circ}$$

5-31



$$Y = \frac{F l}{A \Delta l}$$

F is force stretching the cable

The total force on the cable element is

$$F(z) = W + w \int_0^z A(z) dz$$

Using Young's modulus

$$Y = \frac{F l}{A \Delta l}$$

$$A(z) = \frac{F(z)}{.01 Y}$$

$$= \frac{100 F(z)}{Y}$$

$$A(z) = \frac{100}{Y} \left[W + w \int_0^z A(z) dz \right]$$

$$\frac{dA}{dz} = \frac{100 w}{Y} A$$

$$\frac{dA}{A} = \frac{100 w}{Y} dz$$

$$\int_{A_0}^A \frac{dA}{A} = \int_0^z \frac{100 w}{Y} dz$$

$$\ln A - \ln A_0 = \frac{100 w z}{Y}$$

$$\ln \frac{A}{A_0} = \frac{100 w z}{Y}$$

$$\frac{A}{A_0} = e^{\frac{100 w z}{Y}}$$

$$A = A_0 e^{\frac{100 w z}{Y}}$$

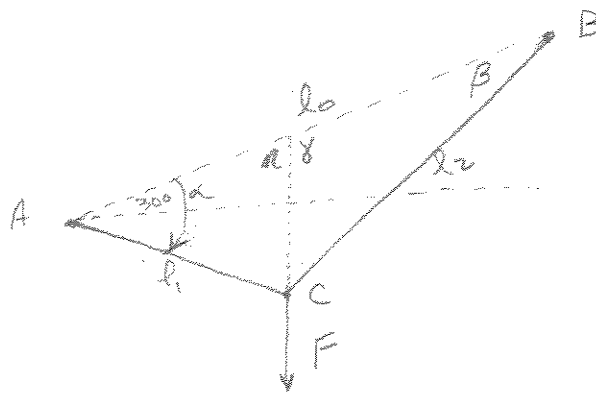
At $z=0$ the force is W

$$A_0 = A(0) = \frac{100 F(0)}{Y}$$

$$A_0 = \frac{100 W}{Y}$$

$$A = \frac{100 W}{Y} e^{\frac{100 w z}{Y}}$$

5-33



$$\begin{aligned} l_0 &= 15 \\ l_1 &= 8 \\ l_2 &= 12 \end{aligned} \quad \left. \begin{array}{l} l_1 + l_2 = 20 \end{array} \right\}$$

$$F = 2000$$

$$\gamma = 120^\circ$$

Law of cosines:

$$l_2^2 = l_0^2 + l_1^2 - 2l_0l_1 \cos \alpha$$

$$l_1^2 = l_0^2 + l_2^2 - 2l_0l_2 \cos \beta$$

$$\cos \alpha = \frac{l_0^2 + l_1^2 - l_2^2}{2l_0l_1}$$

$$\cos \beta = \frac{l_0^2 + l_2^2 - l_1^2}{2l_0l_2}$$

$$= \frac{15^2 + 8^2 - 12^2}{2(15)(8)}$$

$$= \frac{15^2 + 12^2 - 8^2}{2(15)(12)}$$

$$= \frac{145}{240}$$

$$= \frac{305}{360}$$

$$\alpha = \cos^{-1}\left(\frac{29}{48}\right)$$

$$\beta = \cos^{-1}\left(-\frac{61}{72}\right)$$

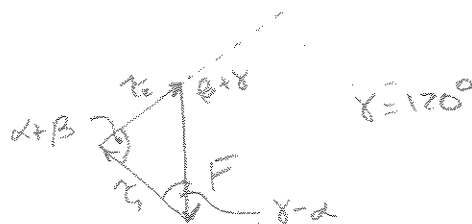
$$\alpha = 52.83^\circ$$

$$\beta = 32.09^\circ$$

a) Position of C and cable tensions

$$\begin{aligned} \alpha - 30^\circ &= 52.83^\circ - 30^\circ \\ &= 22.83^\circ \end{aligned}$$

C is 8 ft from A and
22.83° below horizontal



$$T_1 = F \frac{\sin(\beta + \gamma)}{\sin(\alpha + \beta)} \quad T_2 = F \frac{\sin(\gamma - \alpha)}{\sin(\alpha + \beta)}$$

$$= 2000 \frac{\sin(152.09^\circ)}{\sin(84.92^\circ)} = 2000 \frac{\sin(67.17^\circ)}{\sin(84.92^\circ)}$$

$$T_1 = 9401 \text{ lb} \quad T_2 = 1851 \text{ lb}$$

$$b) d = \frac{1}{2}'' , Y = 5 \times 10^5 \frac{lb}{in^2}$$

$$l_1 = l'_1 (1 + k \tau_1) \quad l_2 = l'_2 (1 + k \tau_2) \quad \frac{1}{k} = Y A = \pi \left(\frac{d}{2}\right)^2 Y$$

$$k = \frac{4}{\pi d^2 Y}$$

$$= \frac{4}{\pi \left(\frac{1}{2}\right)^2 (5 \times 10^5)}$$

$$= \frac{16}{\pi (5 \times 10^5)}$$

$$= 1.02 \times 10^{-5}$$

zero approximation from a)

$$l_1 = 8 = l'_1 \quad l_2 = 12 = l'_2, \quad \tau_1 = 939, \quad \tau_2 = 1850$$

first approximation

$$l_1 = 8(1 + (1.02 \times 10^{-5})(940)) \quad l_2 = 12(1 + (1.02 \times 10^{-5})(1851))$$

$$= 8.077$$

$$= 12.226$$

$$\cos \alpha = \frac{15^2 + (8.077)^2 - (12.226)^2}{2(15)(8.077)}$$

$$= .5809$$

$$\alpha = 54.48^\circ$$

$$\tau_1 = F \frac{\sin(\beta + \gamma)}{\sin(\alpha + \beta)}$$

$$= 2000 \frac{\sin(32.53 + 120^\circ)}{\sin(54.48^\circ + 32.53^\circ)}$$

$$\tau_1 = 924$$

$$\cos \beta = \frac{15^2 + (12.226)^2 - (8.077)^2}{2(15)(12.226)}$$

$$= -.8431$$

$$\beta = 32.53^\circ$$

$$\tau_2 = F \frac{\sin(\gamma - \alpha)}{\sin(\alpha + \beta)}$$

$$= 2000 \frac{\sin(120^\circ - 54.48^\circ)}{\sin(54.48^\circ + 32.53^\circ)}$$

$$\tau_2 = 1823$$

second approximation

$$l_1 = 8.077(1 + (1.02 \times 10^{-5})(924))$$

$$= 8.082$$

$$l_2 = 12.226(1 + (1.02 \times 10^{-5})(1823))$$

$$= 12.460$$

$$\cos \alpha = \frac{15^2 + (8.082)^2 - (12.460)^2}{2(15)(8.082)}$$

$$\alpha = 56.15^\circ$$

$$\tau_1 = 2000 \frac{\sin(32.54 + 120^\circ)}{\sin(56.15^\circ + 32.54^\circ)}$$

$$\tau_1 = 921.16$$

$$\cos \beta = \frac{15^2 + (12.460)^2 - (8.082)^2}{2(15)(12.460)}$$

$$\beta = 32.59^\circ$$

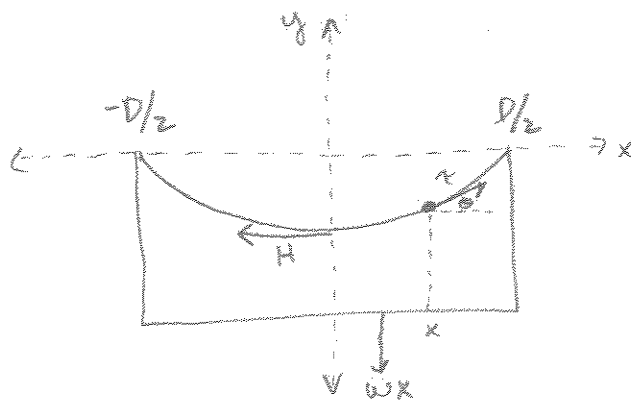
$$\tau_2 = 2000 \frac{\sin(120^\circ - 56.15^\circ)}{\sin(56.15^\circ + 32.59^\circ)}$$

$$\tau_2 = 1796.16$$

$$\alpha - 30^\circ = 26.15^\circ$$

C is 8.082 ft from A and 26.15° below horizontal

5-35



$$T \sin \theta = wx$$

$$T \cos \theta = H$$

$$\tan \theta = \frac{w}{H} x$$

$$\frac{dy}{dx} = \frac{w}{H} x$$

$$dy = \frac{w}{H} x dx$$

$$y = \frac{w}{2H} x^2 + \alpha$$

An endpoint is $(0, \frac{D}{2})$

$$0 = \frac{w}{2H} \left(\frac{D}{2}\right)^2 + \alpha$$

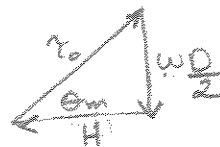
$$\alpha = -\frac{wD^2}{8H}$$

$$y = \frac{w}{2H} x^2 - \frac{wD^2}{8H}$$

$$y = \frac{w}{2H} \left(x^2 - \frac{D^2}{4}\right)$$

The maximum tension, T_0 , will occur at maximum θ , the end of the cable.

$$y = \frac{w}{2(4T_0^2 - w^2D^2)^{1/2}} \left(x^2 - \frac{D^2}{4}\right)$$



$$T_0^2 = \frac{w^2D^2}{4} + H^2$$

$$4H^2 = 4T_0^2 - w^2D^2$$

$$H = \frac{(4T_0^2 - w^2D^2)^{1/2}}{2}$$

$$y = w \left(x^2 - \frac{D^2}{4}\right) (4T_0^2 - w^2D^2)^{-1/2}$$

5-37

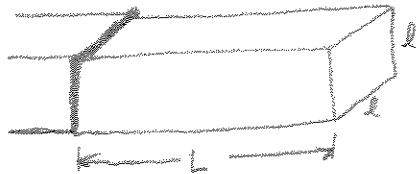
$$Eq(5.165) \quad y = -\frac{L^3}{YK^2A} \left[\frac{1}{8}W + \frac{1}{3}W' \right] - \frac{L}{nA} \left[\frac{1}{2}W + W' \right]$$

First term is deflection due to bending.

Second term is deflection due to shear

W' is force exerted at free end of beam

Given: $V=n$, $W'=0$, assume $W \ll YL^2$



$$a) \quad \frac{L^3}{YK^2A} \left[\frac{1}{8}W + \frac{1}{3}W' \right] = \frac{L}{nA} \left[\frac{1}{2}W + W' \right]$$

$$\frac{L^3}{K^2} \frac{1}{8}W = \frac{LW}{2}$$

$$\frac{L^2}{8K^2} = \frac{1}{2}$$

$$L^2 = 4K^2$$

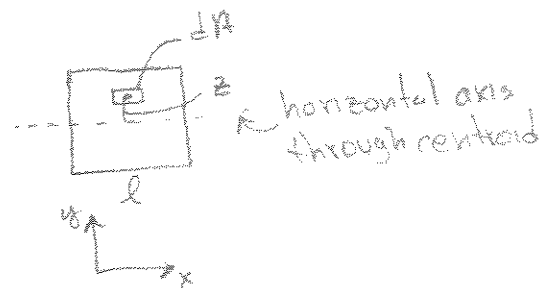
$$L^2 = 4 \frac{l^2}{12}$$

$$= \frac{l^2}{3}$$

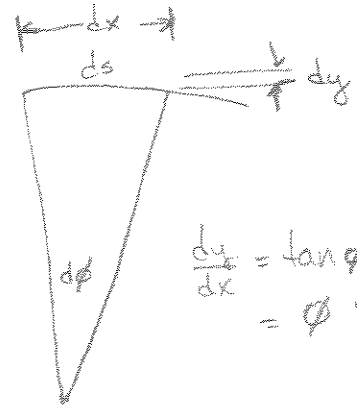
$$L = \frac{l}{\sqrt{3}}$$

$$L = \frac{l\sqrt{3}}{3}$$

$$\begin{aligned} K^2 &= \frac{1}{A} \int \int z^2 dA \\ &= \frac{1}{l^2} \int_{-l/2}^{l/2} \int_{-l/2}^{l/2} y^2 dx dy \\ &= \frac{1}{l} \left[\frac{y^3}{3} \right]_{-l/2}^{l/2} \\ &= \frac{1}{l} \left[\frac{l^3}{24} + \frac{l^3}{24} \right] \\ &= \frac{l^2}{12} \end{aligned}$$



b)



$$\begin{aligned}\frac{d\phi}{ds} &= \frac{d\phi}{dx} \\ &= \frac{d}{dx} \phi \\ &= \frac{d}{dx} \frac{dy}{dx} \\ &= \frac{d^2y}{dx^2}\end{aligned}$$

$$\begin{aligned}\frac{dy}{dx} &= \tan \phi \\ &= \phi \quad \{\phi \text{ small}\}\end{aligned}$$

$$\frac{d\phi}{dx} = \frac{d^2y}{dx^2}$$

$$d\phi = \frac{d^2y}{dx^2} dx$$

$$\phi = \int \left(\frac{d^2y}{dx^2} \right) dx$$

$$y = \frac{-L^3}{YK^2A} \left[\frac{Wx^2}{4L^2} - \frac{2Wx^3}{12L^3} + \frac{Wx^4}{24L^4} \right] - \frac{L}{nA} \left[\frac{Wx}{L} - \frac{Wx^2}{2L^2} \right] \quad (5.16A)$$

$$\frac{dy}{dx} = \frac{-L^3}{YK^2A} \left[\frac{Wx}{2L^2} - \frac{Wx^2}{2L^3} + \frac{Wx^3}{6L^4} \right] - \frac{L}{nA} \left[\frac{W}{L} - \frac{Wx}{L^2} \right]$$

$$\frac{d^2y}{dx^2} = \frac{-L^3}{YK^2A} \left[\frac{W}{2L^2} - \frac{Wx}{L^3} + \frac{Wx^2}{2L^4} \right] - \frac{L}{nA} \left[\frac{W}{L^2} \right]$$

$$\phi = \int_0^L \left[\frac{-L^3}{YK^2A} \left[\frac{W}{2L^2} - \frac{Wx}{L^3} + \frac{Wx^2}{2L^4} \right] - \frac{L}{nA} \left[\frac{W}{L^2} \right] \right] dx$$

$$= \frac{-L^3}{YK^2A} \left[\frac{Wx}{2L^2} - \frac{Wx^2}{2L^3} + \frac{Wx^3}{6L^4} \right] - \frac{L}{nA} \left[\frac{Wx}{L^2} \right] \Big|_0^L$$

$$= \frac{-L^3}{YK^2A} \left[\frac{W}{2L} - \frac{W}{2L} + \frac{W}{6L} \right] - \frac{W}{nA}$$

$$= \frac{-L^3}{YK^2A} \left[\frac{W}{6L} \right] - \frac{W}{nA}$$

$$K = \frac{L^2}{12} \quad A = L^2$$

$$\boxed{\phi = -\frac{2WL^2}{YL^4}}$$

$\frac{W}{nA}$ is shear and does not contribute to face angle

c)



$$y = -\frac{L^3}{YK^2A} \left[\frac{Wx^2}{4L^2} \left(1 - \frac{2x}{3L} + \frac{1}{6} \frac{x^2}{L^2} \right) \right] - \frac{L}{nA} \left[\frac{Wx}{L} \left(1 - \frac{1}{2} \frac{x}{L} \right) \right] \quad \{W'=0\} \quad (5.164)$$

$$y = -\frac{L^3}{YK^2A} \left[\frac{Wx^2}{4L^2} - \frac{2Wx^3}{12L^3} + \frac{Wx^4}{24L^4} \right] - \frac{L}{nA} \left[\frac{Wx}{L} - \frac{Wx^2}{2L^2} \right]$$

$$\frac{dy}{dx} = -\frac{L^3}{YK^2A} \left[\frac{Wx}{2L^2} - \frac{Wx^2}{2L^3} + \frac{Wx^3}{6L^4} \right] - \frac{L}{nA} \left[\frac{W}{L} - \frac{Wx}{L^2} \right]$$

$$\frac{dy}{dx}_{x=L} = -\frac{L^3}{YK^2A} \left[\frac{W}{2L} - \frac{W}{2L} + \frac{W}{6L} \right] - \frac{L}{nA} \left[\frac{W}{L} - \frac{W}{L} \right]$$

$$\alpha = -\frac{L^3}{YK^2A} \left[\frac{W}{6L} \right]$$

$$= -\frac{L^2 W}{6YK^2 A}$$

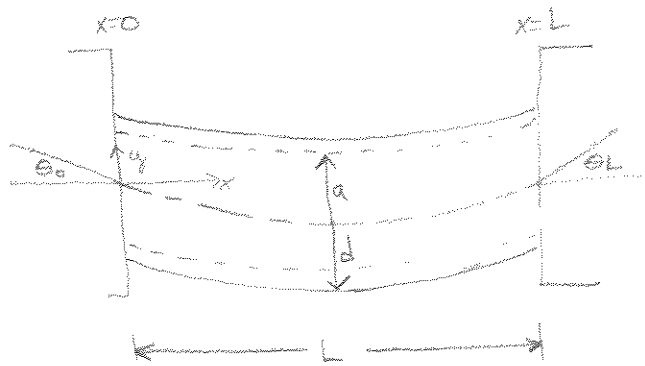
$$= -\frac{L^2 W}{6Y \frac{L^4}{12}}$$

$$K^2 = \frac{L^2}{12}$$

$$A = L^2$$

$$\alpha = -\frac{2L^2 W}{Y L^4}$$

5-39



$$EI \frac{d^4 w}{dx^4} = \frac{1}{nA} \frac{d^2 w}{dx^2} - \frac{w}{YK^2 A}$$

$$EI \frac{d^3 w}{dx^3} = \frac{1}{nA} \frac{dw}{dx} - \frac{wx}{YK^2 A} + C_3$$

$$EI \frac{d^2 w}{dx^2} = \frac{1}{nA} w - \frac{w}{YK^2 A} \frac{x^2}{2} + C_3 x + C_2$$

$$EI \frac{dw}{dx} = \frac{w}{nA} x - \frac{w}{YK^2 A} \frac{x^3}{6} + C_3 \frac{x^2}{2} + C_2 x + C_1$$

$$EI w = \frac{w}{nA} \frac{x^2}{2} - \frac{w}{YK^2 A} \frac{x^4}{24} + C_3 \frac{x^3}{6} + C_2 \frac{x^2}{2} + C_1 x + C_0$$

B.C.

$$y(0)=0, y(L)=0, y'(\frac{L}{2})=0, -y'(0)=y'(L)$$

$$y(0)=0: 0=C_0$$

$$y(L)=0: 0 = \frac{w}{nA} \frac{L^2}{2} - \frac{w}{24YK^2 A} L^4 + C_3 \frac{L^3}{6} + C_2 \frac{L^2}{2} + C_1 L$$

$$C_3 \frac{L^3}{6} + C_2 \frac{L^2}{2} + C_1 L = -\frac{WL}{2nA} + \frac{WL^3}{24YK^2 A} \quad \left\{ \begin{array}{l} w = \frac{W}{L} \end{array} \right.$$

$$y'(\frac{L}{2})=0: 0 = \frac{w}{nA} \frac{L}{2} - \frac{w}{6YK^2 A} \frac{L^3}{8} + C_3 \frac{L^2}{8} + C_2 \frac{L}{2} + C_1$$

$$C_3 \frac{L^2}{8} + C_2 \frac{L}{2} + C_1 = -\frac{W}{2nA} + \frac{WL^2}{48YK^2 A}$$

$$-y'(0)=y'(L): -C_1 = \frac{w}{nA} L - \frac{w}{6YK^2 A} L^3 + C_3 \frac{L^2}{2} + C_2 L + C_1$$

$$C_3 \frac{L^2}{2} + C_2 L + 2C_1 = -\frac{W}{nA} + \frac{WL^2}{6YK^2 A}$$

$$\textcircled{1} \quad C_3 \frac{L^2}{6} + C_2 \frac{L}{2} + C_1 = \frac{WL^2}{24YK^3A} - \frac{W}{2nA}$$

$$\textcircled{2} \quad C_3 \frac{L^2}{8} + C_2 \frac{L}{2} + C_1 = \frac{WL^2}{48YK^3A} - \frac{W}{2nA}$$

$$\textcircled{3} \quad C_3 \frac{L^2}{2} + C_2 L + 2C_1 = \frac{WL^2}{6YK^3A} - \frac{W}{nA}$$

$$\textcircled{1} \quad C_3 \frac{L^2}{6} + C_2 \frac{L}{2} + C_1 = \frac{WL^2}{24YK^3A} - \frac{W}{2nA}$$

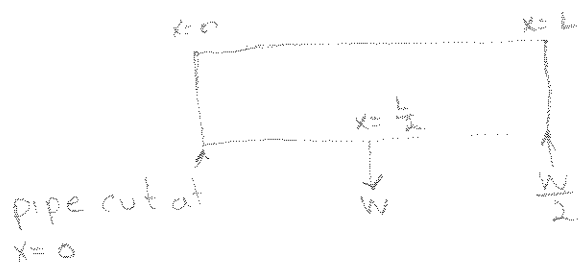
$$\textcircled{2} \quad -C_3 \frac{L^2}{8} - C_2 \frac{L}{2} - C_1 = \frac{-WL^2}{48YK^3A} + \frac{W}{2nA}$$

$$C_3 \frac{L^2}{24} = \frac{WL^2}{48YK^3A}$$

$$C_3 = \frac{W}{2YK^3A}$$

C_2 and C_1 are indeterminate with the given boundary conditions

At $x=0$ the shear force is



$$\sum F = 0 : S - W + \frac{W}{2} = 0$$

$$S - \frac{W}{2} = 0$$

$$S = \frac{W}{2} \text{ (positive shear)}$$

$$y'(0) = C_1 = \theta = \frac{S}{nA} = \frac{W}{2nA}$$

$$\textcircled{1} \quad C_3 \frac{L^2}{6} + C_2 \frac{L}{2} + C_1 = \frac{WL^2}{24YK^3A} - \frac{W}{2nA}$$

$$\frac{W}{2YK^3A} \frac{L^2}{6} + C_2 \frac{L}{2} + \frac{W}{2nA} = \frac{WL^2}{24YK^3A} - \frac{W}{2nA}$$

$$\frac{WL^2}{12YK^2A} + C_2 \frac{L}{2} + \frac{W}{2nA} = \frac{WL^2}{24YK^2A} - \frac{W}{2nA}$$

$$C_2 = \frac{-WL}{6YK^2A} + \frac{WL}{12YK^2A} - \frac{2W}{nAL}$$

$$= \frac{-WL}{12YK^2A} - \frac{2W}{nAL}$$

$$y = \frac{W}{2nAL} x^2 - \frac{W}{24YK^2AL} x^4 + \frac{W}{12YK^2A} x^3 - \left(\frac{WL}{12YK^2A} + \frac{2W}{nAL} \right) \frac{x^2}{2} + \frac{W}{2nA} x$$

$$y\left(\frac{L}{2}\right) = \frac{W}{2nAL} \frac{L^2}{4} - \frac{W}{24YK^2AL} \frac{L^4}{16} + \frac{W}{12YK^2A} \frac{L^3}{8} - \frac{WL}{24YK^2A} \frac{L^2}{4} - \frac{2W}{nAL} \frac{L^2}{4} + \frac{W}{2nA} \frac{L}{2}$$

$$= \frac{-WL^3}{384YK^2A} + \frac{WL^3}{96YK^2A} - \frac{WL^3}{96YK^2A} + \frac{WL}{8nA} - \frac{WL}{2nA} + \frac{WL}{4nA}$$

$$= \frac{-WL^3}{384YK^2A} + \frac{4WL^3}{384YK^2A} - \frac{4WL^3}{384YK^2A} - \frac{WL}{8nA}$$

$$= \frac{-WL^3}{384YK^2A} - \frac{WL}{8nA}$$

$$= \frac{-\rho L^4 \pi (b^2 - a^2)}{384Y \pi (b^4 - a^4)} - \frac{\rho L^2}{8n}$$

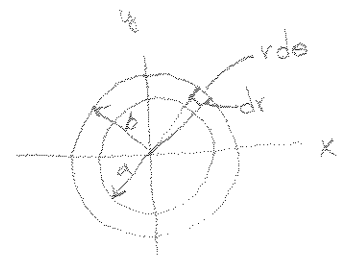
$$y\left(\frac{L}{2}\right) = \frac{-\rho L^4}{96Y(b^2 - a^2)} - \frac{\rho L^2}{8n}$$

$$K_z^2 = \frac{1}{A} \int r^2 dA$$

$$= \frac{1}{A} \int_0^{2\pi} \int_a^b r^3 dr d\theta$$

$$= \frac{2\pi}{A} \left[\frac{r^4}{4} \right]_a^b$$

$$= \frac{\pi}{2A} (b^4 - a^4)$$



$$I_x + I_y = I_z \quad \{ \text{perpendicular axis theorem} \}$$

$$I_x = I_y$$

$$2I_x = I_z$$

$$2K_x = K_z$$

$$K_x = \frac{K_z}{2}$$

$$= \frac{\pi}{4A} (b^4 - a^4)$$

$$W = \rho AL$$

$$W = \rho \pi (b^2 - a^2) L$$

Find increase in deflection when the pipe is filled with a fluid of density ρ_0

Since a fluid does not support shear forces it only adds to the distributed load w .

$$y\left(\frac{L}{2}\right) = \frac{-WL^3}{384YK^2A} - \frac{WL}{8nA}$$
$$= \frac{-WL^3}{96Y\pi(b^4-a^4)} - \frac{WL}{8n\pi(b^2-a^2)}$$

$$\Delta y\left(\frac{L}{2}\right) = \frac{-\Delta WL^2}{96Y\pi(b^4-a^4)} - \frac{\Delta WL}{8n\pi(b^2-a^2)}$$

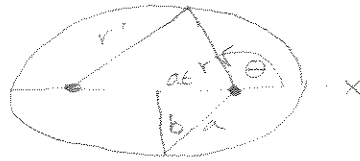
$$\Delta y\left(\frac{L}{2}\right) = \frac{-\rho_0\pi a^2 L^3}{96Y\pi(b^4-a^4)} - \frac{\rho_0\pi a^2 L^2}{8n\pi(b^2-a^2)}$$

$$\Delta W = \text{addition of fluid}$$
$$= \rho_0\pi a^2 L$$

$$\Delta y\left(\frac{L}{2}\right) = \frac{-\rho_0 a^2 L^3}{96Y(b^4-a^4)} - \frac{\rho_0 a^2 L^2}{8n(b^2-a^2)}$$

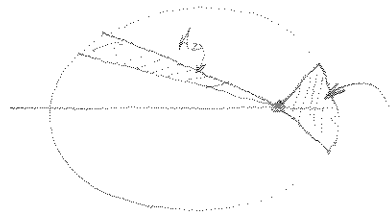
6-1

a) Kepler's 1st Law: $r = \frac{a(1-e^2)}{1+e\cos\theta}$



Kepler's 2nd Law:

$$\frac{d}{dt} \left(\frac{1}{2} r^2 \dot{\theta} \right) = 0$$



$A_1 = A_2$ for $t_1 = t_2$

$$dA = \frac{1}{2} r^2 d\theta$$

$$\frac{dA}{dt} = \frac{1}{2} r^2 \dot{\theta}$$

Newton's Laws: $\vec{F} = m\vec{a}$, $\vec{F} = -\vec{F}$

$$\vec{r} = r \hat{r}(\theta)$$

$$\vec{r} = \frac{d\vec{r}}{dt} = \dot{r} \hat{r} + r \frac{d\hat{r}}{d\theta} \frac{d\theta}{dt} \quad \frac{d\hat{r}}{d\theta} = \hat{\theta}, \quad \frac{d\hat{\theta}}{d\theta} = -\hat{r}$$

$$\vec{r} = \dot{r} \hat{r} + r \dot{\theta} \hat{\theta}$$

$$\vec{\ddot{r}} = \frac{d\vec{r}}{dt} = \dot{r} \frac{d\hat{r}}{dt} + r \frac{d\dot{\theta}}{dt} \frac{d\hat{\theta}}{dt} + \dot{r} \dot{\theta} \hat{\theta} + r [\ddot{\theta} \hat{\theta} + \dot{\theta} \frac{d\hat{\theta}}{d\theta} \frac{d\theta}{dt}]$$

$$= \ddot{r} \hat{r} + \dot{r} \dot{\theta} \hat{\theta} + r \ddot{\theta} \hat{\theta} + r \dot{\theta}^2 (-\hat{r}) - r \dot{\theta}^2 \hat{r}$$

$$\vec{\ddot{r}} = (\ddot{r} - r\dot{\theta}^2) \hat{r} + (r\ddot{\theta} + 2\dot{r}\dot{\theta}) \hat{\theta}$$

$$r = p(1+e\cos\theta) \quad \{ p = a(1-e^2) \}$$

Kepler's 2nd Law

$$\frac{d}{dt} \left(\frac{1}{2} r^2 \dot{\theta} \right) = 0 \quad \{ \frac{dA}{dt} = \text{constant} \}$$

$$\frac{1}{2} r^2 \dot{\theta} = C$$

$$\dot{\theta} = \frac{2C}{r^2} = \frac{K}{r^2} \Rightarrow \ddot{\theta} = -\frac{2K}{r^3} \dot{r}$$

$$\begin{aligned}
 \vec{r} &= (\ddot{r} - r\dot{\theta}^2) \hat{r} + (r\ddot{\theta} + 2\dot{r}\dot{\theta}) \hat{\theta} \\
 &= \left(\ddot{r} - r \left(\frac{K}{r^2} \right)^2 \right) \hat{r} + \left(r \left(\frac{-2K}{r^3} \dot{r} \right) + 2\dot{r} \left(\frac{K}{r^2} \right) \right) \hat{\theta} \\
 &= \left(\ddot{r} - \frac{K^2}{r^3} \right) \hat{r} + \left(-\frac{2K}{r^2} \dot{r} + \frac{2K}{r^2} \dot{r} \right) \hat{\theta} \\
 &= \left(\ddot{r} - \frac{K^2}{r^3} \right) \hat{r}
 \end{aligned}$$

$$r = p(1 + e \cos \theta)^{-1}$$

$$\dot{r} = p e \sin \theta (1 + e \cos \theta)^{-2} \dot{\theta}$$

$$= p e \sin \theta (1 + e \cos \theta)^{-2} \frac{K}{r^2}$$

$$= \frac{p}{1 + e \cos \theta} \frac{e \sin \theta}{1 + e \cos \theta} \frac{K}{r^2}$$

$$= \frac{e \sin \theta}{1 + e \cos \theta} \frac{K}{r}$$

$$\ddot{r} = \frac{e \sin \theta}{1 + e \cos \theta} \left(-\frac{K}{r^2} \right) \dot{r} + \frac{K}{r} \left[\frac{(1 + e \cos \theta) e \cos \theta \dot{\theta} + e \sin \theta (e \sin \theta) \dot{\theta}}{(1 + e \cos \theta)^2} \right]$$

$$= \frac{e \sin \theta}{1 + e \cos \theta} \left(-\frac{K}{r^2} \right) \frac{e \sin \theta}{1 + e \cos \theta} \left(\frac{K}{r} \right) + \frac{K}{r} \frac{K}{r^2} \left[\frac{e \cos \theta}{(1 + e \cos \theta)} + \frac{(e \sin \theta)^2}{(1 + e \cos \theta)^2} \right]$$

$$= -\frac{K^2}{r^3} \frac{(e \sin \theta)^2}{(1 + e \cos \theta)^2} + \frac{K^2}{r^3} \frac{e \cos \theta}{(1 + e \cos \theta)} + \frac{K^2}{r^3} \frac{(e \sin \theta)^2}{(1 + e \cos \theta)^2}$$

$$= \frac{K^2}{r^3} \frac{e \cos \theta}{(1 + e \cos \theta)}$$

$$\vec{r} = \left[\frac{K^2}{r^3} \left(\frac{e \cos \theta}{1 + e \cos \theta} - 1 \right) \right] \hat{r} \quad \frac{r}{p} = (1 + e \cos \theta)^{-1}$$

$$= \frac{K^2}{r^3} \left(\frac{\frac{p-r}{r}}{1 + \frac{p-r}{r}} - 1 \right) \hat{r}$$

$$\frac{p}{r} = 1 + e \cos \theta$$

$$\frac{p}{r} - 1 = e \cos \theta$$

$$\frac{p-r}{r} = e \cos \theta$$

$$= \frac{K^2}{r^3} \left(\frac{\frac{p-r}{r}}{\frac{p}{r}} - 1 \right) \hat{r}$$

$$= \frac{K^2}{r^3} \left(\frac{r}{p} \left(\frac{p-r}{r} \right) - 1 \right) \hat{r}$$

$$= \frac{K^2}{r^3} \left(\frac{p-r}{p} - 1 \right) \hat{r}$$

$$= \frac{K^2}{r^3} \left(\frac{p-r-p}{p} \right) \hat{r}$$

$$\vec{r} = \frac{k^2}{r^3} \left(-\frac{r}{p} \right) \hat{r}$$

$$= -\frac{k^2}{p} \frac{1}{r^2} \hat{r}$$

$$m\ddot{\vec{r}} = -\frac{k^2}{p} \frac{m}{r^2} \hat{r}$$

$$m\ddot{\vec{r}} = -\frac{K_0 m}{r^2} \hat{r}, K_0 = \frac{k^2}{p}$$

b) Kepler's 3rd Law:

$$T^2 = Ka^3$$

$$L^2 = \frac{4\pi^2 a^3 b^2 m^2}{T^2}$$

$$L^2 = \frac{4\pi^2 b^2 m^2}{Ka}$$

$$m\ddot{r} - mr\dot{\theta}^2 = F(r)$$

$$m\ddot{r} - mr \frac{L^2}{m^2 r^4} = F(r)$$

$$m\ddot{r} - \frac{L^2}{mr^3} = F(r)$$

$$m\ddot{r} - \frac{4\pi^2 b^2 m^2}{Ka} \frac{1}{mr^3} = F(r)$$

$$m\ddot{r} - \frac{mC}{r^3} = F(r)$$

$$\therefore F(r) \propto m$$

$$\frac{dS}{dt} = \frac{1}{2} r^2 \ddot{\theta} = \frac{L}{2m} \quad \left\{ \dot{\theta} = \frac{L}{mr^2} \right\}$$

$$S = \frac{L\tau}{2m}$$

$$\pi ab = \frac{L\tau}{2m}$$

$$L^2 = \frac{\pi^2 a^3 b^2 4m^2}{T^2}$$

c) $F_1 = F_2$

$$F_1 = \frac{M_1 K_1}{r^2} \quad F_2 = \frac{m_2 K_2}{r^2}$$

$$m_1 K_1 = m_2 K_2$$

$$\frac{K_1}{m_2} = \frac{K_2}{m_1} = K_3$$

$$K_1 = K_3 m_2$$

$$K_2 = K_3 m_1$$

$$F_1 = F_2$$

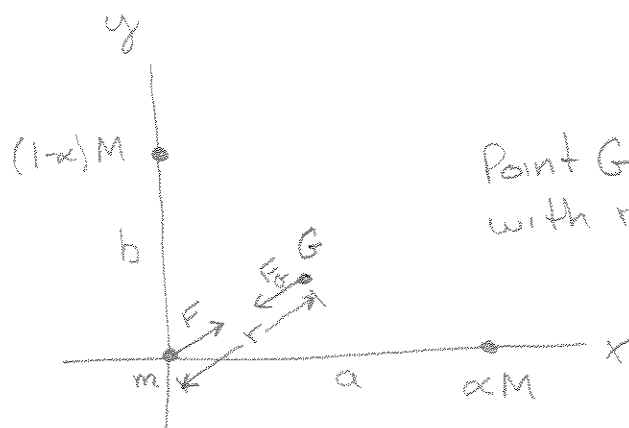
$$F_1^2 = F_1 \cdot F_2$$

$$= \frac{m_1 m_2 k_3}{r^2} \cdot \frac{m_2 m_1 k_3}{r^2}$$

$$= \frac{m_1^2 m_2^2 k_3^2}{r^4}$$

$$\boxed{\begin{aligned} F_1 &= k_3 \frac{m_1 m_2}{r^2} \\ F_2 &= k_3 \frac{m_1 m_2}{r^2} \end{aligned}}$$

3. A mass αM is located at $x = a, y = 0$, and a second mass $(1-\alpha)M$ is located at $x = 0, y = b$, where $0 < \alpha < 1$. Find the coordinates x, y of the center of gravity of the two masses relative to the origin. Show that your formulas for x, y have the proper limits when $\alpha \rightarrow 0$ or $b \rightarrow \infty$.



Point G is center of gravity with respect to origin.

$$\vec{F} = \sum_i \frac{m m_i G (\vec{r}_i - \vec{r}_0)}{|\vec{r}_i - \vec{r}_0|^3} \quad \vec{r}_0 = 0 \text{ (origin)}$$

$$\vec{F} = \frac{m \alpha M G a \hat{x}}{a^3} + \frac{m (1-\alpha) M G b \hat{y}}{b^3}$$

$$F = \left[\left(\frac{m \alpha M G a}{a^3} \right)^2 + \left(\frac{m (1-\alpha) M G b}{b^3} \right)^2 \right]^{1/2}$$

$$= \left[\frac{m^2 \alpha^2 M^2 G^2}{a^4} + \frac{m^2 (1-\alpha)^2 M^2 G^2}{b^4} \right]^{1/2}$$

$$F = m M G \left[\frac{\alpha^2}{a^4} + \frac{(1-\alpha)^2}{b^4} \right]^{1/2}$$

$$\vec{F}_G = \frac{m M G}{r^2}$$

$$\vec{F}_G = F \quad (\text{Newton's Third Law})$$

$$\frac{m M G}{r^2} = m M G \left[\frac{b^4 \alpha^2 + a^4 (1-\alpha)^2}{a^4 b^4} \right]^{1/2}$$

$$\frac{1}{r^2} = \left[\frac{b^4 \alpha^2 + a^4 (1-\alpha)^2}{a^4 b^4} \right]^{1/2}$$

$$r^2 = \left[\frac{a^4 b^4}{b^4 \alpha^2 + a^4 (1-\alpha)^2} \right]^{1/2} = \frac{a^2 b^2}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/2}}$$

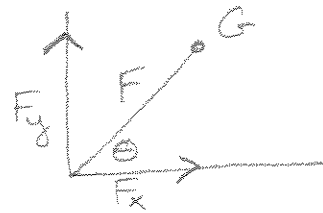
$$r = \frac{ab}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/4}}$$

$$\begin{aligned} \cos \theta &= \frac{F_x}{F} \\ &= \frac{mMG\alpha}{a^2} \\ &= \frac{mMG \frac{a^2 b^2}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/2}}}{a^2 b^2} \end{aligned}$$

$$\cos \theta = \frac{\alpha b^2}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/2}}$$

$$\begin{aligned} x_G &= r \cos \theta \\ &= \frac{ab}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/4}} \cos \theta \\ &= \frac{ab^3 \alpha}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{3/4}} \end{aligned}$$

$$x_G = \frac{a\alpha}{[\alpha^2 + \frac{a^4}{b^4}(1-\alpha)^2]^{3/4}}$$



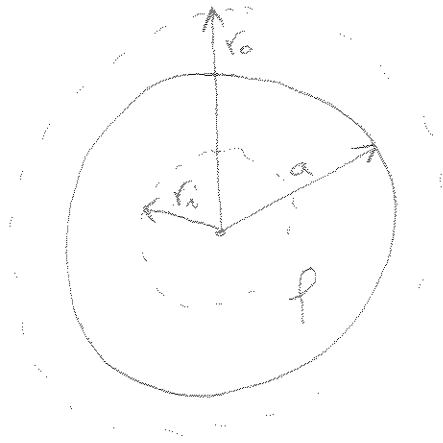
$$\begin{aligned} \sin \theta &= \frac{F_y}{F} \\ &= \frac{mMG(1-\alpha)}{b^2} \\ &= \frac{mMG \frac{a^2 b^2 (1-\alpha)}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/2}}}{a^2 b^2} \end{aligned}$$

$$\sin \theta = \frac{(1-\alpha)a^2}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/2}}$$

$$\begin{aligned} y_G &= r \sin \theta \\ &= \frac{ab}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{1/4}} \sin \theta \\ &= \frac{a^3 b (1-\alpha)}{[b^4 \alpha^2 + a^4 (1-\alpha)^2]^{3/4}} \end{aligned}$$

$$y_G = \frac{b(1-\alpha)}{[\frac{b^4}{a^4} \alpha^2 + (1-\alpha)^2]^{3/4}}$$

5. Assuming that the earth is a sphere of uniform density, with radius a , mass M , calculate the gravitational field intensity and the gravitational potential at all points inside and outside the earth, taking $\phi = 0$ at an infinite distance.



a) Calculate $\vec{g}$

$$\int \vec{g} \cdot d\vec{S} = -4\pi GM$$

$r \geq a$ (outside)

$$\int \vec{g} \cdot d\vec{S} = -4\pi GM$$

$$g 4\pi r^2 = -4\pi GM$$

$$g = -\frac{MG}{r^2}$$

$$\boxed{\vec{g} = -\frac{MG}{r^2} \frac{\vec{r}}{r}}$$

$r \leq a$ (inside)

$$m = \rho \frac{4}{3} \pi r^3$$

$$\int \vec{g} \cdot d\vec{S} = -4\pi Gm$$

$$g 4\pi r^2 = -4\pi G \rho \frac{4}{3} \pi r^3$$

$$g = -G \rho \frac{4}{3} \pi r$$

$$\vec{g} = -\frac{MG}{a^3} r \frac{\vec{r}}{r}$$

$$\boxed{\vec{g} = -\frac{MG}{a^3} \vec{r}}$$

$$M = \rho \frac{4}{3} \pi a^3$$

$$\frac{M}{a^3} = \rho \frac{4}{3} \pi$$

b) Calculate U

$$U = \int_{r_s}^r \vec{g} \cdot d\vec{r}$$

$$\begin{aligned}
 U_o &= \int_{\infty}^r -\frac{MG}{r'^2} dr' \\
 &= -MG \int_{\infty}^r r'^{-2} dr' \\
 &= MG \frac{1}{r'} \Big|_{\infty}^r
 \end{aligned}$$

$$\boxed{U_o = \frac{MG}{r} \quad (r \geq a)}$$

$$\begin{aligned}
 U_i &= \int_{r_s}^r -\frac{MG r'}{a^3} dr' \\
 &= -\frac{MG}{a^3} \int_{r_s}^r r' dr' \\
 &= -\frac{MG}{a^3} \frac{r'^2}{2} \Big|_{r_s}^r \\
 &= -\frac{MG}{a^3} \left[\frac{r^2}{2} - \frac{r_s^2}{2} \right] \\
 &= \frac{MG}{2a^3} [r_s^2 - r^2]
 \end{aligned}$$

To determine r_s , $U_o = U_i$ at $r = a$

$$U_{o, r=a} = \frac{MG}{a} \qquad U_{i, r=a} = \frac{MG}{2a^3} [r_s^2 - a^2]$$

$$\frac{MG}{a} = \frac{MG}{2a^3} [r_s^2 - a^2]$$

$$2a^2 = r_s^2 - a^2$$

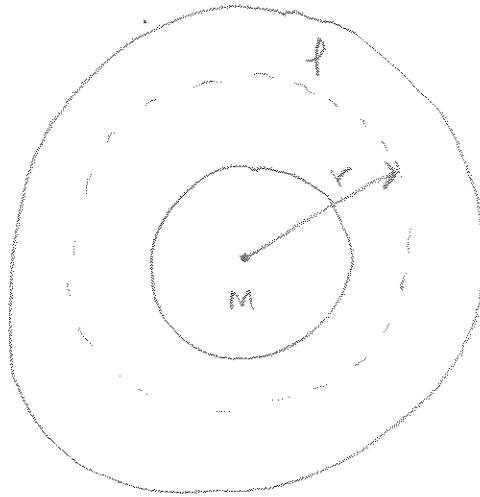
$$3a^2 = r_s^2$$

$$\boxed{U_i = \frac{MG}{2a^3} [3a^2 - r^2]}$$

7. Show that if the sun were surrounded by a spherical cloud of dust of uniform density ρ , the gravitational field within the dust cloud would be

$$\mathbf{g} = -\left(\frac{MG}{r^2} + \frac{4\pi}{3}\rho Gr\right)\frac{\mathbf{r}}{r},$$

where M is the mass of the sun, and $\mathbf{r}$ is a vector from the sun to any point in the dust cloud.



Outside the Sun

$$\int \vec{g} \cdot d\vec{s} = -4\pi GM$$

$$g 4\pi r^2 = -4\pi GM$$

$$g = -\frac{MG}{r^2}$$

$$\vec{g}_s = -\frac{MG}{r^2} \frac{\vec{r}}{r}$$

Inside dust cloud

$$\int \vec{g} \cdot d\vec{s} = -4\pi Gm \quad m = \rho \frac{4}{3}\pi r^3$$

$$g 4\pi r^2 = -4\pi G \rho \frac{4}{3}\pi r^3$$

$$g = -\frac{4}{3}\rho \pi Gr$$

$$\vec{g}_d = -\frac{4\pi}{3}\rho Gr \frac{\vec{r}}{r}$$

$$\vec{g} = \vec{g}_s + \vec{g}_d$$

$$\boxed{\vec{g} = -\left(\frac{MG}{r^2} + \frac{4\pi}{3}\rho Gr\right)\frac{\vec{r}}{r}}$$

6-9

$$\vec{\nabla}P = \rho g$$

$$\frac{dP}{dr} \frac{1}{\rho} = g$$

$$\frac{dg}{dr} = \frac{d^2P}{dr^2} \frac{1}{\rho} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{1}{\rho} \right)$$

$$g = -\frac{GM}{r^2} \quad \{ \text{spherical body} \}$$

$$\frac{dg}{dr} = -\frac{G}{r^2} \frac{dM}{dr} = \frac{2GM}{r^3}$$

$$\frac{d^2P}{dr^2} \frac{1}{\rho} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{1}{\rho} \right) = -\frac{GdM}{r^2 dr} + \frac{2GM}{r^3}$$

$$\frac{1}{\rho} \frac{d^2P}{dr^2} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{1}{\rho} \right) - \frac{2GM}{r^3} = -\frac{GdM}{r^2 dr}$$

$$\frac{1}{\rho} \frac{d^2P}{dr^2} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{1}{\rho} \right) + GM \frac{d}{dr} \left(\frac{1}{r^2} \right) = -\frac{GdM}{r^2 dr}$$

$$\frac{r^2}{\rho} \frac{d^2P}{dr^2} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{r^2}{\rho} \right) + GM \frac{d}{dr} \left(\frac{r^2}{r^2} \right) = -\frac{GdM}{dr}$$

$$\frac{r^2}{\rho} \frac{d^2P}{dr^2} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{r^2}{\rho} \right) = -G \frac{dM}{dr}$$

$$\begin{aligned} \frac{dM}{dr} &= \rho dV \\ &= \rho 4\pi r^2 dr \end{aligned}$$

$$\frac{r^2}{\rho} \frac{d^2P}{dr^2} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{r^2}{\rho} \right) = -4\pi r^2 G \rho$$

$$\rho = \frac{AP}{RT}$$

$$\frac{RT r^2}{AP} \frac{d^2P}{dr^2} + \frac{dP}{dr} \frac{d}{dr} \left(\frac{RT r^2}{AP} \right) = -4\pi r^2 G \frac{AP}{RT}$$

$$\frac{1}{\rho} = \frac{RT}{AP}$$

$$\frac{R^2 T r^2}{A^2 P} \frac{d^2P}{dr^2} + \frac{P^2}{A^2} \frac{dP}{dr} \frac{d}{dr} \left(\frac{T r^2}{P} \right) = -4\pi r^2 G \frac{P}{T}$$

$$\frac{d}{dr} \left(\frac{R^2 T r^2}{A^2 P} \frac{dP}{dr} \right) = -4\pi r^2 G \frac{P}{T}$$

$$\boxed{T \frac{d}{dr} \left(\frac{R^2 T r^2}{A^2 P} \frac{dP}{dr} \right) = -4\pi r^2 G P}$$

$$\text{B.C.: } M = \int_0^\infty \rho dV$$

$$M = \int_0^\infty \frac{AP}{RT} 4\pi r^2 dr$$

$$\rho(\infty) = 0 \quad A = \frac{M}{n}$$

6-11

$$\rho = \frac{Ma^2}{2\pi r(r^2+a^2)^2}, 0 \leq r < \infty$$

$$\vec{f} = \rho \vec{g}$$

$$\vec{\nabla} P = \vec{f}$$

$$\vec{\nabla} P = -\rho \vec{g}$$

$$\frac{dP}{dr} = -\rho g$$

For a spherical mass

$$g = \frac{GM(r)}{r^2}$$

$$M(r) = \int_0^r \rho dV$$

$$= \int_0^r \frac{Ma^2}{2\pi r'(r'^2+a^2)^2} 4\pi r'^2 dr'$$

$$= Ma^2 \int_0^r \frac{2r' dr'}{(r'^2+a^2)^2} \quad \text{let } u = r'^2+a^2$$

$$du = 2r' dr'$$

$$= Ma^2 \int \frac{du}{u^2}$$

$$= Ma^2 \left[-\frac{1}{u} \right]$$

$$M(r) = -Ma^2 \left[\frac{1}{r^2+a^2} \right]_0^r$$

$$M(r) = -Ma^2 \left[\frac{1}{r^2+a^2} - \frac{1}{a^2} \right]$$

$$\frac{dP}{dr} = \frac{-Ma^2}{2\pi r(r^2+a^2)^2} = \frac{-GMa^2}{r^2} \left[\frac{1}{r^2+a^2} - \frac{1}{a^2} \right]$$

$$dP = \frac{GM^2 a^4}{2\pi} \left[\frac{1}{r^3(r^2+a^2)^3} - \frac{1}{a^2 r^3(r^2+a^2)^2} \right] dr$$

$$P = \frac{GM^2 a^4}{2\pi} \left[\int \frac{dr}{r^3(r^2+a^2)^3} - \frac{1}{a^2} \int \frac{dr}{r^3(r^2+a^2)^2} \right]$$

$$\text{Evaluate } \int \frac{dr}{r^3(r^2+a^2)^3}$$

$$\int \frac{dr}{r^3(r^2+a^2)^3} = \int \frac{a \sec^2 \theta d\theta}{a^3 \tan^3 \theta (a^2 \tan^2 \theta + a^2)^3}$$

$$\text{Let } r = a \tan \theta$$

$$dr = a \sec^2 \theta d\theta = \int \frac{\sec^2 \theta d\theta}{a^2 \tan^3 \theta (a^2 \sec^2 \theta)^3}$$

$$= \frac{1}{a^8} \int \frac{d\theta}{\tan^3 \theta \sec^4 \theta} = \frac{1}{a^8} \int \frac{\cos^7 \theta d\theta}{\sin^3 \theta}$$

$$= \frac{1}{a^8} \int \frac{\cos^5 \theta (1 - \sin^2 \theta) d\theta}{\sin^3 \theta}$$

$$= \frac{1}{a^8} \left[\int \frac{\cos^5 \theta d\theta}{\sin^3 \theta} - \int \frac{\cos^3 \theta d\theta}{\sin \theta} \right]$$

$$\int \frac{dr}{r^3(r^2+a^2)^3} - \frac{1}{a^2} \int \frac{dr}{r^3(r^2+a^2)^2} = \frac{1}{a^8} \left[\int \frac{\cos^5 \theta d\theta}{\sin^3 \theta} - \int \frac{\cos^5 \theta}{\sin \theta} d\theta - \int \frac{\cos^3 \theta d\theta}{\sin^3 \theta} \right]$$

$$= -\frac{1}{a^8} \int \frac{\cos^5 \theta d\theta}{\sin \theta} = -\frac{1}{a^8} \int \frac{\cos^3 \theta (1 - \sin^2 \theta) d\theta}{\sin \theta}$$

$$= -\frac{1}{a^8} \left[\int \frac{\cos^3 \theta}{\sin \theta} d\theta - \int \cos^3 \theta \sin \theta d\theta \right]$$

$$= -\frac{1}{a^8} \left[\int \frac{\cos \theta (1 - \sin^2 \theta) d\theta}{\sin \theta} - \int \cos^3 \theta \sin \theta d\theta \right]$$

$$= -\frac{1}{a^8} \left[\int \frac{\cos \theta}{\sin \theta} d\theta - \int \cos \theta \sin \theta d\theta - \int \cos^3 \theta \sin \theta d\theta \right]$$

$$u = \sin \theta \quad u' = \cos \theta \quad u' = \cos \theta$$

$$du = \cos \theta d\theta \quad -du' = \sin \theta d\theta \quad -du' = \sin \theta d\theta$$

$$\text{Evaluate } \frac{1}{a^2} \int \frac{dr}{r^3(r^2+a^2)^2}$$

$$\frac{1}{a^2} \int \frac{dr}{r^3(r^2+a^2)^2} = \frac{1}{a^2} \int \frac{a \sec^2 \theta d\theta}{a^3 \tan^3 \theta (a^2 \tan^2 \theta + a^2)^2}$$

$$\text{let } r = a \tan \theta$$

$$dr = a \sec^2 \theta d\theta = \frac{1}{a^2} \int \frac{\sec^2 \theta d\theta}{a^2 \tan^3 \theta (a^2 \sec^2 \theta)^2}$$

$$= \frac{1}{a^8} \int \frac{d\theta}{\tan^3 \theta \sec^4 \theta} = \frac{1}{a^8} \int \frac{\cos^5 \theta d\theta}{\sin^3 \theta}$$

$$= \frac{-1}{a^8} \left[\int \frac{du}{u} + \int u' du' + \int u^3 du' \right]$$

$$= \frac{-1}{a^8} \left[\ln \sin \theta + \frac{\cos^2 \theta}{2} + \frac{\cos^4 \theta}{4} \right]$$



$$= \frac{-1}{a^8} \left[\ln \frac{r}{(r^2 + a^2)^{1/2}} + \frac{a^2}{2(r^2 + a^2)} + \frac{a^4}{4(r^2 + a^2)^2} \right]$$

$$= \frac{1}{a^8} \left[\ln \frac{(r^2 + a^2)^{1/2}}{r} - \frac{a^4}{4(r^2 + a^2)^2} - \frac{a^2}{2(r^2 + a^2)} \right]$$

$$= \frac{1}{2a^8} \left[\ln \frac{r^2 + a^2}{r^2} - \frac{a^4}{2(r^2 + a^2)^2} - \frac{a^2}{r^2 + a^2} \right]$$

$$P = \frac{GM^2 a^4}{4\pi a^8} \left[\ln \frac{r^2 + a^2}{r^2} - \frac{a^4}{2(r^2 + a^2)^2} - \frac{a^2}{r^2 + a^2} \right]$$

$$P = \frac{GM^2}{4\pi a^4} \left[\ln \frac{r^2 + a^2}{r^2} - \frac{a^4}{2(r^2 + a^2)^2} - \frac{a^2}{r^2 + a^2} \right]$$

$$PV = nRT \quad \frac{M}{A} = n$$

$$PV = \frac{MRT}{A}$$

$$\frac{AP}{RT} = \frac{M}{V} = \rho$$

$$T = \frac{A}{R} \frac{P}{\rho}$$

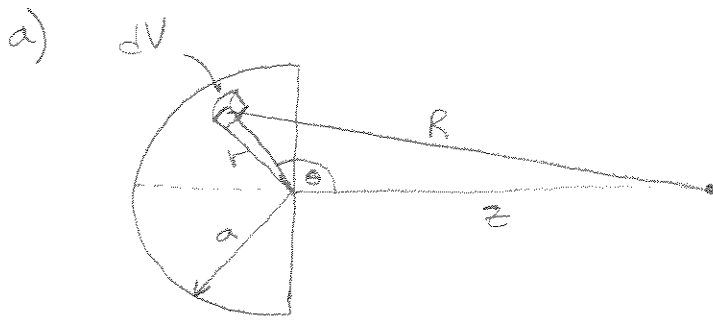
$$= \frac{A}{R} \frac{2\pi r (r^2 + a^2)^2}{Ma^2} \frac{GM^2}{4\pi a^4} \left[\ln \frac{r^2 + a^2}{r^2} - \frac{a^4}{2(r^2 + a^2)^2} - \frac{a^2}{r^2 + a^2} \right]$$

$$= \frac{AGMr}{2Ra^2} \left[\frac{(r^2 + a^2)^2}{a^4} \ln \frac{r^2 + a^2}{r^2} - \frac{1}{2} - \frac{r^2 + a^2}{a^2} \right]$$

$$T = \frac{AGMr}{2Ra^2} \left[\frac{(r^2 + a^2)^2}{a^4} \ln \frac{r^2 + a^2}{r^2} - \frac{3}{2} - \frac{r^2}{a^2} \right]$$

6-13

Gravitational Field of Hemisphere

Potential at z

$$G_H = G \int \frac{dm}{R}$$

$$= 2\pi\rho G \int_0^a \int_{\pi/2}^{\pi} \frac{r^2 \sin\theta d\theta dr}{(r^2 + z^2 - 2rz\cos\theta)^{1/2}}$$

$$= \frac{\pi\rho G}{z} \int_0^a \int_{u_1}^{u_2} \frac{du}{u^{1/2}} r dr$$

$$= \frac{2\pi\rho G}{z} \int_0^a \left(r^2 + z^2 - 2rz\cos\theta \right)^{1/2} \Big|_{\pi/2}^{\pi} r dr$$

$$= \frac{2\pi\rho G}{z} \int_0^a \left[r + z - (r^2 + z^2)^{1/2} \right] r dr$$

$$= \frac{2\pi\rho G}{z} \left[\frac{r^3}{3} + \frac{r^2 z}{2} - \frac{1}{3} (r^2 + z^2)^{3/2} \right] \Big|_0^a$$

$$G_H(z) = \frac{2\pi\rho G}{z} \left[\frac{a^3}{3} + \frac{a^2 z}{2} - \frac{1}{3} (a^2 + z^2)^{3/2} + \frac{z^3}{3} \right]$$

$$\vec{g}_H = \vec{\nabla} G_H$$

$$= \frac{\partial}{\partial z} G_H \hat{z}$$

$$= \frac{\partial}{\partial z} 2\pi\rho G \left[\frac{a^3}{3z} + \frac{a^2}{2} - \frac{(a^2 + z^2)^{3/2}}{3z} + \frac{z^2}{3} \right] \hat{z}$$

$$= 2\pi\rho G \left[\frac{-a^3}{3z^2} - \frac{3z(\frac{3}{2})(a^2 + z^2)^{1/2}(2z)}{3z^2} + \frac{2z}{3} \right] \hat{z}$$

$$\vec{g}_H(z) = 2\pi\rho G \left[\frac{-a^3}{3z^2} - (a^2 + z^2)^{1/2} + \frac{(a^2 + z^2)^{1/2}}{3z^2} + \frac{2z}{3} \right] \hat{z}$$

$$dm = \rho dV$$

$$= \rho r^2 \sin\theta d\phi d\theta dr$$

$$R = (r^2 + z^2 - 2rz\cos\theta)^{1/2}$$

$$u = r^2 + z^2 - 2rz\cos\theta$$

$$du = 2rz\sin\theta d\theta$$

$$\frac{r du}{2z} = r^2 \sin\theta d\theta$$

$$\vec{g}_H(a) = 2\pi\rho G \left[-\frac{a}{3} - \sqrt{2}a + \frac{2\sqrt{2}a}{3} + \frac{2}{3}a \right] \hat{z}$$

$$= 2\pi\rho G \left[\frac{a}{3} - \frac{\sqrt{2}a}{3} \right] \hat{z}$$

$$M = \frac{\rho}{2} \frac{4}{3}\pi a^3$$

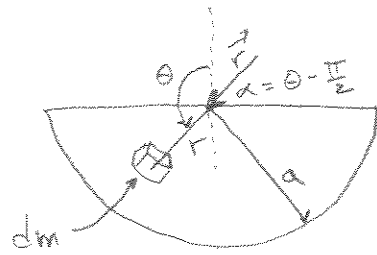
$$= \frac{MG}{a^2} [1 - \sqrt{2}] \hat{z}$$

$$g = g_0 - g_H(a) - \frac{MG}{a^2}$$

$$= g_0 - \frac{MG}{a^2} [2 - \sqrt{2}]$$

$$g_0 - g = \frac{MG}{a^2} [2 - \sqrt{2}]$$

b)



$$\vec{g} = \int \frac{G \rho \vec{r}}{|\vec{r}|^3} dV \quad dm = \rho dV$$

$$= \rho r^2 \sin \theta d\theta d\phi dr$$

$$\vec{g}_y = \int \frac{G \rho r \sin \alpha \hat{y}}{r^3} dV$$

$$\vec{r} = r (\cos \alpha \hat{x} + \sin \alpha \hat{y})$$

$$= - \int \frac{G \rho \cos \theta \hat{y}}{r^2} dV$$

$$|\vec{r}| = r$$

$$= -2\pi G \rho \int_0^a \int_{\pi/2}^{\pi} \frac{r^2 \sin \theta \cos \theta}{r^2} d\theta dr \hat{y} \quad \sin \alpha = \sin(\theta - \frac{\pi}{2}) = -\cos \theta$$

$$= -2\pi G \rho \int_0^a \int_{\pi/2}^{\pi} \sin \theta \cos \theta d\theta dr \hat{y}$$

$$= -2\pi G \rho \int_0^a \left[\frac{\sin^2 \theta}{2} \right]_{\pi/2}^{\pi} dr \hat{y}$$

$$= -\pi G \rho \int_0^a (-1) dr \hat{y}$$

$$= \pi G \rho \int_0^a dr \hat{y}$$

$$= \pi G \rho a \hat{y}$$

$$M_E = \rho \frac{4}{3} \pi R_E^3$$

$$M = \frac{\rho}{2} \frac{4}{3} \pi a^3 \cdot \frac{1}{2}$$

$$g_{yE} = \frac{3 M_E G a}{4 R_E^3}$$

$$\frac{3 M_E}{4 \pi R_E^3} = \rho$$

$$\frac{3 M}{4 \pi a^3} = \rho$$

$$g_{ym} = \frac{3 M G a}{4 a^3}$$

$$g_{ym} = \frac{3 M G}{4 a^2}$$

Field due to earth

$$g_0 = -\frac{G M_E}{R_E^2}$$

Field at center surface of hemisphere

$$g = g_0 + g_{yE} - g_{ym}$$

$$= g_0 + \frac{3}{4} \frac{M_E G a}{R_E^3} - \frac{3 M G}{4 a^2}$$

$$\frac{3 M_E}{4 \pi R_E^3} = \frac{3 M}{2 \pi a^3}$$

$$= g_0 + \frac{3}{4} \frac{2 M G}{a^2} - \frac{3 M G}{4 a^2}$$

$$M_E = \frac{2 M R_E^3}{a^3}$$

$$= g_0 + \frac{6}{4} \frac{M G}{a^2} - \frac{3}{4} \frac{M G}{a^2}$$

$$g = g_0 + \frac{3}{4} \frac{MG}{a^2}$$

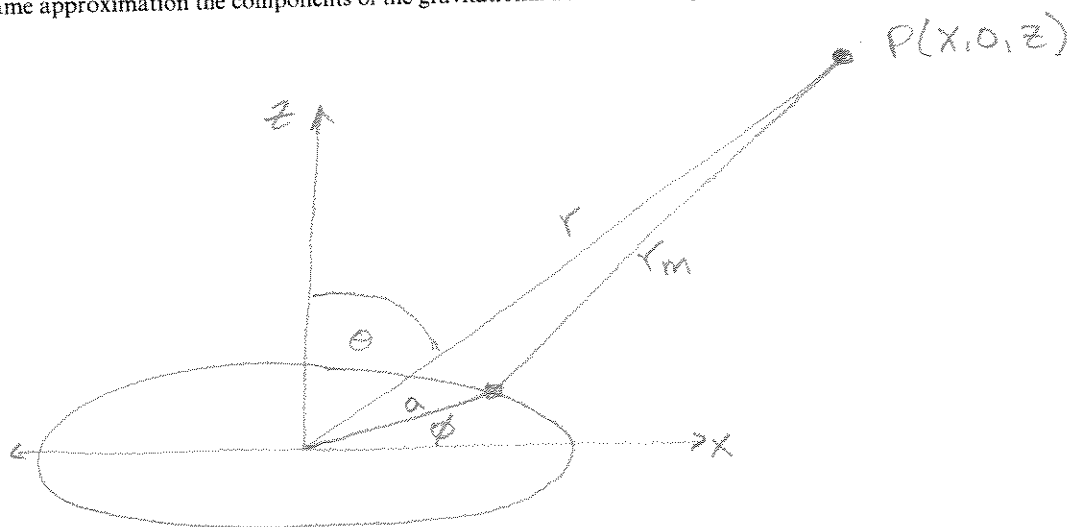
$$g_0 - g = -\frac{GM_E}{R_E^2} + \frac{GM_E}{R_E^2} - \frac{3}{4} \frac{MG}{a^2}$$

$$g_0 - g = -\frac{3}{4} \frac{MG}{a^2}$$

6 -

15. (a) Calculate the gravitational potential of a uniform circular ring of matter of radius a , mass M , at a distance r from the center of the ring in a direction making an angle θ with the axis of the ring. Assume that $r \gg a$, and calculate the potential only to second order in a/r .

b) Calculate to the same approximation the components of the gravitational field of the ring at the specified point.



a) U_g is independent of ϕ due to symmetry.

$$U_g = \int \frac{G dm}{|\vec{r}' - \vec{r}|}$$

$$|\vec{r}_m| = |\vec{r}_a - \vec{r}| \quad \vec{r}_a = a \cos \phi \hat{i} + a \sin \phi \hat{j}$$

$$\vec{r} = r \sin \theta \hat{i} + r \cos \theta \hat{k}$$

$$= G \sigma a \int_0^{2\pi} \frac{d\phi}{[r^2 + a^2 - 2ar \sin \theta \cos \phi]^{1/2}}$$

$$= 2G \sigma a \int_0^{\pi} [r^2 + a^2 - 2ar \sin \theta \cos \phi]^{-1/2} d\phi$$

$$= [(a \cos \phi - r \sin \theta)^2 + a^2 \sin^2 \phi + r^2 \cos^2 \theta]^{1/2}$$

$$= [a^2 (\cos^2 \phi + \sin^2 \phi) + r^2 (\cos^2 \theta + \sin^2 \theta) - 2ar \sin \theta \cos \phi]^{1/2}$$

Binomial Expansion

$$(1+b)^n = 1 + nb + \frac{n(n-1)}{2!} b^2 + \frac{n(n-1)(n-2)}{3!} b^3 + \dots$$

$$[r^2 + a^2 - 2ar \sin \theta \cos \phi]^{-1/2} =$$

$$\frac{1}{r} \left[1 + \frac{a^2}{r^2} - \frac{2a}{r} \sin \theta \cos \phi \right]^{-1/2}$$

$$n = -\frac{1}{2} \quad b = \frac{a^2}{r^2} - \frac{2a}{r} \sin \theta \cos \phi$$

$$(1+b)^n = 1 - \frac{a^2}{2r^2} + \frac{a}{r} \sin \theta \cos \phi + \frac{(-\frac{1}{2})(-\frac{3}{2})}{2} \frac{4a^2}{r^2} \sin^2 \theta \cos^2 \phi + \text{terms higher than } \frac{a^2}{r^2}$$

$$\approx 1 - \frac{a^2}{2r^2} + \frac{a}{r} \sin \theta \cos \phi + \frac{3}{2} \frac{a^2}{r^2} \sin^2 \theta \cos^2 \phi$$

$$|\vec{r}_m| = [r^2 + a^2 - 2ar \sin \theta \cos \phi]^{1/2}$$

$$dm = \sigma a d\phi, \quad \sigma = \text{linear density}$$

$$U_g = \frac{2G\sigma a}{r} \int_0^\pi \left[1 - \frac{a^2}{2r^2} + \frac{a}{r} \sin\theta \cos\phi + \frac{3}{2} \frac{a^2}{r^2} \sin^2\theta \cos^2\phi \right] d\phi$$

$$\int_0^\pi \cos\phi d\phi = \sin\phi \Big|_0^\pi = 0$$

$$\int_0^\pi \cos^2\phi d\phi = \frac{1}{2} \int_0^\pi (1 + \cos 2\phi) d\phi = \frac{1}{2} \left[\phi \Big|_0^\pi + \frac{1}{2} \sin 2\phi \Big|_0^\pi \right] = \frac{\pi}{2}$$

$$U_g = \frac{2G\sigma a}{r} \left[\pi - \frac{a^2}{2r^2} \pi + 0 + \frac{3}{2} \frac{a^2}{r^2} \sin^2\theta \frac{\pi}{2} \right] \quad M = 2\pi\sigma a$$

$$= \frac{MG}{r} \left[1 - \frac{a^2}{2r^2} + \frac{3}{4} \frac{a^2}{r^2} \sin^2\theta \right]$$

$$= \frac{MG}{r} \left[1 - \frac{a^2}{2r^2} + \frac{3}{4} \frac{a^2}{r^2} (1 - \cos^2\theta) \right]$$

$$= \frac{MG}{r} \left[1 - \frac{a^2}{2r^2} + \frac{3a^2}{4r^2} - \frac{3a^2}{4r^2} \cos^2\theta \right]$$

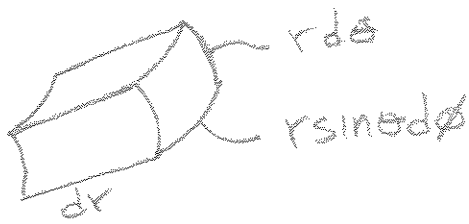
$$= \frac{MG}{r} \left[1 + \frac{a^2}{4r^2} - \frac{3a^2}{4r^2} \cos^2\theta \right]$$

$$= \frac{MG}{r} \left[1 + \frac{a^2}{4r^2} (1 - 3\cos^2\theta) \right]$$

$$\boxed{U_g = \frac{MG}{r} + \frac{MGa^2}{4r^3} (1 - 3\cos^2\theta)}$$

b) Gradient in spherical coordinates

$$\vec{\nabla} = \vec{e}_1 \frac{\partial}{\partial s_1} + \vec{e}_2 \frac{\partial}{\partial s_2} + \vec{e}_3 \frac{\partial}{\partial s_3}$$



$$\vec{e}_1 = \hat{r} \, ds_1 = dr \quad \vec{e}_2 = \hat{\theta} \, ds_2 = r d\theta \quad \vec{e}_3 = \hat{\phi} \, ds_3 = r \sin\theta d\phi$$

$$\vec{V} = \frac{d}{dr} \hat{r} + \frac{1}{r} \frac{d}{d\theta} \hat{\theta} + \frac{1}{r \sin\theta} \frac{d}{d\phi} \hat{\phi}$$

$\vec{g}$ is independent of ϕ

$$\vec{g}_r = \frac{dU}{dr} \hat{r}$$

$$\vec{g}_r = \left[-\frac{MG}{r^2} - \frac{3MGa^2}{r^4} (1 - 3\cos^2\theta) \right] \hat{r}$$

$$\vec{g}_\theta = \frac{1}{r} \frac{dU}{d\theta} \hat{\theta}$$

$$= \frac{1}{r} \frac{6MGa^2}{4r^3} \cos\theta \sin\theta \hat{\theta}$$

$$\sin(A+B) = \sin A \cos B + \cos A \sin B$$

$$\sin(2A) = 2 \sin A \cos A$$

$$\vec{g}_\theta = \frac{3MGa^2}{4r^4} \sin 2\theta \hat{\theta}$$

7-1

a) Fixed coordinate system:

$$m \frac{d^2 \vec{x}}{dt^2} = \vec{F}$$

Coordinate system translating with acceleration $\vec{g}$.

$$m \frac{d^2 \vec{x}^*}{dt^2} + m \vec{a}_h = \vec{F}$$

$$\vec{a}_h = \vec{g}$$

$$m \frac{d^2 \vec{x}^*}{dt^2} + m \vec{g} = \vec{F}$$

$$m \frac{d^2 \vec{x}^*}{dt^2} = \vec{F} - m \vec{g}$$

$$\vec{F} = m \vec{g}$$

$$\frac{d^2 \vec{x}^*}{dt^2} = \vec{g} - \vec{g}$$

$$\frac{d^2 \vec{x}^*}{dt^2} = 0 = \vec{a}_x^*$$

$$\frac{d \vec{x}^*}{dt} = C_1$$

$$v_0^* = 0 \rightarrow \frac{d \vec{x}^*}{dt} = 0 \rightarrow C_1 = 0$$

$$\vec{x}^* = C_2$$

$$\vec{x}_0^* = 0 \rightarrow C_2 = 0$$

$$\boxed{\vec{x}^* = 0}$$

$$a_x = a_x^* + a_{hx} \quad a_{hx} = -g$$

$$a_x = 0 - g$$

$$m a_x = -m g$$

$$a_x = -g$$

$$\frac{d^2 x}{dt^2} = -g \rightarrow \frac{dx}{dt} = -gt + C_1 \rightarrow \frac{dx}{dt} = -gt \rightarrow x = -\frac{1}{2} g t^2 + C_2$$

$$x_0 = 0$$

$$\boxed{x = -\frac{1}{2} g t^2}$$

b)

$$\vec{a}_h = \vec{g}$$

$$m\ddot{x} + b\dot{x} + kx = F$$

$$F = m\ddot{x} + b\dot{x}, k=0, F = mg, a_h = g$$

$$\ddot{x} = \ddot{x}^* - a_h$$

air is fixed

$$\dot{x}^* = \dot{x} - \frac{dh}{dt}$$

$$\frac{dh}{dt} = g$$

$$\dot{x}^* = \dot{x} - gt$$

$$\frac{dh}{dt} = gt + C_1$$

$$\dot{x} = \dot{x}^* + gt$$

$$\frac{dh}{dt} = 0 \rightarrow C_1 = 0$$

$$mg = m(\ddot{x}^* - a_h) + b(\dot{x}^* + gt)$$

$$= m\ddot{x}^* - mg + b(\dot{x}^* + gt)$$

$$m\ddot{x}^* = -b(\dot{x}^* + gt)$$

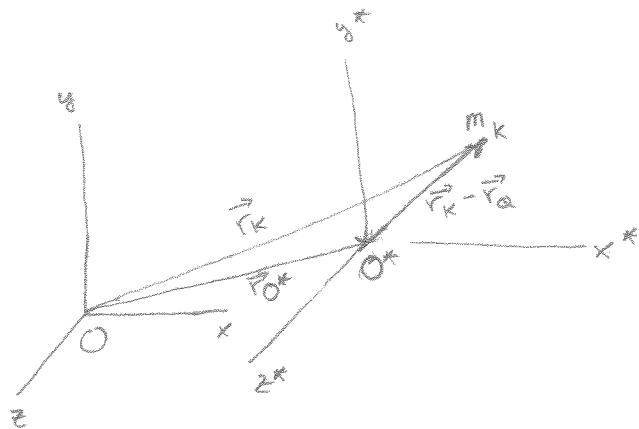
$$m\dot{x}^* = -bv^* - bgt$$

7-3

$$\text{Eq. (5-5)} \quad \frac{d\vec{L}}{dt} = \vec{N}$$

where $\vec{L}$ and $\vec{N}$ are about the point R

$$M\vec{R} = \sum_{k=1}^N m_k \vec{r}_k$$



$$a_h = \frac{d^2 \vec{r}_{O^*}}{dt^2} = \frac{d^2 \vec{h}}{dt^2} = \ddot{\vec{r}}_{O^*}$$

$$\vec{r} = \vec{r}_k$$

$$\vec{r}^* = \vec{r}_k - \vec{r}_{O^*}$$

$$(7.38) \quad \vec{r} = \vec{r}^* + \vec{h}$$

$$(7.39) \quad \frac{d\vec{r}}{dt} = \frac{d^* \vec{r}^*}{dt} + \vec{\omega} \times \vec{r}^* + \frac{d\vec{h}}{dt}$$

$$(7.40) \quad \frac{d^2 \vec{r}}{dt^2} = \frac{d^{*2} \vec{r}^*}{dt^2} + \vec{\omega} \times (\vec{\omega} \times \vec{r}^*) + 2\vec{\omega} \times \frac{d^* \vec{r}^*}{dt} + \frac{d\vec{\omega}}{dt} \times \vec{r}^* + \frac{d^2 \vec{h}}{dt^2}$$

$$\vec{L}_{kO^*} = m_k (\vec{r}_k - \vec{r}_{O^*}) \times (\dot{\vec{r}}_k - \dot{\vec{r}}_{O^*})$$

$$\frac{d\vec{L}_{kO^*}}{dt} = (\vec{r}_k - \vec{r}_{O^*}) \times \frac{d\vec{p}_k}{dt} + m_k (\vec{r}_k - \vec{r}_{O^*}) \times (\dot{\vec{r}}_k - \dot{\vec{r}}_{O^*}) - m_k (\vec{r}_k - \vec{r}_{O^*}) \times \ddot{\vec{r}}_{O^*}$$

$$= (\vec{r}_k - \vec{r}_{O^*}) \times \vec{F}_k^e + (\vec{r}_k - \vec{r}_{O^*}) \times \vec{F}_k^i - m_k (\vec{r}_k - \vec{r}_{O^*}) \times \ddot{\vec{r}}_{O^*}$$

$$\vec{L}_{O^*} = \sum_{k=1}^N \vec{L}_{kO^*}, \quad \vec{N}_{O^*} = \sum_{k=1}^N (\vec{r}_k - \vec{r}_{O^*}) \times \vec{F}_k^e$$

$$\frac{d\vec{L}_{O^*}}{dt} = \vec{N}_{O^*} - m_k (\vec{r}_k - \vec{r}_{O^*}) \times \ddot{\vec{r}}_{O^*} \quad \{ \text{internal torque is zero} \}$$

$$= \vec{N}_{O^*} - M(\vec{R} - \vec{r}_{O^*}) \times \ddot{\vec{r}}_{O^*}$$

$$\vec{r}_{O^*} = a_h = \frac{d^2 \vec{h}}{dt^2}$$

From Eq (7.40)

$$a_h = \frac{d^2 \vec{h}}{dt^2} = \frac{d^2 \vec{r}}{dt^2} - \frac{d^2 \vec{r}^*}{dt^2} - \vec{\omega} \times (\vec{\omega} \times \vec{r}^*) - 2\vec{\omega} \times \frac{d\vec{r}^*}{dt} - \frac{d\vec{\omega}}{dt} \times \vec{r}^*$$

$$\frac{d\vec{L}}{dt} = \vec{N}_{O^*} - M(\vec{R}^* - \vec{r}_{O^*}) \times \left[\frac{d^2 \vec{r}}{dt^2} - \frac{d^2 \vec{r}^*}{dt^2} - \vec{\omega} \times (\vec{\omega} \times \vec{r}^*) - 2\vec{\omega} \times \frac{d\vec{r}^*}{dt} - \frac{d\vec{\omega}}{dt} \times \vec{r}^* \right]$$

$$\xrightarrow{v, \ell}$$

$$\vec{f} = \vec{\nabla} p = \rho \vec{g}$$

Introducing the centrifugal and Coriolis forces in the rotating coordinate system can be treated as a fixed coordinate system

$$m \frac{d^2 \vec{r}}{dt^2} = \vec{F} + m \vec{g} - 2m \vec{\omega} \times \frac{d\vec{r}}{dt}$$

$$\frac{d\vec{r}}{dt} = v \hat{x} \quad (\text{westerly wind with velocity } v)$$

$$m \frac{d^2 \vec{r}}{dt^2} = 0 \quad (\text{constant velocity})$$

$$0 = \vec{F} - 2m \vec{\omega} \times v \hat{x}$$

$$\vec{F} = 2m \omega v \sin \alpha$$

$$\vec{F} = \rho \vec{g} V$$

$$\frac{\vec{F}}{V} = \rho \vec{g} = \vec{\nabla} p$$

$$\vec{\nabla} p = 2 \frac{m}{V} \omega v \sin \alpha$$

$$= 2 \rho \omega v \sin \alpha$$

$$\sin \alpha = \cos \theta$$



$$\boxed{\vec{\nabla} p = 2 \rho \omega v \cos \theta}$$

$$\rho_{\text{air}} = 1.2 \frac{\text{kg}}{\text{m}^3} \quad \omega_e = \frac{2\pi}{24 \text{ hrs}} = 7.3 \times 10^{-5} \frac{\text{rad}}{\text{s}} \quad v = 15 \frac{\text{m}}{\text{s}} \quad (10 \text{ miles per hour})$$

$$\nabla p = 2 \left(1.2 \frac{\text{kg}}{\text{m}^3} \right) (7.3 \times 10^{-5} / \text{s}) \left(15 \frac{\text{m}}{\text{s}} \right)$$

$$= .002 \frac{\text{kg}}{\text{m}^3} \frac{\text{m}}{\text{s}^2}$$

$$= .002 \frac{\text{N}}{\text{m}^3}$$

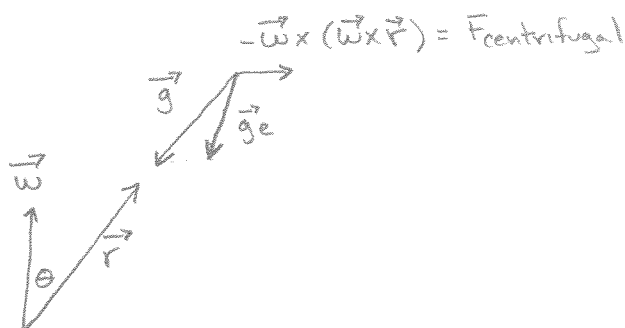
$$2.2 \text{ lb} = 1 \text{ kg}$$

$$= 9.81 \text{ N}$$

$$= .002 \frac{\text{N}}{\text{m}^3} \times \frac{2.2 \text{ lb}}{9.81 \text{ N}} \times \frac{(0.254 \text{ m})^3}{\text{in}^3} \times \frac{12 \text{ in}}{1 \text{ ft}} \times \frac{5280 \text{ ft}}{1 \text{ mile}}$$

$$\boxed{\nabla p = 4.7 \times 10^{-4} \frac{\text{lb}}{\text{in}^2 \cdot \text{mile}}}$$

7-7
a) $\vec{F}_{\text{cor}} = 2m\vec{\omega} \times \frac{d^* \vec{r}}{dt}$



$$|\vec{\omega} \times \vec{r}| = \omega r \sin \theta \rightarrow |\vec{\omega} \times (\vec{\omega} \times \vec{r})| = \omega^2 r \sin \theta$$

$$\vec{g}_e = \vec{g} - \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

$$\vec{g}_e = \vec{g} - \omega^2 r \sin \theta \hat{r}$$

To a first approximation

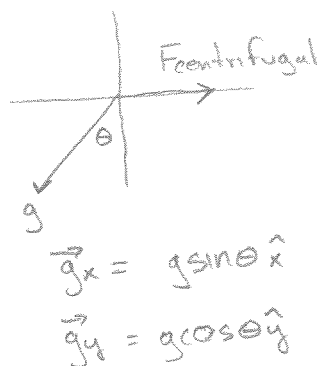
$$\vec{g}_e \approx \vec{g}$$

$$\frac{d^* \vec{r}}{dt} = \vec{g}$$

$$\frac{d^* \vec{r}}{dt} = \vec{g} t$$

$$F_{\text{cor}}(t) = 2m\vec{\omega} \times \vec{g} t$$

$$F_{\text{cor}}(t) = 2m\omega g t \sin \theta, \text{ towards the east}$$



b) $F_{\text{cor}}(t) = 2m\omega g t \sin \theta$

$$h = \frac{1}{2} g t^2$$

$$t^2 = \frac{2h}{g}$$

$$F_{\text{cor}} = 2m g \left(\frac{2h}{g} \right)^{1/2} \sin \theta$$

$$m a_{\text{cor}} = 2m \left(g h \right)^{1/2} \sin \theta$$

$$a_{\text{cor}} = 2 \omega \left(g h \right)^{1/2} \sin \theta$$

$$d = \frac{1}{2} a_{\text{cor}} t^2$$

$$= \frac{1}{2} a_{\text{cor}} \frac{2h}{g}$$

$$d = a_{\text{cor}} \frac{h}{g}$$

$$d = 2 \omega \frac{h_1^{3/2}}{g^{1/2}} \sin \theta \quad d'(h) = \frac{2\omega}{g^{1/2}} \frac{3h^{1/2}}{2} \sin \theta$$

$$x_{n+1} = x_n - \frac{f(x_n)}{f'(x_n)}$$

$$h_{n+1} = h_1 - \frac{h_1^{3/2}}{\frac{3}{2} h_1^{1/2}}$$

$$h_2 = h_1 - \frac{2}{3} h_1$$

$$= \frac{1}{3} h_1$$

$$d_2 = a_{\text{cor}} \frac{h_2}{g}$$

$$d_2 = a_{\text{cor}} \frac{h_1}{3g}$$

$$d_2 = \frac{1}{3} d_1 = \frac{2^{3/2} \omega h^{3/2}}{3 g^{1/2}} \sin \theta = \left(\frac{8 \omega^2 h^3}{9 g} \right)^{1/2} \sin \theta$$

Alternate method for b)

$$F_{\text{cor}} = 2m\omega g t \sin\theta$$

$$a_{\text{cor}} = 2\omega g t \sin\theta$$

$$v = \int a_{\text{cor}} dt = 2\omega g \sin\theta \int t dt$$

$$v = \omega g \sin\theta t^2$$

$$x = \int v dt = \omega g \sin\theta \int t^2 dt$$

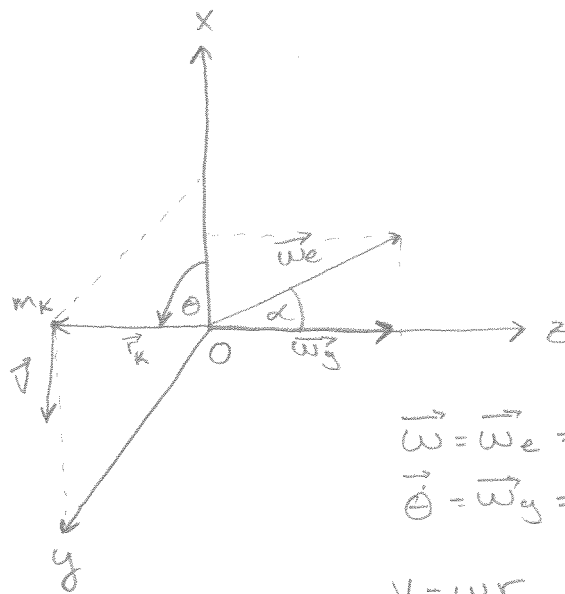
$$x = \frac{1}{3} \omega g t^3 \sin\theta$$

$$h = \frac{1}{2} g t^2$$

$$t = \left(\frac{2h}{g}\right)^{1/2}$$

$$x = \frac{1}{3} \omega g \left(\frac{2h}{g}\right)^{3/2} \sin\theta$$

$$x = \left(\frac{8\omega^2 h^3}{9g}\right)^{1/2} \sin\theta$$

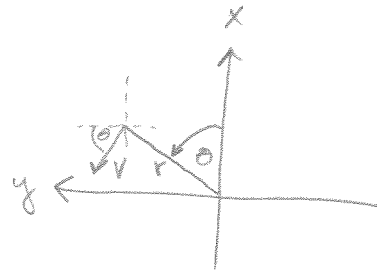


$$\vec{\omega} = \vec{\omega}_e = \omega \sin \alpha \hat{i} + \omega \cos \alpha \hat{k}$$

$$\vec{\dot{\theta}} = \vec{\omega}_g = \dot{\theta} \hat{k}$$

$$V = \omega_g r$$

$$= \dot{\theta} r$$



$$\vec{V} = -\dot{\theta} r \sin \theta \hat{i} + \dot{\theta} r \cos \theta \hat{j}$$

$$\vec{F}_{\text{cor}_{m_K}} = -2m_K \vec{\omega}_{\text{net}} \times \vec{V}$$

$$\vec{\omega}_{\text{net}} = \vec{\omega} + \vec{\omega}_g$$

$$= \omega \sin \alpha \hat{i} + (\omega \cos \alpha + \dot{\theta}) \hat{k}$$

$$= -2m_K \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \omega \sin \alpha & 0 & \omega \cos \alpha + \dot{\theta} \\ -\dot{\theta} r \sin \theta & \dot{\theta} r \cos \theta & 0 \end{vmatrix}$$

$$= -2m_K [-\dot{\theta} r \cos \theta (\omega \cos \alpha + \dot{\theta}) \hat{i} - \dot{\theta} r \sin \theta (\omega \cos \alpha + \dot{\theta}) \hat{j} + \omega \dot{\theta} r \cos \theta \sin \alpha \hat{k}]$$

$$\vec{N}_{\text{cor}_{m_K}} = \vec{r}_K \times \vec{F}_{\text{cor}_{m_K}}$$

$$\vec{r}_K = r \cos \theta \hat{i} + r \sin \theta \hat{j}$$

$$= -2m_K \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ r \cos \theta & r \sin \theta & 0 \\ -\dot{\theta} r \cos \theta (\omega \cos \alpha + \dot{\theta}) & -\dot{\theta} r \sin \theta (\omega \cos \alpha + \dot{\theta}) & \omega \dot{\theta} r \cos \theta \sin \alpha \end{vmatrix}$$

$$\begin{aligned}\vec{N}_{\text{cor } m_k} &= -2m_k \left[\omega \dot{\theta} r^2 \sin\theta \cos\theta \sin\alpha \hat{i} + \omega \dot{\theta} r^2 \cos^2\theta \sin\alpha \hat{j} \right. \\ &\quad \left. + (-\dot{\theta} r^2 \sin\theta \cos\theta (\omega \cos\alpha + \dot{\theta}) + \dot{\theta} r^2 \sin\theta \cos\theta (\omega \cos\alpha + \dot{\theta})) \hat{k} \right] \\ &= -2m_k \left[\omega \dot{\theta} r^2 \sin\theta \cos\theta \sin\alpha \hat{i} + \omega \dot{\theta} r^2 \cos^2\theta \sin\alpha \hat{j} \right]\end{aligned}$$

$$\boxed{\vec{N}_{\text{cor } m_k} = -2m_k \omega \dot{\theta} r^2 \sin\alpha \left[\sin\theta \cos\theta \hat{i} + \cos^2\theta \hat{j} \right]}$$

$$\vec{N}_{\text{cor}} = \sum_{k=1}^N \vec{N}_{\text{cor } m_k}$$

$$= \int_0^{2\pi} \frac{\vec{N}_{\text{cor } m_k}}{m_k} \lambda r d\theta$$

λ = linear mass density

$$= -2\lambda r^3 \omega \dot{\theta} \sin\alpha \left[\int_0^{2\pi} \sin\theta \cos\theta d\theta \hat{i} + \int_0^{2\pi} \cos^2\theta d\theta \hat{j} \right]$$

$$= -2\lambda r^3 \omega \dot{\theta} \sin\alpha \left[\frac{\sin^2\theta}{2} \Big|_0^{2\pi} \hat{i} + \int_0^{2\pi} \frac{1}{2} (1 + \cos 2\theta) d\theta \hat{j} \right]$$

$$= -2\lambda r^3 \omega \dot{\theta} \sin\alpha \left[\pi + \frac{1}{4} \sin 2\theta \Big|_0^{2\pi} \right] \hat{j}$$

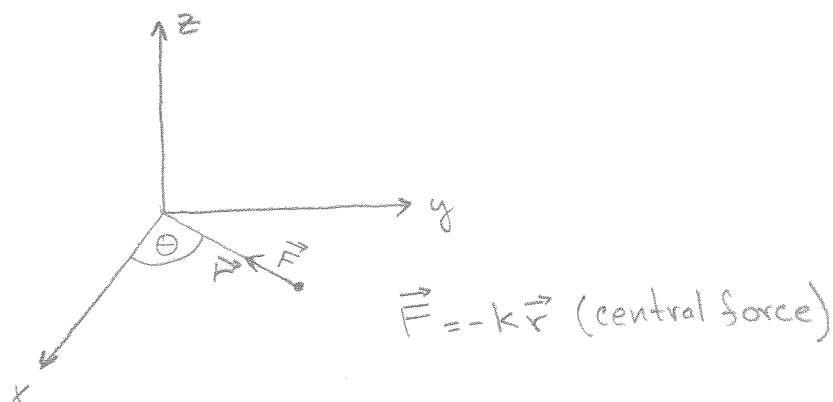
$$= -2\lambda \pi r^3 \omega \dot{\theta} \sin\alpha \hat{j}$$

$$\boxed{\vec{N}_{\text{cor}} = -\hat{j} M r^2 \omega \dot{\theta} \sin\alpha}$$

$$M = 2\pi r \lambda$$

Note: answer in text is $-\frac{1}{2} \hat{j} M r^2 \omega \dot{\theta} \sin\alpha$

7-13



Introducing a rotating coordinate system about the z -axis such that $m\vec{\omega} \times (\vec{\omega} \times \vec{r}) = \vec{F}$ {centrifugal force cancels F }.

With respect to the rotating coordinate system:

$$m \frac{d^{*2} \vec{r}}{dt^2} = \vec{F} - m\vec{\omega} \times (\vec{\omega} \times \vec{r}) - 2m\vec{\omega} \times \frac{d^* \vec{r}}{dt}$$

Now,

$$\vec{\omega} = \omega \hat{z}^*$$

$$\vec{r} = x \hat{x}^* + y \hat{y}^*$$

$$\vec{\omega} \times \vec{r} = \begin{vmatrix} \hat{x}^* & \hat{y}^* & \hat{z}^* \\ 0 & 0 & \omega \\ x & y & 0 \end{vmatrix}$$

$$= -y\omega \hat{x}^* + x\omega \hat{y}^*$$

$$\vec{\omega} \times (\vec{\omega} \times \vec{r}) = \begin{vmatrix} \hat{x}^* & \hat{y}^* & \hat{z}^* \\ 0 & 0 & \omega \\ -y\omega & x\omega & 0 \end{vmatrix}$$

$$= -x\omega^2 \hat{x}^* - y\omega^2 \hat{y}^*$$

$$= -\omega^2 (x \hat{x}^* + y \hat{y}^*)$$

$$\vec{\omega} \times (\vec{\omega} \times \vec{r}) = -\omega^2 \vec{r}$$

But, $m\vec{\omega} \times (\vec{\omega} \times \vec{r}) = \vec{F}$

$$-m\omega^2 \vec{r} = -k\vec{r}$$

$$\omega^2 = \frac{k}{m} \rightarrow \boxed{\omega = \sqrt{\frac{k}{m}}}$$

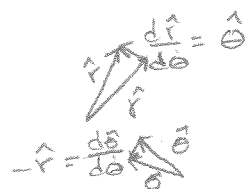
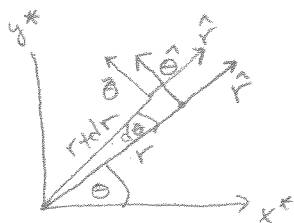
Since $\vec{F}$ cancels $-m\vec{\omega} \times (\vec{\omega} \times \vec{r})$,

$$m \frac{d^2 \vec{r}}{dt^2} = -2m\vec{\omega} \times \frac{d\vec{r}}{dt}$$

And since $\vec{r}$ lies in the x-y plane, $\frac{d\vec{r}}{dt}$ lies in the same plane, thus, $\vec{\omega}$ and $\frac{d\vec{r}}{dt}$ are always $\perp$.

$$\vec{r} = r(\theta) \hat{r}$$

$$\begin{aligned} \frac{d\vec{r}}{dt} &= \frac{dr}{dt} \hat{r} + r \frac{d\hat{r}}{dt} \\ &= \frac{dr}{dt} \hat{r} + r \frac{d\hat{r}}{d\theta} \frac{d\theta}{dt} \\ &= \dot{r} \hat{r} + r\dot{\theta} \hat{\theta} \end{aligned}$$



$$-2m\vec{\omega} \times \frac{d\vec{r}}{dt} = -2m \begin{vmatrix} \hat{r} & \hat{\theta} & \hat{z} \\ 0 & 0 & \omega \\ \dot{r} & r\dot{\theta} & 0 \end{vmatrix}$$

$$= -2m [-r\omega\dot{\theta} \hat{r} + \dot{r}\omega \hat{\theta}]$$

$$= 2mr\dot{\theta}\omega \hat{r} - 2m\dot{r}\omega \hat{\theta}$$

$$\frac{d^2 \vec{r}}{dt^2} = \frac{d}{dt} \left(\frac{d\vec{r}}{dt} \right)$$

$$= \frac{d}{dt} (\dot{r} \hat{r} + r\dot{\theta} \hat{\theta})$$

$$= \ddot{r} \hat{r} + \dot{r} \frac{d\hat{r}}{dt} + r\dot{\theta} \frac{d\hat{\theta}}{dt} + [\ddot{\theta} + \dot{\theta}^2] \hat{\theta}$$

$$= \ddot{r} \hat{r} + \dot{r} \frac{d\hat{r}}{d\theta} \frac{d\theta}{dt} + r\dot{\theta} \frac{d\hat{\theta}}{d\theta} \frac{d\theta}{dt} + [\ddot{\theta} + \dot{\theta}^2] \hat{\theta}$$

$$= \ddot{r} \hat{r} + \dot{r}\dot{\theta} \hat{\theta} - r\dot{\theta}^2 \hat{r} + r\ddot{\theta} \hat{\theta} + \dot{r}\dot{\theta} \hat{\theta}$$

$$= (\ddot{r} - r\dot{\theta}^2) \hat{r} + (2\dot{r}\dot{\theta} + r\ddot{\theta}) \hat{\theta}$$

Since $\vec{F}$ and $\vec{F}_{\text{centrifugal}}$ just cancel each other, there is no acceleration in the $\hat{r}^*$ direction. So,

$$\frac{d^2 \vec{r}}{dt^2} = (2\dot{r}\dot{\theta} + r\ddot{\theta})\hat{\theta}^*$$

$$\frac{d^2 \vec{r}}{dt^2} = r\ddot{\theta}\hat{\theta}^*$$

$$-2m\vec{\omega} \times \frac{d^2 \vec{r}}{dt^2} = 2mr\dot{\theta}\hat{r}^*$$

So,

$$1) mr\ddot{\theta}\hat{\theta}^* = -2m\dot{r}\omega\hat{\theta}^*$$

$$2) mr\dot{\theta}^2\hat{r}^* = 2mr\dot{\theta}\omega\hat{r}^* \quad \dot{r} = \text{constant} = C_0$$

$$1) mr\ddot{\theta} = -2mC_0\omega$$

$$2) mr\dot{\theta}^2 = 2mr\dot{\theta}\omega$$

$$1) \ddot{\theta} = -2\frac{C_0\omega}{r}$$

$$\frac{d}{dt}\dot{\theta} = -\frac{2C_0\omega}{r}$$

$$\dot{\theta} = -\frac{2C_0\omega}{r}t + C_1$$

$$\theta = -\frac{C_0\omega}{r}t^2 + C_1t + C_2$$

$$\theta(0) = \theta_0$$

$$\theta = -\frac{C_0\omega}{r}t^2 + C_1t + \theta_0$$

$$2) -r\dot{\theta}^2 - 2r\omega\dot{\theta} = 0$$

$$\dot{\theta}^2 + 2\omega\dot{\theta} = 0$$

$$\dot{\theta}(\dot{\theta} + 2\omega) = 0$$

$$\dot{\theta} = 0 \text{ or } \dot{\theta} = -2\omega$$

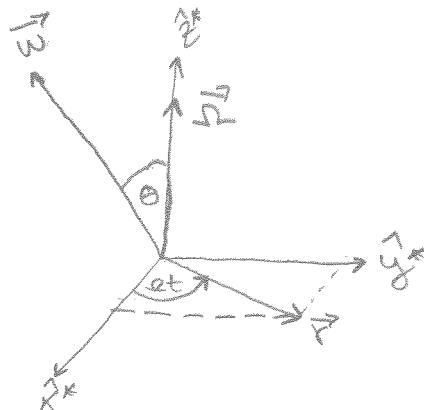
$$\theta = \text{Constant} \text{ or } \theta = -2\omega t + \theta_0$$

Therefore, the motion is circular where r and $\dot{\theta}$ depend on the initial conditions. The mass, m , has an angular velocity of -2ω .

7-15

$$\text{Eq. 7.46: } m \frac{d^{*2} \vec{r}}{dt^2} = \vec{r} + \vec{m}_{ge} - 2m\vec{\omega} \times \frac{d^{*} \vec{r}}{dt}$$

Let the circular motion of the bob have an angular frequency Ω . Then



$\hat{z}^*$ is $\perp$ to earth surface
 Θ is colatitude

$$\vec{r} = r \cos(\Omega t) \hat{x}^* + r \sin(\Omega t) \hat{y}^*$$

$$\frac{d^{*} \vec{r}}{dt} = -r\Omega \sin(\Omega t) \hat{x}^* + r\Omega \cos(\Omega t) \hat{y}^*$$

$$\vec{F}_{cor} = -2m\vec{\omega} \times \frac{d^{*} \vec{r}}{dt}$$

$$= -2m \begin{vmatrix} \hat{x}^* & \hat{y}^* & \hat{z}^* \\ 0 & -\omega \sin \Theta & \omega \cos \Theta + \Omega \\ -r\Omega \sin(\Omega t) & r\Omega \cos(\Omega t) & 0 \end{vmatrix}$$

$$= -2m \left[-r\Omega \cos(\Omega t) [\omega \cos \Theta + \Omega] \hat{x}^* - r\Omega \sin(\Omega t) [\omega \cos \Theta + \Omega] \hat{y}^* + r\omega \Omega \sin \Theta \sin(\Omega t) \hat{z}^* \right]$$

$$\vec{F}_{cor,vert} = -2mr\omega\Omega \sin \Theta \sin(\Omega t) \hat{z}^* \quad \left\{ \Omega = \frac{2\pi}{T} \right\}$$

The time average of $\vec{F}_{cor,vert}$ is

$$\frac{1}{T} \int_0^T \vec{F}_{cor,vert} dt = \frac{-2mr\omega\Omega \sin \Theta}{T} \int_0^T \sin\left(\frac{2\pi}{T}t\right) dt$$

$$= \frac{2mr\omega\Omega \sin \Theta}{T} \left[\frac{T}{2\pi} \cos\left(\frac{2\pi}{T}t\right) \Big|_0^T \right]$$

$$= \frac{mr\omega\Omega \sin \Theta}{\pi} [1-1]$$

$$= 0, \text{ and } |\vec{F}_{cor,v}| \ll 1 \quad \left\{ \omega = 10^{-5} \text{ rad/s} \right\}$$

Therefore, the vertical component of the Coriolis Force can be neglected.

The horizontal component is

$$\begin{aligned}\vec{F}_{\text{Cor}_H} &= 2mr\Omega [\cos(\Omega t) \hat{x}^* + \sin(\Omega t) \hat{y}^*] [\omega \cos\theta + \Omega] \\ &= 2mr\Omega \omega \cos\theta [\cos(\Omega t) \hat{x}^* + \sin(\Omega t) \hat{y}^*] + 2mr\Omega^2 [\cos(\Omega t) \hat{x}^* + \sin(\Omega t) \hat{y}^*]\end{aligned}$$

7-17

Problem 7-16 must be solved first.

7-16 For Larmor's Theorem to apply,
 $\omega_c \gg \omega_L$

To find ω_c , the angular frequency due to the central force,
 use Kepler's Law to relate the period to the semi major axis

$$\tau^2 = 4\pi^2 a^3 \left| \frac{m}{K} \right|$$

$$\tau^2 = 4\pi^2 10^{-30} \left| \frac{9.1 \times 10^{-31}}{(9 \times 10^9)(1.6 \times 10^{-19})^2} \right|$$

$$= 1.6 \times 10^{-31} \text{ s}^2$$

$$\tau = 4 \times 10^{-16} \text{ s}$$

$$\omega = \frac{2\pi}{\tau}$$

$$\omega_c = 1.6 \times 10^{16} \text{ rad/s}$$

$$\omega_L = -\frac{q}{2m} B \quad B = 10,000 \text{ G} = 1 \text{ T} \{ \text{MKS units} \}$$

$$= \frac{1.6 \times 10^{-19}}{2(9.1 \times 10^{-31})} (1)$$

$$\omega_L = 8.8 \times 10^{10} \text{ rad/s}$$

$$a = 10^{-8} \text{ cm} = 10^{-10} \text{ m}$$

Gaussian Units:

$$K = q^2 = (ce)^2 = (4.8 \times 10^{-10})^2$$

$$c = 2.99 \times 10^8 \text{ m/s} \times 2.99 \times 10^9 \text{ dm/s}$$

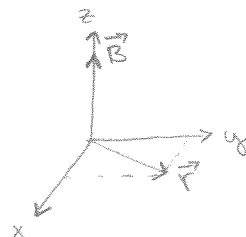
$$m_e = 9.1 \times 10^{-31} \text{ kg} = 9.1 \times 10^{-34} \text{ g}$$

Therefore, Larmor's Theorem applies and the angular velocity
 of precession is

$$\boxed{\omega_L = 8.8 \times 10^{10} \text{ rad/s}}$$

The potential for the last term of Eq. (7.58) when $\vec{B}$ is $\perp$ to
 the plane of the orbit is, starting with

$$\frac{q^2}{4mc^2} \vec{B} \times (\vec{B} \times \vec{r}) = -\frac{q^2 B^2}{4mc^2} \hat{r}$$



$$\vec{F}_1(r) = -\frac{K}{r^2}$$

$$V_1(r) = -\int_0^r F_1(r) dr$$

$$= -\frac{K}{r}$$

$$V_2(r) = -\int_0^r F_2(r) dr$$

$$= \frac{q^2 B^2}{4mc^2} \int_0^r r dr$$

$$= \frac{q^2 B^2}{4mc^2} \frac{r^2}{2}$$

$$V'(r) = V_1(r) + V_2(r) + \frac{L^2}{2mr^2}$$

$$= -\frac{K}{r} + \frac{q^2 B^2}{4mc^2} \frac{r^2}{2} + \frac{L^2}{2mr^2}$$

$$\frac{dV'}{dr} = \frac{K}{r^2} + \frac{q^2 B^2}{4mc^2} r - \frac{L^2}{mr^3}$$

$$0 = K r_0 + \frac{q^2 B^2}{4mc^2} r_0^4 - \frac{L^2}{m}$$

$$\frac{d^2 V'}{dr^2} = -\frac{2K}{r^3} + \frac{q^2 B^2}{4mc^2} + \frac{3L^2}{mr^4}$$

$$\omega_r^2 = \frac{1}{m} \left(\frac{d^2 V'}{dr^2} \right)_{r_0} = \frac{1}{m} \left(-\frac{2K}{r_0^3} + \frac{q^2 B^2}{4mc^2} + \frac{3L^2}{mr_0^4} \right)$$

$$L^2 = mK r_0 + \frac{q^2 B^2}{4c^2} r_0^4$$

$$\omega_r^2 = \frac{1}{m} \left(-\frac{2K}{r_0^3} + \frac{q^2 B^2}{4mc^2} + \frac{3}{mr_0^4} \left[mK r_0 + \frac{q^2 B^2}{4c^2} r_0^4 \right] \right)$$

$$= \frac{1}{m} \left(-\frac{2K}{r_0^3} + \frac{q^2 B^2}{4mc^2} + \frac{3K}{r_0^3} + \frac{3q^2 B^2}{4mc^2} \right)$$

$$= \frac{1}{m} \left(\frac{K}{r_0^3} + \frac{q^2 B^2}{4mc^2} + \frac{3q^2 B^2}{4mc^2} \right)$$

$$\omega_r = \left(\frac{K}{mr_0^3} + \frac{q^2 B^2}{4mc^2} + \frac{3q^2 B^2}{4mc^2} \right)^{1/2}$$

$$= \left(\frac{K}{mr_0^3} + 4\omega_L^2 \right)^{1/2}$$

$$\approx \left(\frac{K}{mr_0^3} \right)^{1/2} + \frac{1}{2} \left(\frac{mr_0^3}{K} \right)^{1/2} [4\omega_L^2]$$

$$(a+b)^{1/2} = a^{1/2} + \frac{1}{2} a^{-1/2} b + \dots$$

$$L = m r_0^2 \dot{\theta}$$

$$m r_0^2 \dot{\theta} = \left(mK r_0 + \frac{q^2 B^2}{4c^2} r_0^4 \right)^{1/2}$$

$$\dot{\theta} = \left(\frac{K}{mr_0^3} + \frac{q^2 B^2}{4mc^2} \right)^{1/2}$$

$$\dot{\theta} = \left(\frac{K}{mr_0^3} + \omega_L^2 \right)^{1/2}$$

$$\dot{\theta} \approx \left(\frac{K}{mr_0^3} \right)^{1/2} + \frac{1}{2} \left(\frac{mr_0^3}{K} \right)^{1/2} \omega_L^2$$

$$\omega_p = \omega_r - \dot{\Theta}$$

$$= \left(\frac{K}{mr_0^3} \right)^{1/2} + \frac{1}{2} \left(\frac{mr_0^3}{K} \right)^{1/2} (4\omega_L^2) - \left[\left(\frac{K}{mr_0^3} \right)^{1/2} + \frac{1}{2} \left(\frac{mr_0^3}{K} \right)^{1/2} (\omega_L^2) \right]$$

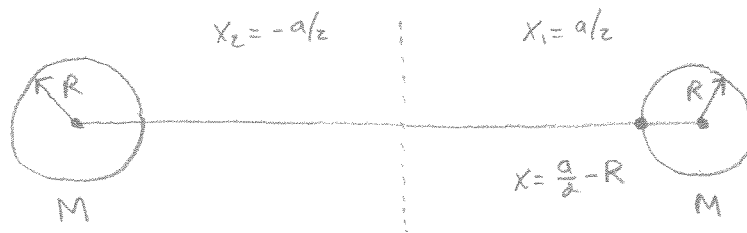
$$= -\frac{1}{2} \left(\frac{mr_0^3}{K} \right)^{1/2} (3\omega_L^2)$$

$$= -\frac{1}{2} \left[\frac{(9.1 \times 10^{-31})(10^{-10})^3}{(9 \times 10^9)(1.6 \times 10^{-19})^2} \right]^{1/2} (3(8.8 \times 10^6)^2)$$

$$\boxed{\omega_p = -0.73 \times 10^6 \text{ rad/s,}}$$

Therefore, ω_p should be subtracted from ω_L when the electron orbital angular frequency vector is in the same direction as $\vec{B}$, and added when the frequency vector is anti-parallel to $\vec{B}$.

7-21



$$V' = \frac{-mMG}{[(x-x_1)^2]^{1/2}} - \frac{mMG}{[(x-x_2)^2]^{1/2}} - \frac{m(M+M)Gx^2}{2a^3}$$

To escape the planet system

$$V = \pm \sqrt{\frac{2}{m} (E - V(x))}^{1/2}, \quad E = 0$$

$$= \pm \sqrt{\frac{2}{m} (-V(x))}^{1/2}$$

$$V' = \frac{-mMG}{\left[\left(\frac{a}{2} - R - \frac{a}{2}\right)^2\right]^{1/2}} - \frac{mMG}{\left[\left(\frac{a}{2} - R + \frac{a}{2}\right)^2\right]^{1/2}} - \frac{mMG}{a^3} \left(\frac{a}{2} - R\right)^2$$

$$V' = -mMG \left[\frac{1}{R} + \frac{1}{a-R} + \frac{\left(\frac{a}{2} - R\right)^2}{a^3} \right]$$

$$V = \sqrt{\frac{2}{m} (mMG)}^{1/2} \left(\frac{1}{R} + \frac{1}{a-R} + \frac{(a-2R)^2}{4a^3} \right)^{1/2}$$

The effective potential, V' , at $x=0$ is

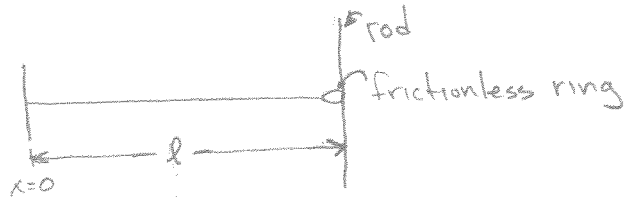
$$V'_{x=0} = \frac{-mMG}{\frac{a}{2}} - \frac{mMG}{\frac{a}{2}} = -\frac{4mMG}{a}$$

Therefore, $V'_{x=0}$ is subtracted from the planet system escape potential so that the rocket remains in the system and travels from one planet to the other. So,

$$V = \sqrt{2MG} \left[\frac{1}{R} + \frac{1}{a-R} - \frac{4}{a} + \frac{(a-2R)^2}{4a^3} \right]^{1/2}$$

If the system is non-rotating, the centrifugal term would be dropped thereby showing the escape velocity would be less compared to the rotational system.

8-1



a) Determine boundary condition at $x=l$

The vertical component of string tension, τ_v , is

$$\tau_v = \tau \frac{du}{dx}$$

Since the sliding ring is frictionless at $x=l$, there is no vertical force present.

So,

$$0 = \tau_v = \tau \frac{du}{dx}$$

Since $\tau \neq 0$ then

$$\left[\frac{du}{dx} \right]_{x=l} = 0$$

b) At $x=0$, the string is fixed

$$\text{B.C.: } u(0,t) = 0, \left[\frac{du}{dx} \right]_{x=l} = 0$$

$$\frac{\partial^2 u}{\partial x^2} - \frac{1}{c^2} \frac{\partial^2 u}{\partial t^2} = 0$$

$$u(x,t) = X(x) \Theta(t)$$

$$\frac{c^2}{X} \frac{d^2 X}{dx^2} = \frac{1}{\Theta} \frac{d^2 \Theta}{dt^2} = -\omega^2 \quad \frac{\partial^2 u}{\partial x^2} = \Theta \frac{d^2 X}{dx^2} \quad \frac{\partial^2 u}{\partial t^2} = X \frac{d^2 \Theta}{dt^2}$$

$$\frac{d^2 \Theta}{dt^2} + \omega^2 \Theta = 0$$

$$\frac{d^2 X}{dx^2} + \frac{\omega^2}{c^2} X = 0$$

$$\Theta = C_1 e^{\gamma_1 t}$$

$$X = C_2 e^{\gamma_2 x}$$

$$\gamma_1^2 + \omega^2 = 0$$

$$\gamma_2^2 + \frac{\omega^2}{c^2} = 0$$

$$\gamma_1^2 = -\omega^2$$

$$\gamma_2^2 = -\frac{\omega^2}{c^2}$$

$$\gamma_1 = \pm i\omega$$

$$\gamma_2 = \pm i \frac{\omega}{c}$$

$$\Theta = C_1 e^{\pm i\omega t}$$

$$X = C_2 e^{\pm i \frac{\omega}{c} x}$$

$$\Theta = A \cos \omega t + B \sin \omega t$$

$$X = C \cos \frac{\omega x}{c} + D \sin \frac{\omega x}{c}$$

$$\text{B.C. 1 } u(0,t) = X(0)\Theta(t) = 0$$

$$X(0) = 0$$

$$X(0) = C = 0$$

$$X = D \sin \frac{\omega x}{c}$$

$$\text{B.C. 2 } \left[\frac{du}{dx} \right]_{x=l} = 0$$

$$\frac{du}{dx} = \frac{dX}{dx} \Theta(t)$$

$$= D \frac{\omega}{c} \cos \frac{\omega x}{c} \Theta(t)$$

$$\left[\frac{du}{dx} \right]_{x=l} = D \frac{\omega}{c} \cos \frac{\omega l}{c} \Theta(t) = 0$$

$$\frac{\omega l}{c} = \frac{n\pi}{2}, n=1, 3, 5, \dots$$

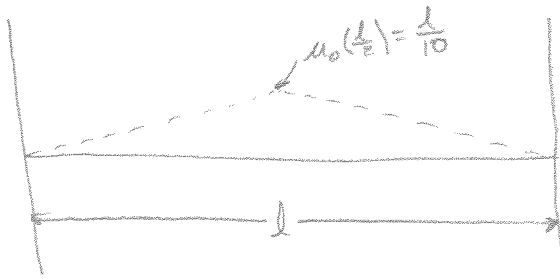
$$\omega_n = \frac{n\pi c}{2l}, n=1, 3, 5$$

$$u(x,t) = X(x)\Theta(t) \quad \{D=1\}$$

$$= \sin \frac{n\pi x}{2l} \left[A \cos \frac{n\pi ct}{2l} + B \sin \frac{n\pi ct}{2l} \right], n=1, 3, 5, \dots$$

$$u(x,t) = A \sin \frac{n\pi x}{2l} \cos \frac{n\pi ct}{2l} + B \sin \frac{n\pi x}{2l} \sin \frac{n\pi ct}{2l}, n=1, 3, 5, \dots$$

8-3



$$u(x,t) = \sum_{n=1}^{\infty} \left(A_n \sin \frac{n\pi x}{l} \cos \frac{n\pi ct}{l} + B_n \sin \frac{n\pi x}{l} \sin \frac{n\pi ct}{l} \right)$$

$$A_n = \frac{2}{l} \int_0^l u_0(x) \sin \frac{n\pi x}{l} dx$$

$$B_n = \frac{2}{n\pi c} \int_0^l v_0(x) \sin \frac{n\pi x}{l} dx$$

Determine $u_0(x)$

$$u_0(x) = \frac{x}{5} \quad 0 \leq x \leq \frac{l}{2} \quad u_0(x) = -\frac{x}{5} + \frac{l}{5} \quad \frac{l}{2} \leq x \leq l$$

$$v_0(x) = 0 \rightarrow B_n = 0$$

$$A_n = \frac{2}{l} \left[\int_0^{l/2} \frac{x}{5} \sin \frac{n\pi x}{l} dx - \int_{l/2}^l \frac{x}{5} \sin \frac{n\pi x}{l} dx + \int_{l/2}^l \frac{l}{5} \sin \frac{n\pi x}{l} dx \right]$$

$$= \frac{2}{5l} \left[\int_0^{l/2} x \sin \frac{n\pi x}{l} dx - \int_{l/2}^l x \sin \frac{n\pi x}{l} dx + l \int_{l/2}^l \sin \frac{n\pi x}{l} dx \right]$$

$$\int_a^b x \sin kx dx = uv|_a^b - \int_a^b v du = -\frac{x}{k} \cos kx|_a^b + \frac{1}{k} \int_a^b \cos kx dx$$

$$u=x \quad dv=\sin kx$$

$$du=dx \quad v=-\frac{1}{k} \cos kx$$

$$= -\frac{x}{k} \cos kx|_a^b + \frac{1}{k^2} \sin kx|_a^b$$

$$A_n = \frac{2}{5l} \left[-\frac{l x}{n\pi} \cos \frac{n\pi x}{l} \Big|_0^{l/2} + \frac{l^2}{n\pi^2} \sin \frac{n\pi x}{l} \Big|_0^{l/2} + \frac{l x}{n\pi} \cos \frac{n\pi x}{l} \Big|_{l/2}^l - \frac{l^2}{n\pi^2} \sin \frac{n\pi x}{l} \Big|_{l/2}^l + \frac{l^2}{n\pi} \cos \frac{n\pi x}{l} \Big|_{l/2}^l \right]$$

$$= \frac{2}{5l} \left[-\frac{l^2}{2n\pi} \cos \frac{n\pi}{2} + 0 + \frac{l^2}{n\pi^2} \sin \frac{n\pi}{2} - 0 + \frac{l^2}{n\pi} \cos n\pi - \frac{l^2}{2n\pi} \cos \frac{n\pi}{2} - \frac{l^2}{n\pi^2} \sin n\pi + \frac{l^2}{n\pi^2} \sin \frac{n\pi}{2} - \frac{l^2}{n\pi} \cos n\pi + \frac{l^2}{n\pi} \cos \frac{n\pi}{2} \right]$$

$$= \frac{2}{5l} \left[\frac{2l^2}{n\pi^2} \sin \frac{n\pi}{2} - \frac{l^2}{n\pi} \cos \frac{n\pi}{2} + \frac{l^2}{n\pi} \cos \frac{n\pi}{2} \right]$$

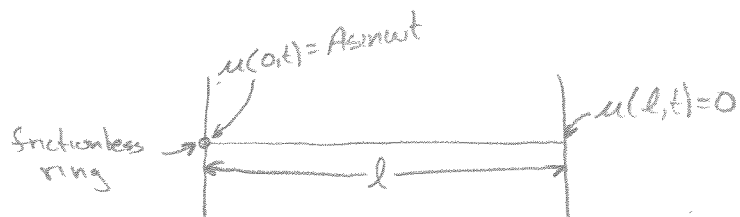
$$= \frac{2}{5l} \left[\frac{2l^2}{n\pi^2} \sin \frac{n\pi}{2} \right]$$

$$= \frac{4l}{5\pi^2 n^2} \sin \frac{n\pi}{2}$$

$$= \frac{4l}{5\pi^2} \left[1 - \frac{1}{9} + \frac{1}{25} - \dots \right] - \{ A_n = 0 \text{ for } n=2, 4, 6, \dots \}$$

$$u(x,t) = \frac{4l}{5\pi^2} \left(\sin \frac{\pi x}{l} \cos \frac{\pi ct}{l} - \frac{1}{9} \sin \frac{3\pi x}{l} \cos \frac{3\pi ct}{l} + \frac{1}{25} \sin \frac{5\pi x}{l} \cos \frac{5\pi ct}{l} - \dots \right)$$

8-5



Boundary conditions:

$$u(0,t) = A \sin \omega t$$

$$u(l,t) = 0$$

$$u(x,t) = X(x) \Theta(t)$$

$$X = C \cos \frac{\omega x}{c} + D \sin \frac{\omega x}{c}$$

$$A \sin \omega t = X(0) \Theta(t)$$

$$= C \Theta(t)$$

$$C = \frac{A \sin \omega t}{\Theta(t)}$$

$$X(l) \Theta(t) = 0$$

$$\frac{A \sin \omega t}{\Theta(t)} \cos \frac{\omega l}{c} + D \sin \frac{\omega l}{c} = 0$$

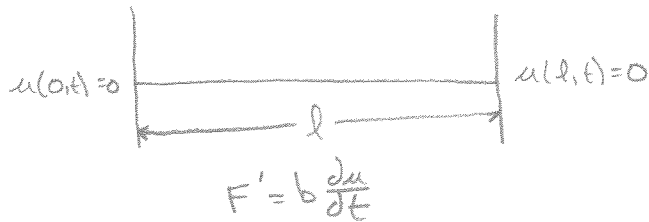
$$D = -\frac{A \sin \omega t}{\Theta(t)} \cot \frac{\omega l}{c}$$

$$u(x,t) = X(x) \Theta(t)$$

$$= \left[\frac{A \sin \omega t}{\Theta(t)} \cos \frac{\omega x}{c} - \frac{A \sin \omega t}{\Theta(t)} \cot \frac{\omega l}{c} \sin \frac{\omega x}{c} \right] \Theta(t)$$

$$u(x,t) = A \sin \omega t \left[\cos kx - \cot kl \sin kx \right], \quad k = \frac{\omega}{c}$$

8-7



$$\sigma \frac{\partial^2 u}{\partial t^2} = \tau \frac{\partial^2 u}{\partial x^2} + b \frac{du}{dt}$$

$$\sigma \frac{\partial^2 u}{\partial t^2} + b \frac{du}{dt} = \tau \frac{\partial^2 u}{\partial x^2}$$

$$\frac{\partial^2 u}{\partial t^2} + \frac{b}{\sigma} \frac{du}{dt} = \frac{\tau}{\sigma} \frac{\partial^2 u}{\partial x^2}$$

$$\frac{\partial^2 u}{\partial t^2} + \frac{b}{\sigma} \frac{du}{dt} = c^2 \frac{\partial^2 u}{\partial x^2}$$

$$\frac{\partial^2 u}{\partial t^2} - \frac{b}{\sigma} \frac{du}{dt} = -\omega^2 \quad c^2 \frac{\partial^2 u}{\partial x^2} = -\omega^2$$

$$u(x,t) = X(x) \Theta(t)$$

$$\frac{\partial^2 u}{\partial t^2} = X \frac{d^2 \Theta}{dt^2} \quad \frac{\partial^2 u}{\partial x^2} = \Theta \frac{d^2 X}{dx^2}$$

$$\frac{\partial u}{\partial t} = X \frac{d\Theta}{dt}$$

$$X \frac{d^2 \Theta}{dt^2} + \frac{b}{\sigma} X \frac{d\Theta}{dt} = c^2 \Theta \frac{d^2 X}{dx^2}$$

$$\frac{1}{\Theta} \frac{d^2 \Theta}{dt^2} + \frac{b}{\sigma} \frac{1}{\Theta} \frac{d\Theta}{dt} = \frac{c^2}{X} \frac{d^2 X}{dx^2} = -\omega^2$$

$$\frac{d^2 \Theta}{dt^2} + \frac{b}{\sigma} \frac{d\Theta}{dt} + \omega^2 \Theta = 0 \quad \frac{d^2 X}{dx^2} + \frac{\omega^2}{c^2} X = 0$$

$$\Theta = A e^{\gamma_1 t}$$

$$\gamma_1^2 + \frac{b}{\sigma} \gamma_1 + \omega^2 = 0$$

$$\gamma_1 = \frac{-\frac{b}{\sigma} \pm \sqrt{(\frac{b}{\sigma})^2 - 4\omega^2}}{2}$$

$$\gamma_1 = \frac{-\frac{b}{\sigma} \pm \sqrt{(\frac{b}{\sigma})^2 - \omega^2}}{2}$$

$$\Theta = A_1 e^{\frac{-\frac{b}{\sigma} \pm \sqrt{(\frac{b}{\sigma})^2 - \omega^2}}{2} t} = A_1 e^{\frac{-\frac{b}{\sigma} \pm i \sqrt{\omega^2 - (\frac{b}{\sigma})^2}}{2} t}$$

$$\Theta = e^{\frac{-\frac{b}{\sigma}}{2} t} (A \cos[\omega_1 t + \phi] + B \sin[\omega_1 t + \phi])$$

$$X = A_2 e^{\gamma_2 x}$$

$$\gamma_2^2 + \frac{\omega^2}{c^2} = 0$$

$$\gamma_2 = \pm i \frac{\omega}{c}$$

$$X = C \cos \frac{\omega x}{c} + D \sin \frac{\omega x}{c}$$

$$X(0) = C = 0$$

$$X(l) = D \sin \frac{\omega l}{c} = 0$$

$$\frac{\omega l}{c} = n\pi$$

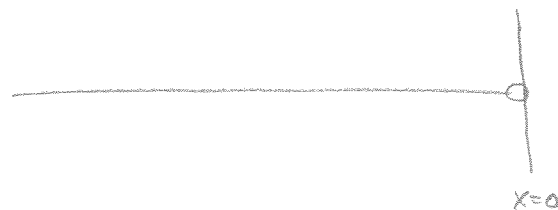
$$\omega_n = \frac{n\pi c}{l}, \quad n=1, 2, 3, \dots$$

$$X = \sin \frac{n\pi c}{l} x \quad \{D=1\}$$

$$u(x,t) = X(x) \Theta(t)$$

$$u(x,t) = A e^{-\frac{b}{2a}t} \sin \frac{n\pi c}{l} \cos \left\{ \left(\frac{n^2 \pi^2 c^2}{l^2} - \frac{b^2}{4a^2} \right)^{1/2} t + \Theta_0 \right\}, n=1, 2, 3, \dots$$

8-9



The vertical force, F_v , due to tension is

$$F_v = \tau \frac{du}{dx}$$

Therefore, the frictional force due to the ring is

$$F_f = -F_v$$

$$F_f = -\tau \frac{du}{dx}$$

Given that F_f is proportional to its velocity, this gives

$$-\tau \frac{du}{dx} \Big|_{x=0} = b \frac{du}{dt} \Big|_{x=0}$$

as a boundary condition. Now,

$$u(x,t) = f(\xi) + g(\eta), \quad \xi = x - ct, \quad \eta = x + ct \quad (f(\xi) \text{ is a wave moving to the right and } g(\eta) \text{ is a wave moving to the left})$$

$$= f(x - ct) + g(x + ct)$$

$$\frac{du}{dx} = \frac{df}{d\xi} \frac{d\xi}{dx} + \frac{dg}{d\eta} \frac{d\eta}{dx}$$

$$= \frac{df}{d\xi} + \frac{dg}{d\eta}$$

$$-\tau \frac{du}{dx} \Big|_{x=0} = -\tau \frac{df}{d\xi} \Big|_{x=0} - \tau \frac{dg}{d\eta} \Big|_{x=0}, \quad d\xi = dx - cdt, \quad d\eta = dx + cdt$$

$$= -\tau \frac{df}{-cdt} - \tau \frac{dg}{cdt}$$

$$= \tau \frac{df}{c} \frac{dt}{dt} - \tau \frac{dg}{c} \frac{dt}{dt}$$

$$\frac{du}{dt} = \frac{df}{d\xi} \frac{d\xi}{dt} + \frac{dg}{d\eta} \frac{d\eta}{dt}, \quad \frac{d\xi}{dt} = -c, \quad \frac{d\eta}{dt} = c$$

$$= -c \frac{df}{d\xi} + c \frac{dg}{d\eta}$$

$$b \frac{du}{dt} \Big|_{x=0} = -bc \frac{df}{-cdt} + bc \frac{dg}{cdt}$$

$$= b \frac{df}{dt} + b \frac{dg}{dt}$$

$$\text{B.C. } -\tau \frac{du}{dx} \Big|_{x=0} = b \frac{du}{dt} \Big|_{x=0}$$

$$\frac{\tau}{c} \frac{df}{dt} - \frac{\tau}{c} \frac{dg}{dt} = b \frac{df}{dt} + b \frac{du}{dt}$$

$$\frac{df}{dt} \left(\frac{\tau}{c} - b \right) = \frac{dg}{dt} \left(\frac{\tau}{c} + b \right)$$

$$\frac{df}{dt} \left(\frac{\tau - bc}{c} \right) = \frac{dg}{dt} \left(\frac{\tau + bc}{c} \right)$$

$$\frac{df}{dt} (\tau - bc) = \frac{dg}{dt} (\tau + bc)$$

$$\frac{dg}{dt} = \left(\frac{\tau - bc}{\tau + bc} \right) \frac{df}{dt}$$

Integrating both sides gives

$$g(n) = \left(\frac{\tau - bc}{\tau + bc} \right) f(\xi)$$

where $g(n)$ is the reflected wave.

When $bc < \tau$ there is no phase change upon reflection and the reflected amplitude is less than the amplitude of $f(\xi)$. When $bc > \tau$ a 180° phase change occurs upon reflection and its amplitude is less than $f(\xi)$.

Limiting cases:

i) $b \ll 1$

$$g(n) \approx f(\xi)$$

no phase change

no change in amplitude

ii) $b \gg 1$

$$g(n) \approx -f(\xi)$$

180° phase change

no change in amplitude

For no reflection

$$g(n) = 0$$

$$0 = \left(\frac{\tau - bc}{\tau + bc} \right) f(\xi)$$

$$0 = \tau - bc$$

$$b = \frac{\tau}{c} \quad \left(c = \left(\frac{\tau}{\sigma} \right)^{1/2} \right)$$

$$b = (\sigma \tau)^{1/2}$$

8-13

Eq. (8.139)

$$\frac{\partial \vec{v}}{\partial t} + \vec{v} \cdot \vec{\nabla} \vec{v} + \frac{1}{\rho} \vec{\nabla} p = \frac{\vec{f}}{\rho}$$

$$\frac{\partial \rho \vec{v}}{\partial t} + \rho \vec{v} \cdot \vec{\nabla} \vec{v} + \vec{\nabla} p = \vec{f}$$

$$\vec{r} \times \frac{\partial \rho \vec{v}}{\partial t} + \vec{r} \times \rho \vec{v} (\vec{v} \cdot \vec{\nabla}) + \vec{r} \times \vec{\nabla} p = \vec{r} \times \vec{f}$$

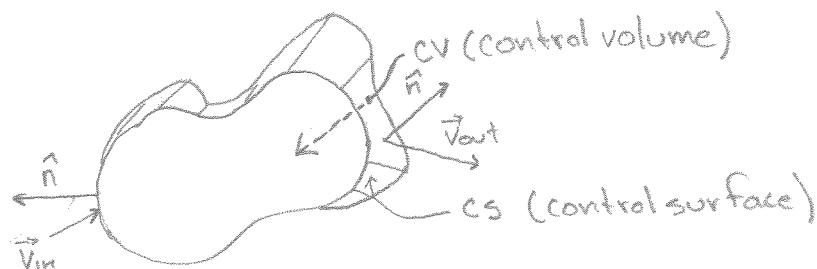
$$\frac{\partial}{\partial t} (\vec{r} \times \rho \vec{v}) + (\vec{v} \cdot \vec{\nabla}) \vec{r} \times \rho \vec{v} = \vec{r} \times \vec{f} - \vec{r} \times \vec{\nabla} p$$

Let $\vec{H} = \vec{r} \times \rho \vec{v}$, then

$$\begin{aligned} \frac{\partial \vec{H}}{\partial t} + \vec{H} (\vec{v} \cdot \vec{\nabla}) &= \vec{r} \times \vec{f} - \vec{r} \times \vec{\nabla} p \\ &= \vec{r} \times (\vec{f} - \vec{\nabla} p) \end{aligned}$$

$$\boxed{\frac{\partial \vec{H}}{\partial t} + \vec{H} (\vec{v} \cdot \vec{\nabla}) = \vec{Q}, \quad \vec{Q} = \vec{r} \times (\vec{f} - \vec{\nabla} p)}$$

8-15



Let B represent any amount (mass, linear momentum, angular momentum, energy, etc.)

$\beta = \frac{dB}{dm}$ be the amount per unit mass

Then

$$B_{cv} = \int_{cv} \beta \rho dV$$

The flux of B entering and leaving CS is

$$\int_{cs} \beta \rho \hat{n} \cdot \vec{v} dt dS \rightarrow B = B_{cv} + B_{flux}$$

The time rate of change of B is

$$\frac{d}{dt} B = \frac{d}{dt} \left(\int_{cv} \beta \rho dV \right) + \int_{cs} \beta \rho \hat{n} \cdot \vec{v} dS$$

Now, B is any amount. So, we use the energy per unit mass

$$\beta = \frac{1}{2} v^2 - G + u \quad \{\text{kinetic, gravitational, internal}\}$$

$$\frac{d}{dt} \left(\int_{cv} \left(\frac{1}{2} \rho v^2 - \rho G + \rho u \right) dV \right) + \int_{cs} \hat{n} \cdot \vec{v} \left(\frac{1}{2} \rho v^2 - \rho G + \rho u \right) dS = \frac{d}{dt} B_{outside}$$

The outside influence of flux is due to an inward pressure potential $\frac{p}{\rho}$ acting on the control surface. Also, the only outside influence acting within the control volume is G

$$\begin{aligned} \frac{d}{dt} B_{outside} &= \frac{d}{dt} \left(\int_{cv} -\rho G dV \right) - \int_{cs} \frac{p}{\rho} \rho \hat{n} \cdot \vec{v} dS \\ &= - \int_{cv} \rho \frac{\partial G}{\partial t} dV - \int_{cs} \hat{n} p \cdot \vec{v} dS \end{aligned}$$

8-17

The perfect gas law in terms of p and M :

$$p = \frac{\rho}{M} RT$$

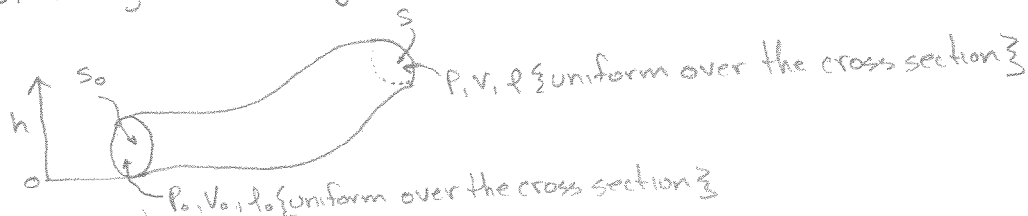
$$u = \int_{p_0}^p \frac{\rho d\ell}{\rho^2} \quad \ell = \frac{pM}{RT} \rightarrow d\ell = dP \frac{M}{RT}$$

$$= \int_{p_0}^p P dP \frac{M}{RT} \left(\frac{RT}{PM}\right)^2$$

$$= \int_{p_0}^p \frac{RT}{M} \frac{dP}{P}$$

$$\boxed{u = \frac{RT}{M} \ln\left(\frac{p}{p_0}\right)}$$

The flow of the gas is steady and isothermal.



For steady flow

$$\int_s \left(\frac{1}{2} \rho v^2 + p - \rho G_0 + \rho u \right) v dS = \int_{s_0} \left(\frac{1}{2} \rho v_0^2 + p_0 - \rho G_0 + \rho u_0 \right) v_0 dS_0$$

$$G(h) = \int_{h_0=0}^h \vec{g} \cdot d\vec{h}$$

$$= -gh \rightarrow G_0 = G(0) = 0$$

$$u_0 = \frac{RT}{M} \ln\left(\frac{p_0}{p_0}\right)$$

$$= 0$$

Equating the pressure terms, p and p_0 :

$$pVS = p_0V_0S_0$$

$$p = p_0 \frac{V_0S_0}{VS}$$

Then

$$u = \frac{RT}{M} \ln\left(\frac{V_0S_0}{VS}\right)$$

Also, for steady flow

$$\frac{d}{dt} \left[\left(\frac{1}{2} \rho V^2 + P - \rho G + \rho u \right) \delta V \right] = 0 \quad \left\{ \frac{\partial \rho}{\partial t} = 0 \text{ and } \frac{\partial G}{\partial t} = 0 \right\}$$

$$\frac{1}{2} \rho V^2 + P - \rho G + \rho u = \text{const.} \quad \text{divide both sides by } \delta m = \rho \delta V$$

$$\frac{1}{2} V^2 + \frac{P}{\rho} - G + u = \text{const.}$$

$$\frac{1}{2} V^2 + \frac{P}{\rho} - G + u = \frac{1}{2} V_0^2 + \frac{P_0}{\rho_0} - G_0 + u_0$$

$$V^2 + \frac{2P}{\rho} - 2G + 2u = V_0^2 + \frac{2P_0}{\rho_0} - 2G_0 + 2u_0$$

$$u_0 = G_0 = 0$$

$$\frac{2P}{\rho} = \frac{2P_0}{\rho_0} \rightarrow \frac{P}{\rho} = \frac{P_0}{\rho_0} \rightarrow \rho = \rho_0 \frac{P}{P_0}$$

$$= \rho_0 \frac{P_0 V_0 S_0}{P_0 V S}$$

$$= \rho_0 \frac{V_0 S_0}{V S}$$

$$G = -gh$$

$$V^2 + 2gh + 2u = V_0^2$$

$$V_0^2 - V^2 - 2u = 2gh$$

$$V_0^2 - V^2 - 2 \frac{RT}{M} \ln \left(\frac{V_0 S_0}{V S} \right) = 2gh$$

$$V_0^2 - V^2 + 2 \frac{RT}{M} \ln \left(\frac{V S}{V_0 S_0} \right) = 2gh$$

$$P = P_0 \frac{V_0 S_0}{V S}$$

$$\rho = \rho_0 \frac{V_0 S_0}{V S}$$

8-19

$$\phi = \frac{a}{r}$$

$$\vec{V} = \vec{\nabla} \phi$$

The gradient in spherical coordinates is

$$\vec{\nabla} = \hat{r} \frac{\partial}{\partial r} + \frac{1}{r} \frac{\partial}{\partial \theta} \hat{\theta} + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} \hat{\phi}$$

$$\vec{V} = \hat{r} \frac{\partial}{\partial r} \left(\frac{a}{r} \right)$$

$$\boxed{\vec{V} = -\frac{a}{r^2} \hat{r}}$$

8-21

Show that the normal modes of vibration of a fluid in a box have the velocity oscillation 90° out of phase with the pressure at any point.

$$\frac{\partial v_x}{\partial t} = -\frac{1}{\rho_0} \frac{\partial p'}{\partial x} \quad \frac{\partial v_y}{\partial t} = -\frac{1}{\rho_0} \frac{\partial p'}{\partial y} \quad \frac{\partial v_z}{\partial t} = -\frac{1}{\rho_0} \frac{\partial p'}{\partial z}$$

$$p' = (A \cos \omega_{lmn} t + B \sin \omega_{lmn} t) \cos \frac{l\pi x}{L_x} \cos \frac{m\pi y}{L_y} \cos \frac{n\pi z}{L_z} \quad (\text{P. 225})$$

Since the partial of p' is with respect to the space coordinates and the partial of v is with respect to time, it's clear that after finding $\frac{\partial p'}{\partial x}$, $\frac{\partial p'}{\partial y}$, and $\frac{\partial p'}{\partial z}$ then integrating with respect to time, the time dependent sine and cosine velocity terms will be 90° out of phase with p' .

The reason the velocity is out of phase by 90° with p' is due to Bernoulli's theorem:

$$\frac{v^2}{2} + \frac{p}{\rho} - \vec{g} \cdot \vec{u} = \text{a constant}$$

Here, $\vec{g}$ and $\vec{u}$ are zero. So,

$$v^2 + p = \text{a constant}$$

This states that when the particle velocity is zero the pressure is a maximum.

There is no discrepancy with the fact that a plane wave velocity and pressure are in phase. This is because a plane wave propagates with pressure whereas particle velocities oscillate about an equilibrium point and are stationary where pressure is a maximum.

8-23

a) Find the fluid velocity for the wave

$$p' = A \cos \frac{\ell \pi x}{L_x} \cos \frac{m \pi y}{L_y} \cos(k_z z - \omega t)$$

$$\frac{\partial v_x}{\partial t} = -\frac{1}{\rho_0} \frac{\partial p'}{\partial x} \quad \frac{\partial v_y}{\partial t} = -\frac{1}{\rho_0} \frac{\partial p'}{\partial y} \quad \frac{\partial v_z}{\partial t} = -\frac{1}{\rho_0} \frac{\partial p'}{\partial z}$$

$$-\frac{1}{\rho_0} \frac{\partial p'}{\partial x} = -\frac{1}{\rho_0} \left(-A \frac{\ell \pi}{L_x} \sin \frac{\ell \pi x}{L_x} \cos \frac{m \pi y}{L_y} \cos(k_z z - \omega t) \right)$$

$$-\frac{1}{\rho_0} \frac{\partial p'}{\partial y} = -\frac{1}{\rho_0} \left(-A \frac{m \pi}{L_y} \cos \frac{\ell \pi x}{L_x} \sin \frac{m \pi y}{L_y} \cos(k_z z - \omega t) \right)$$

$$-\frac{1}{\rho_0} \frac{\partial p'}{\partial z} = -\frac{1}{\rho_0} \left(-A k_z \cos \frac{\ell \pi x}{L_x} \cos \frac{m \pi y}{L_y} \sin(k_z z - \omega t) \right)$$

$$v_x = \int \frac{A \ell \pi}{L_x} \sin \frac{\ell \pi x}{L_x} \cos \frac{m \pi y}{L_y} \cos(k_z z - \omega t) \frac{dt}{\rho_0}$$

$$v_x = -\frac{A \ell \pi}{\omega \rho_0 L_x} \sin \frac{\ell \pi x}{L_x} \cos \frac{m \pi y}{L_y} \sin(k_z z - \omega t)$$

$$v_y = \int \frac{A m \pi}{L_y} \cos \frac{\ell \pi x}{L_x} \sin \frac{m \pi y}{L_y} \cos(k_z z - \omega t) \frac{dt}{\rho_0}$$

$$v_y = -\frac{A m \pi}{\omega \rho_0 L_y} \cos \frac{\ell \pi x}{L_x} \sin \frac{m \pi y}{L_y} \sin(k_z z - \omega t)$$

$$v_z = \int \frac{A k_z}{\rho_0} \cos \frac{\ell \pi x}{L_x} \cos \frac{m \pi y}{L_y} \sin(k_z z - \omega t) \frac{dt}{\rho_0}$$

$$v_z = \frac{A k_z}{\omega \rho_0} \cos \frac{\ell \pi x}{L_x} \cos \frac{m \pi y}{L_y} \cos(k_z z - \omega t)$$

b) Calculate the mean rate of power flow through the pipe.

$$P_{ave} = \langle p' v \rangle_{ave} = \frac{\langle p'^2 \rangle_{ave}}{(\rho_0 B)^{1/2}} \quad B = c \rho_0^{1/2}$$

$$\langle p'^2 \rangle_{ave} = \frac{1}{T} \int_0^T p'^2 dt \quad T = \frac{2\pi}{\omega}$$

$$= \frac{\omega}{2\pi} \int_0^{2\pi/\omega} p'^2 dt$$

$$= \frac{\omega}{2\pi} A^2 \cos^2 \frac{\ell \pi x}{L_x} \cos^2 \frac{m \pi y}{L_y} \int_0^{2\pi/\omega} \cos^2(k_z z - \omega t) dt$$

The average value of $\cos^2(k_z z - \omega t)$ is $\frac{1}{2}$, then

$$P_{\text{ave}} = \frac{\omega}{4\pi(\epsilon_0)^{1/2}} A^2 \cos^2 \frac{2\pi x}{L_x} \cos^2 \frac{m\pi y}{L_y}$$

8-25

$$p' = A \cos \frac{2\pi x}{L_x} \cos \frac{m\pi y}{L_y} \cos(k_z z - \omega t) \quad \{ \text{plane wave in } +z\text{-direction} \}$$

Boundary Condition: $v_z(0) = 0$ {this is the boundary condition for a plane wave in a fluid}



The reflected plane wave will simply be the plane wave p' traveling in the opposite direction. Namely

$$p'_R = A \cos \frac{2\pi x}{L_x} \cos \frac{m\pi y}{L_y} \cos(k_z z + \omega t)$$

8-27

Calculate the group velocity of the wave of a discrete string and compare to the phase velocity. show that the two are very nearly equal for wavelengths much greater than h .



$$u_j = A \cos(Kx_j - \omega t), \quad x_j = jh$$

For a discrete string

$$\cos p = 1 - \frac{\omega^2 m h}{2\tau}, \quad p = kh \quad \{8.73\}$$

$$1 - \cos(kh) = \frac{\omega^2 m h}{2\tau}$$

$$\frac{1 - \cos(kh)}{2} = \frac{\omega^2 m h}{4\tau}$$

$$\sin^2\left(\frac{kh}{2}\right) = \frac{\omega^2 m h}{4\tau}$$

$$\sin\left(\frac{kh}{2}\right) = \frac{\omega}{2} \left(\frac{m h}{\tau}\right)^{1/2}$$

$$\omega = \left(\frac{\tau}{m h}\right)^{1/2} 2 \sin\left(\frac{kh}{2}\right)$$

$$V_g = \frac{d\omega}{dk}$$

$$= \left(\frac{\tau}{m h}\right)^{1/2} 2 \left(\frac{h}{2}\right) \cos\left(\frac{kh}{2}\right)$$

$$V_g = \left(\frac{\tau h}{m}\right)^{1/2} \cos\left(\frac{kh}{2}\right)$$

$$c = \frac{\omega}{k}$$

$$= \left(\frac{\tau}{m h}\right)^{1/2} \frac{2}{k} \sin\left(\frac{kh}{2}\right)$$

$$c = \left(\frac{\tau h}{m}\right)^{1/2} \frac{2}{kh} \sin\left(\frac{kh}{2}\right)$$

$$k = \frac{2\pi}{\lambda}$$

$$V_g = \left(\frac{\hbar^2 k}{m}\right)^{1/2} \cos\left(\frac{k h}{2}\right)$$

$$= \left(\frac{\hbar^2 k}{m}\right)^{1/2} \cos\left(\frac{\pi h}{\lambda}\right)$$

$$C = \left(\frac{\hbar^2 k}{m}\right)^{1/2} \frac{2}{kh} \sin\left(\frac{k h}{2}\right)$$

$$= \left(\frac{\hbar^2 k}{m}\right)^{1/2} \frac{\lambda}{\pi h} \sin\left(\frac{\pi h}{\lambda}\right)$$

For $\lambda \gg h$

$$\cos\left(\frac{\pi h}{\lambda}\right) \rightarrow 1 \quad \text{and} \quad \frac{\lambda}{\pi h} \sin\left(\frac{\pi h}{\lambda}\right) \rightarrow \frac{\lambda}{\pi h} \cdot \frac{\pi h}{\lambda} \rightarrow 1$$

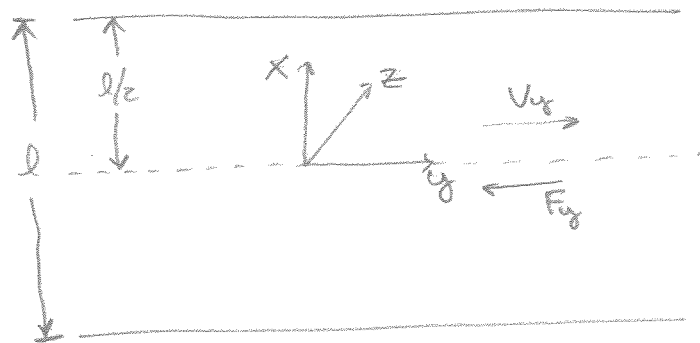
Therefore, when $\lambda \gg h$

$$V_g \doteq \left(\frac{\hbar^2 k}{m}\right)^{1/2}$$

$$C \doteq \left(\frac{\hbar^2 k}{m}\right)^{1/2}$$

8-29

Given μ and I' for flow between two infinite parallel plates find the velocity distribution and the pressure gradient parallel to the plates. Assume the pressure varies only in the direction of flow. I' is the current flow per unit length.



$$\mu = \frac{F_y / A_{yz}}{\frac{dV_x}{dx}} \quad F_y / A_{yz} = \tau \text{ \{shear stress\} } \rightarrow \tau = \mu \frac{dV_x}{dx}$$

Sum of forces must be zero:

$$F_{\text{press}} + F_y = 0$$

$$dp dx dz + d\tau dy dz = 0$$

$$-dp dx = d\tau dy$$

$$-\frac{dp}{dy} = \frac{d\tau}{dx}$$

$$= \frac{d}{dx} \left(\mu \frac{dV_x}{dx} \right)$$

$$-\frac{dp}{dy} \frac{1}{\mu} = \frac{d^2 V_x}{dx^2}$$

$$-\frac{1}{\mu} \frac{dp}{dy} dx = \frac{1}{dx} d^2 V_x$$

$$-\frac{1}{\mu} \frac{dp}{dy} x + A = \frac{1}{dx} dV_x$$

$$-\frac{1}{\mu} \frac{dp}{dy} x dx + A dx = dV_x$$

$$-\frac{1}{\mu} \frac{dp}{dy} \frac{x^2}{2} + Ax + B = V_x$$

$$v_y = 0 \text{ at } x = l/2 \text{ and } -l/2$$

$$0 = -\frac{1}{n} \frac{dp}{dy} \left(\frac{l^2}{8} \right) + A \left(\frac{l}{2} \right) + B$$

$$B = \frac{1}{n} \frac{dp}{dy} \frac{l^2}{8} - A \frac{l}{2}$$

$$0 = -\frac{1}{n} \frac{dp}{dy} \left(\frac{l^2}{8} \right) - A \frac{l}{2} + B$$

$$0 = -\frac{1}{n} \frac{dp}{dy} \frac{l^2}{8} - A \frac{l}{2} + \frac{1}{n} \frac{dp}{dy} \frac{l^2}{8} - A \frac{l}{2}$$

$$0 = -A l$$

$$0 = A$$

$$B = \frac{1}{n} \frac{dp}{dy} \frac{l^2}{8}$$

$$v_y = -\frac{1}{n} \frac{dp}{dy} \frac{x^2}{2} + \frac{1}{n} \frac{dp}{dy} \frac{l^2}{8}$$

$$v_y = \frac{1}{n} \frac{dp}{dy} \left(\frac{l^2}{8} - \frac{x^2}{2} \right)$$

$$I = \iint \rho v_y dS \quad dS = dx dz$$

$$= \frac{1}{n} \frac{dp}{dy} \int_{-l/2}^{l/2} \int_{-l/2}^{l/2} \left(\frac{l^2}{8} - \frac{x^2}{2} \right) dx dz$$

$$= \frac{1}{n} \frac{dp}{dy} \int_{-l/2}^{l/2} \left. \frac{l^2}{8} x - \frac{x^3}{6} \right|_{-l/2}^{l/2} dz$$

$$= \frac{1}{n} \frac{dp}{dy} \left[\frac{l^3}{8} - \frac{l^3}{24} \right] l$$

$$\frac{I}{l} = I' = \frac{1}{n} \frac{dp}{dy} \frac{l^3}{12}$$

$$\boxed{\frac{dp}{dy} = \frac{12 n I'}{l^3}}$$

$$v_y = \frac{1}{n} \frac{12 n I'}{l^3} \left(\frac{l^2}{8} - \frac{x^2}{2} \right)$$

$$\boxed{v_y = \frac{3 n I'}{2 l^3} (l^2 - 4 x^2)}$$